

REVIEWED

By Jake Mowat at 12:42 pm, Jul 24, 2019



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736

MANUFACTURER DATA REPORT

132" OD x 82'-10" S/S INLET SLUG CATCHER

for

ANADARKO E&P ONSHORE LLC

EMP JOB # 5361-1

TAG # V-1000

May 8, 2019



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736

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Eaton Metal Products Company LLC

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PETROLEUM EQUIPMENT

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Document Index Log

EATON METAL PRODUCTS COMPANY LLC

Document Index Log

JOB NUMBER 5361-1

DATA SHEET REGISTERED YES ☒ NO ☐

DOCUMENT	STORAGE LOCATION	RETENTION DATE	QAM	AI
☒ Manufacturer's Data Report	PWA - electronic	5/15/2024	Data Reports <i>FM</i>	<i>Z</i>
☒ Nameplate Picture	PWA - electronic	5/15/2024	Data Reports <i>FM</i>	<i>Z</i>
☒ Manufacturer's Drawings	PWA - electronic	5/15/2024	Drawings <i>FM</i>	<i>Z</i>
☒ Design Calculations	PWA - electronic	5/15/2024	Calculations <i>FM</i>	<i>Z</i>
☒ MTRs	PWA - electronic	5/15/2024	Material Records <i>FM</i>	<i>Z</i>
☒ WPS / PQR	PWA - electronic	5/15/2024	WPS / WPQ <i>FM</i>	<i>Z</i>
☒ WPQ / Continuity Records	PWA - electronic	5/15/2024	WPS / WPQ <i>FM</i>	<i>Z</i>
☒ NDE Reports	PWA - electronic	5/15/2024	NDE Reports <i>FM</i>	<i>Z</i>
☐ Repair Procedure / Records	PWA - electronic	N/A	N/A	N/A
☒ Process Control Sheets (ITP)	PWA - electronic	5/15/2024	Inspection Records <i>FM</i>	<i>Z</i>
☒ Weld Map Description	PWA - electronic	5/15/2024	Inspection Records <i>FM</i>	<i>Z</i>
☒ Paint Inspection Records	PWA - electronic	5/15/2024	Inspection Records <i>FM</i>	N/A
☒ Hydrostatic Test Records	PWA - electronic	5/15/2024	Inspection Records <i>FM</i>	<i>Z</i>
☐ PWHT Records	PWA - electronic	N/A	N/A	N/A
☐ NCRs	PWA - electronic	N/A	N/A	N/A



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736

ASME Data Reports

1. Manufactured and certified by Eaton Metal Products Company LLC Plant #3, 669 West Quinn Road Building #16, Pocatello, Idaho, 83201
(Name and address of Manufacturer)

2. Manufactured for ANADARKO E&P ONSHORE LLC, UNKOWN, Colorado
(Name and address of Purchaser)

3. Location of Installation Johnstown Compressor Station, Colorado
(Name and address)

4. Type Horizontal 282 N/A D-5361-1 274 2019
(Horizontal or vertical, tank) (Manufacturer's serial number) (CRN) (Drawing number) (National Board number) (Year built)

5. ASME Code, Section VIII, Division 1 2017/ N/A N/A N/A
(Edition and Addenda, if applicable (date)) (Code Case numbers) (Special service per UG-120(d))

6. Shell: SA-516-70 .875 in 0 in 11' (OD) 82' 10"
(Material spec. number, grade) (Nominal thickness) (Corr. allow.) (Inner diameter) (Length (overall))

Body Flanges on Shells												
No.	Type	ID	OD	Flange Thk	Min Hub Thk	Material	How Attached	Location	Bolting			
									Num & Size	Bolting Material	Washer (OD, ID, thk)	Washer Material
N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

7. Seams: Type 1, Butt Full 100 N/A N/A Type 1, Butt Spot 85 8
(Long. (welded, dbl., sngl., lap, butt)) (R.T. (spot or full)) (Eff. %) (H.T. temp) (Time, hr) (Girth. (welded, dbl., sngl., lap, butt)) (R.T. (spot or full)) (Eff. %) (No. of courses)

8. Heads: (a) Material SA-516-70 (b) Material SA-516-70
(Spec. no., grade) (Spec. no., grade)

	Location (Top, Bottom, Ends)	Minimum Thickness	Corrosion Allowance	Crown Radius	Knuckle Radius	Elliptical Ratio	Conical Apex Angle	Hemispherical Radius	Flat Diameter	Side to Pressure (Convex or Concave)
(a)	End	.85	0	N/A	N/A	2:1	N/A	N/A	N/A	Concave
(b)	End	.85	N/A	N/A	N/A	2:1	N/A	N/A	N/A	Concave

Body Flanges on Heads												
	Location	Type	ID	OD	Flange Thk	Min Hub Thk	Material	How Attached	Bolting			
									Num & Size	Bolting Material	Washer (OD, ID, thk)	Washer Material
(a)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A		N/A	N/A	N/A

9. MAWP 250 psi N/A at max. temp. 125 °F N/A
(Internal) (External) (Internal) (External)

Min. design metal temp. -20 °F at 250 psi . Hydro, pneu., or comb. test pressure HYDRO at 325 psi .

Proof test N/A .

10. Nozzles, inspection and safety valve openings:

Purpose (Inlet, Outlet, Drain, etc.)	No.	Diameter or Size	Type	Material		Nozzle Thickness		Reinforcement Material	Attachment Details		Location (Insp. Open.)
				Nozzle	Flange	Nom.	Corr.		Nozzle	Flange	
Manway	3	20	RF150WN	SA-106B	SA-105	.5	0	SA-516-70	UW-16.1 (d)	Butt weld	In Shell/ Head
Inlet/Outlet	2	24	RF150WN	SA-106B	SA-105	.5	0	SA-516-70	UW-16.1 (d)	Butt weld	
Various	3	2	RF150LWN	SA-105		.53	0	Inherent	UW-16.1 (d)		
Various	3	3	RF150LWN	SA-105		1.02	0	Inherent	UW-16.1 (d)		
Various	3	6	RF150LWN	SA-105		1.245	0	Inherent	UW-16.1 (d)		
Level Gauge	1	2	CPLG6000	SA-105		.625	0	Inherent	UW-16.1 (d)		
LAHH	1	4	RF150LWN	SA-105		1.305	0	Inherent	UW-16.1 (d)		
Boot	1	36	RF150WN	SA-106B	SA-105	.5	0	SA-516-70	UW-16.1 (d)	Butt weld	

Additional Nozzles - See Attached U-4...

11. Supports: Skirt No Lugs 0 Legs 0 Other Saddles Attached Welded to Wear Pad
(Yes or no) (Number) (Number) (Describe) (Where and how)

12. Remarks: Manufacturer's Partial Data Reports properly identified and signed by Commissioned Inspectors, have been furnished for the following items of the report:

N/A

(Name of part, item number, Manufacturer's name and identifying stamp)

Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F
Safety Relief Device By Others
(3) 20" RF150BLIND attached to vessel with (20) 1 - 1/8" Full Thread Studs (SA-193-B7) and (40) 1 - 1/8" Heavy Hex Studs (SA-194-2H) each

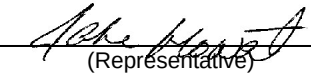
Manufactured by Eaton Metal Products Company LLC Plant #3, 669 West Quinn Road Building #16, Pocatello, Idaho, 83201
Manufacturer's Serial No. 282 CRN N/A National Board No. 274

CERTIFICATE OF SHOP/FIELD COMPLIANCE

We certify that the statements made in this report are correct and that all details of design, material, construction, and workmanship of this vessel conform to the ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1. "U" Certificate of Authorization Number 32962

expires December 13, 2019

Date 07/25/2019 Co. name Eaton Metal Products Company LLC Plant #3
(Manufacturer)

Signed 
(Representative)

CERTIFICATE OF SHOP/FIELD INSPECTION

Vessel constructed by Eaton Metal Products Company LLC Plant #3 at 669 West Quinn Road Building #16, Pocatello, Idaho, 83201

I, the undersigned, holding a valid commission issued by The National Board of Boiler and Pressure Vessel Inspectors and employed by The Hartford Steam Boiler Inspection and Insurance Company, of Hartford, CT

have inspected the component described in this Manufacturer's Data Report on July 25, 2019, and state that, to the best of my knowledge and belief, the Manufacturer has constructed this pressure vessel in accordance with ASME BOILER AND PRESSURE VESSEL CODE, Section VIII, Division 1. By signing this certificate neither the Inspector nor his/her employer makes any warranty, expressed or implied, concerning the pressure vessel described in this Manufacturer's Data Report. Furthermore, neither the Inspector nor his/her employer shall be liable in any manner for any personal injury or property damage or a loss of any kind arising from or connected with this inspection.

Date 07/25/2019 Signed 
(Authorized Inspector)

Commissions 14735, UTS0635
(National Board Authorized Inspector Commission number)

5361-1

FORM U-4 MANUFACTURER'S DATA REPORT SUPPLEMENTARY SHEET

Job #

As Required by the Provisions of the ASME Boiler and Pressure Vessel Code Rules, Section VIII, Division 1

282

**Corrected
Copy**

Serial #

1. Manufactured and certified by Eaton Metal Products Company LLC Plant #3, 669 West Quinn Road Building #16, Pocatello, Idaho, 83201
(Name and address of Manufacturer)

2. Manufactured for ANADARKO E&P ONSHORE LLC, UNKOWN, Colorado
(Name and address of Purchaser)

3. Location of installation Johnstown Compressor Station, Colorado
(Name and address)

4. Type Horizontal N/A 282
(Horizontal, vertical, or sphere) (Tank, separator, heat exch., etc.) (Manufacturer's serial number)

N/A
(CRN)

D-5361-1
(Drawing number)

274
(National Board number)

2019
(Year built)

Data Report

Item Number

Remarks

Additional nozzles, inspection and safety valve openings:

Purpose (Inlet, Outlet, Drain, etc.)	No.	Diameter or Size	Type	Material		Nozzle Thickness		Reinforcement Material	Attachment Details		Location (Insp. Open.)
				Nozzle	Flange	Nom.	Corr.		Nozzle	Flange	
Boot Interface	1	3	RF150LWN	SA-105		.6	0	Inherent	UW-16.1 (d)		

Certificate of Authorization: Type "U"No. 32962Expires December 13, 2019Date 07/25/2019

Name

Eaton Metal Products Company LLC Plant #3
(Manufacturer)

Signed

(Representative)

Date 07/25/2019

Name

[Signature]
(Authorized Inspector)

Commissions

14735, UTS0635

(National Board Authorized Inspector Commission number)

NB 274

CERTIFIED BY



EATON METAL PRODUCTS COMPANY LLC, PLANT #3



RT-4

250

psig at

125

°F

MAWP

N/A

psig at

N/A

°F

-20

°F at

250

MDMT

282

2019

Serial Number

Year

EMP JOB 5361-S01

Anadarko E&P Onshore LLC

132" OD x 82'-10" S/S Inlet Slug Catcher

Shell thickness: 0.875"

C.A. = 0"

Vessel Tag # V-1000

P.O. # 4500100246

Head thickness: 0.85" min.

Hydro tested at 325 psig

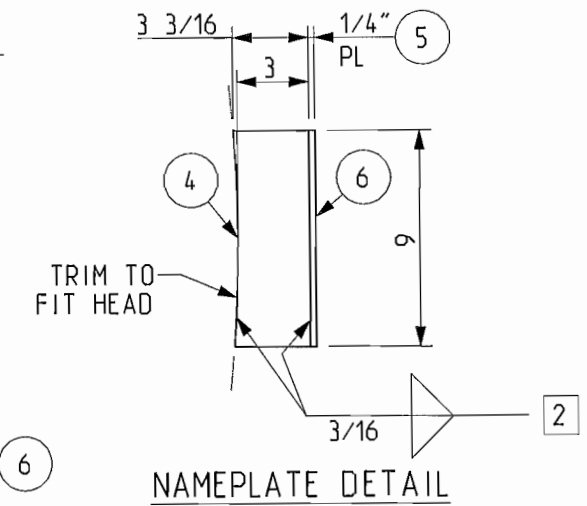
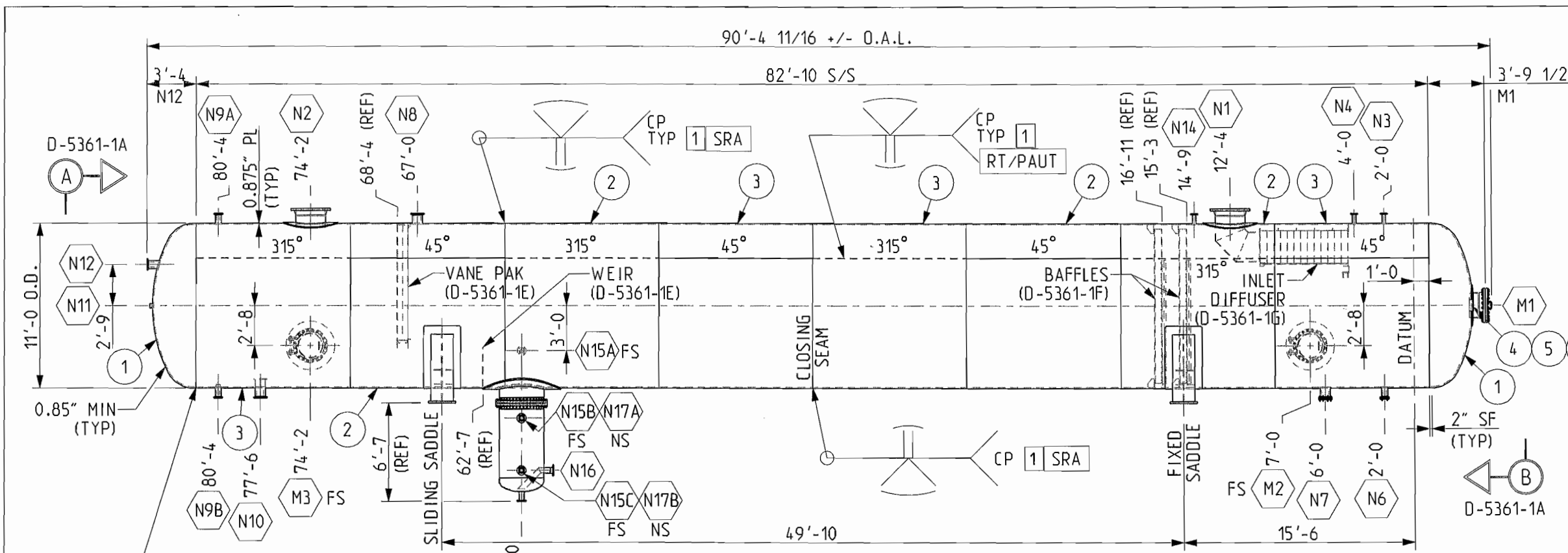


Eaton Metal Products Company LLC

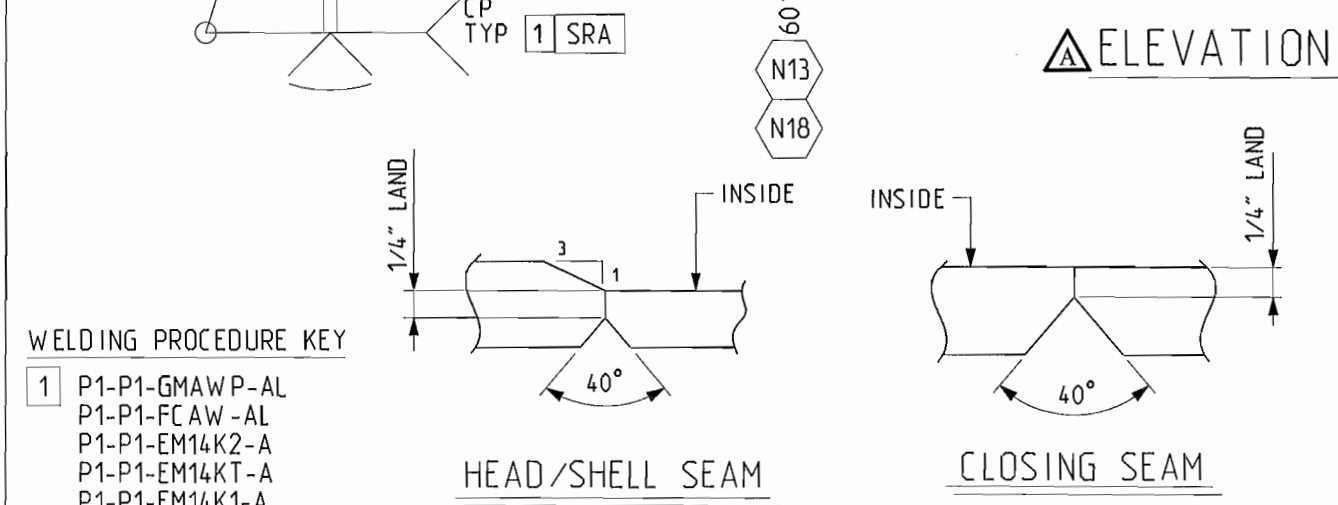
ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736

Fabrication Drawings



SHOP NOTE: ALL INTERNAL WELDS MUST BE SUITABLY PREPPED FOR INTERNAL LINING. ALL SHARP EDGES & ROUGH WELD CONTOURS ARE TO BE ROUNDED/SMOOTHED OUT. POROSITY & WELD SPATTER SHALL BE REMOVED.



NOTE: ALL DIMENSIONS ARE TAKEN FROM DATUM WHICH IS LOCATED 12" TO THE LEFT OF RIGHT H/S SEAM

CONSTRUCTION : ALL WELDED ASME CODE SECTION VIII DIV. 1				2017 EDITION	
INSPECTED BY : HSB CT					
STAMP REQ'D: YES		SERIAL NO.: LATER		NAT'L BOARD NO.: LATER	
INT DESIGN PRESS:		250	PSIG	INT DESIGN TEMP: 125 °F	
EXT DESIGN PRESS:		N/A	PSIG	EXT DESIGN TEMP: N/A °F	
OPERATING PRESS:		130	PSIG	OPERATING TEMP: 60 °F	
MINIMUM DESIGN METAL TEMP:				-20 °F	
RADIOGRAPHY: LONG SEAMS: FULL / GIRTH SEAMS: SPOT PER UW-11(a)(5)(b)					
COMPONENT EFFICIENCY:		HEAD: 1.00		SHELL: 1.00	
CORROSION ALLOWANCE:		HEAD: NONE		SHELL: NONE	
				NOZZLES: NONE	

STRESS RELIEVE: NO		INTERNAL COATING PER 5361-PS1	
HYDRO TEST PRESS: 325 PSIG @ 40°F		SURF PREP: COATING:	
HOLD FOR 1 HOUR			
EST SHIP WGT: 138000 LBS			
EST OPER WGT: LBS			
EST TEST WGT: 639000 LBS		EXTERNAL COATING PER 5361-PS1	
INSULATION THK: 2"		SURF PREP: COATING:	
SPECIFIC GRAVITY: 1.00			
EST CAPACITY: 60000 GALS			

DESIGN DATA

APPROVED FOR CONSTRUCTION
DATE 11/8/18 BY [Signature]

NDE KEY
SRA SPOT RT OR PAUT REQUIRED ON EVERY GIRTH SEAM
RT/PAUT WELD TO BE 100% EXAMINED BY RT OR PHASED ARRAY UT

SEE DWG D-5361-1A FOR END VIEWS
SEE DWG D-5361-1B FOR SADDLE DETAILS
SEE DWG D-5361-1C FOR MANWAY M1 DETAILS
SEE DWG D-5361-1D & -1DA FOR NOZZLE DETAILS
SEE DWG D-5361-1E FOR VANE PAK & WEIR DETAILS
SEE DWG D-5361-1F & -1FA FOR BAFFLE DETAILS
SEE DWG D-5361-1G & -1GA FOR INLET DIFFUSER DETAILS
SEE DWG D-5361-1H FOR BOOT DETAILS
SEE DWG D-5361-1J FOR MANWAY M2 & M3 DETAILS

BILL OF MATERIAL

Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
ONE	V-1000		VESSEL	132" OD INLET SLUG CATCHER							
	5361-1-1	2	HEAD	0.85" MIN x 132" OD ASME 2:1 SF=2"				SA-516-70		X	11263
	5361-1-2	4	PLATE	0.875" SHELL, ROLLED	0.875	124.25	411.938	SA-516-70		X	50805
	5361-1-3	4	PLATE	0.875" SHELL, ROLLED	0.875	124.25	411.938	SA-516-70		X	50805
	5361-1-4	1	PLATE	1/4" PLATE SK	0.250	3.188	9	A-36		X	2
	5361-1-5	1	PLATE	1/4" PLATE	0.250	6	9	A-36			4
	5361-1-6	1	NAMEPL	ASME NAMEPLATE (EMP STD)				STN STL			-

Nozzle	Qty	Size	Rating	Face Flange	Type	Service	Remarks
M3	1	20"	150#	RF	WN	MANWAY	w/ HINGE
M2	1	20"	150#	RF	WN	MANWAY	w/ HINGE
M1	1	20"	150#	RF	WN	MANWAY	w/ HINGE
N18	1	3"	150#	RF	LWN	DRAIN (IN BOOT)	
N17A/B	2	3"	150#	RF	LWN	SPARE LEVEL (IN BOOT)	
N16	1	4"	150#	RF	WN	WATER OUTLET (IN BOOT)	w/ INT PIPE
N15B/C	2	3"	150#	RF	LWN	LEVEL GAUGE (IN BOOT)	
N15A	1	3"	150#	RF	WN	LEVEL (BOOT INTERFACE)	
N14	1	2"	150#	RF	LWN	HP DRAIN RECYCLE	
N13	1	36"	150#	RF	WN	BOOT	SERIES "B"
N12	1	4"	150#	RF	LWN	LAHH	
N11	1	2"	6000#	FNPT	CPLG	SPARE	
N10	1	6"	150#	RF	LWN	LIQUID OUTLET (OIL)	w/ V.B.
N9A/B	2	3"	150#	RF	LWN	BRIDLE	w/ STINGER (N9B)
N8	1	6"	150#	RF	LWN	PSV	
N7	1	6"	150#	RF	LWN	DRAIN	w/ BLIND
N6	1	3"	150#	RF	LWN	DRAIN	w/ BLIND
N4	1	2"	150#	RF	LWN	PUMP RECYCLE	
N3	1	2"	150#	RF	LWN	VRU RECYCLE	
N2	1	24"	150#	RF	WN	OUTLET	
N1	1	24"	150#	RF	WN	INLET	w/ DIFFUSER

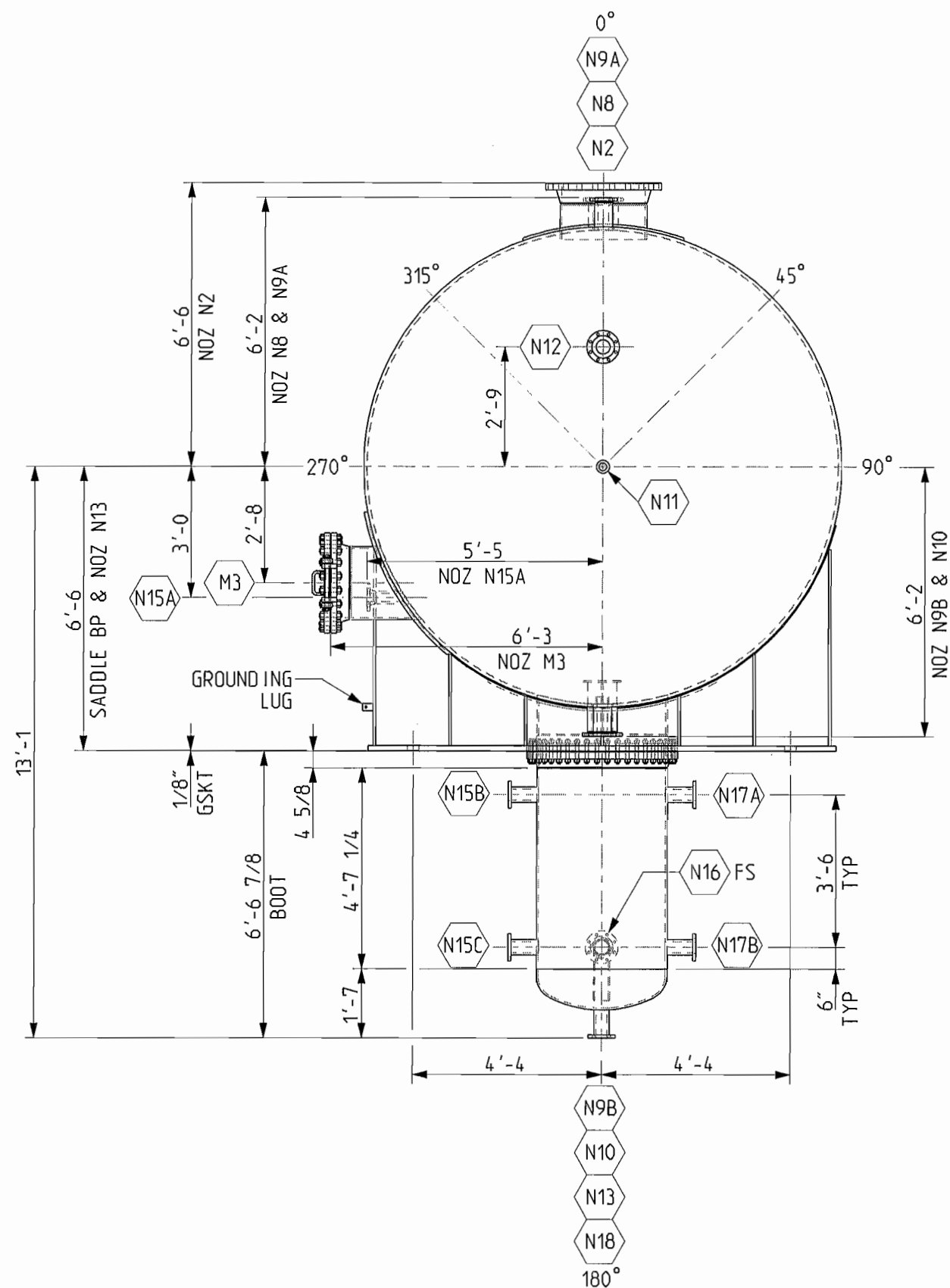
NOZZLE SCHEDULE

REVISIONS

No.	Date	By	Chk'd	Revision Description
A	10/23/18	RT	[Signature]	REVISED PER CUSTOMER MARK-UPS

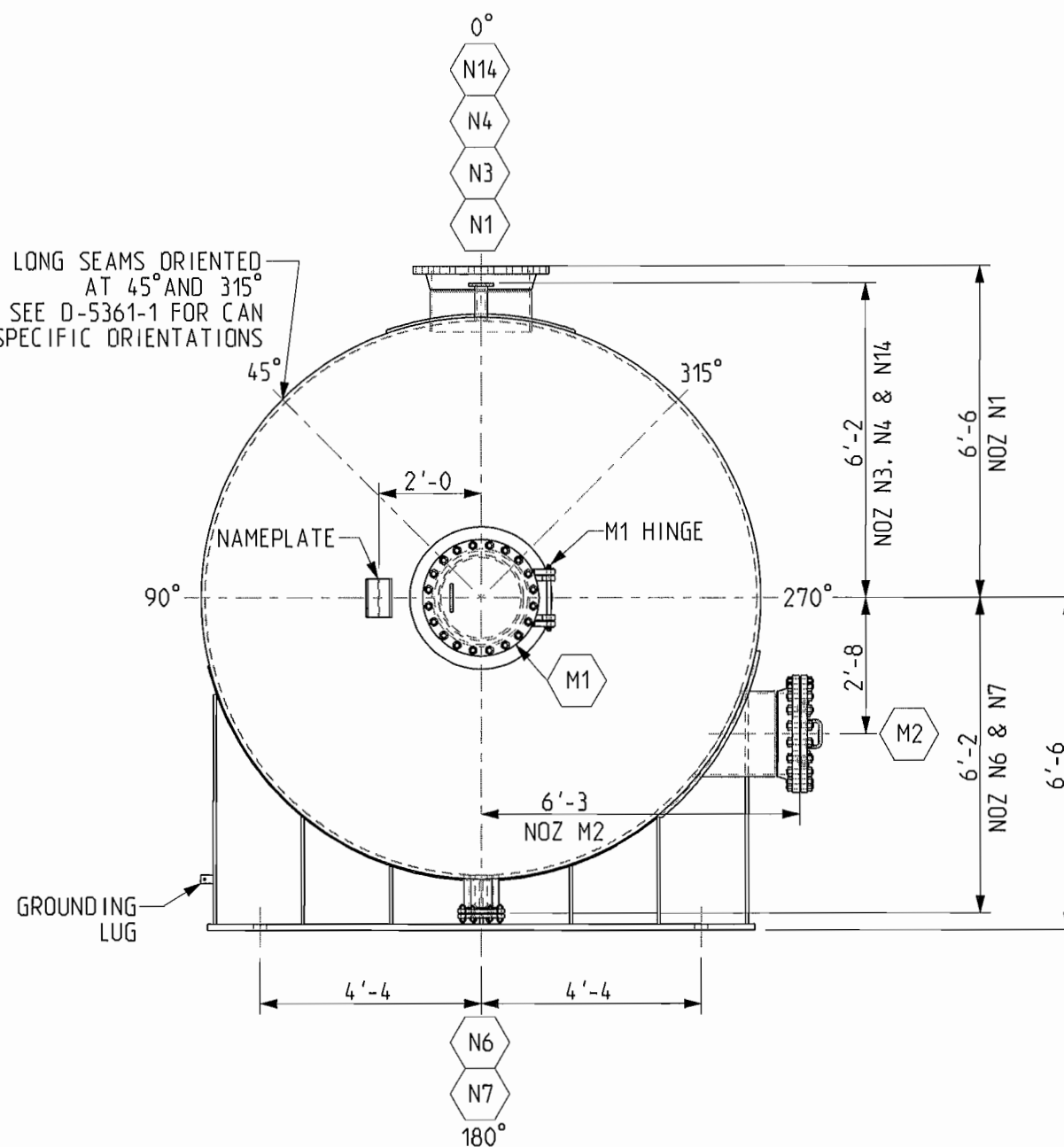
EATON METAL PRODUCTS CO LLC
DENVER - SALT LAKE CITY

GENERAL ARRANGEMENT
132" OD x 82'-10" S/S INLET SLUG CATCHER
P.O. # 4500100246 - TAG # V-1000
Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
Cust: ANADARKO E&P ONSHORE LLC
EMP 5361-S01 Dwg. D-5361-1 Job No. A



LEFT END VIEW (A)
D-5361-1

LONG SEAMS ORIENTED
AT 45° AND 315°
SEE D-5361-1 FOR CAN
SPECIFIC ORIENTATIONS

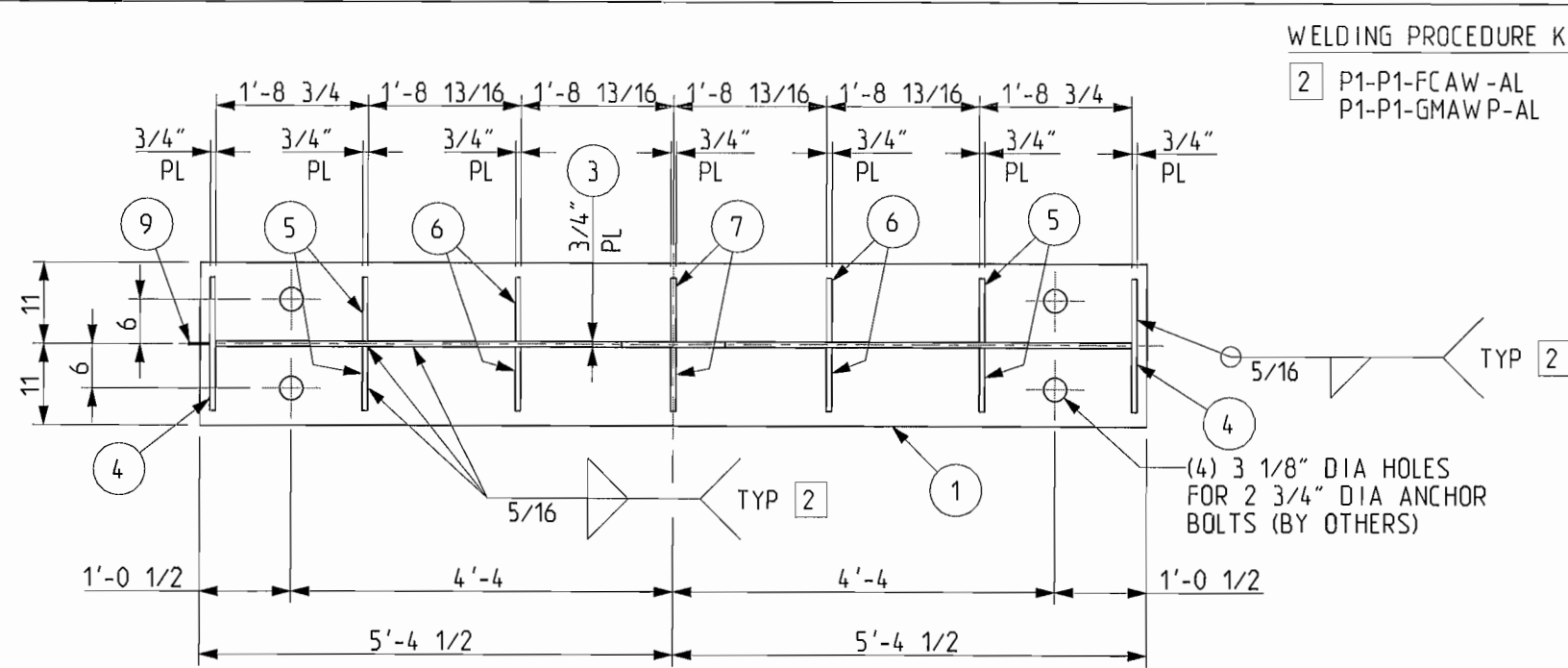


RIGHT END VIEW (B)
D-5361-1

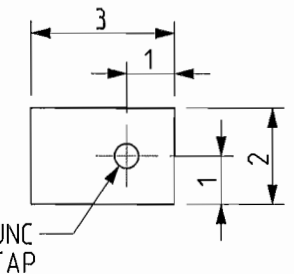
APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY DB

A 10/23/18 RT				ADDED BLIND FLANGES TO NOZZLES N6 & N7	
No.	Date	By	Chk'd	Revision Description	
EATON				EATON METAL PRODUCTS CO LLC	
				DENVER -- SALT LAKE CITY	
				END VIEWS	
				132" OD x 82'-10" S/S INLET SLUG CATCHER	
				P.O. # 4500100246 - TAG # V-1000	
				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO	
				Cust: ANADARKO E&P ONSHORE LLC	
				EMP	
				Dwg. No. 5361-S01	
				Rev. No. D-5361-1A	
				A	

WORK THIS DWG WITH D-5361-1



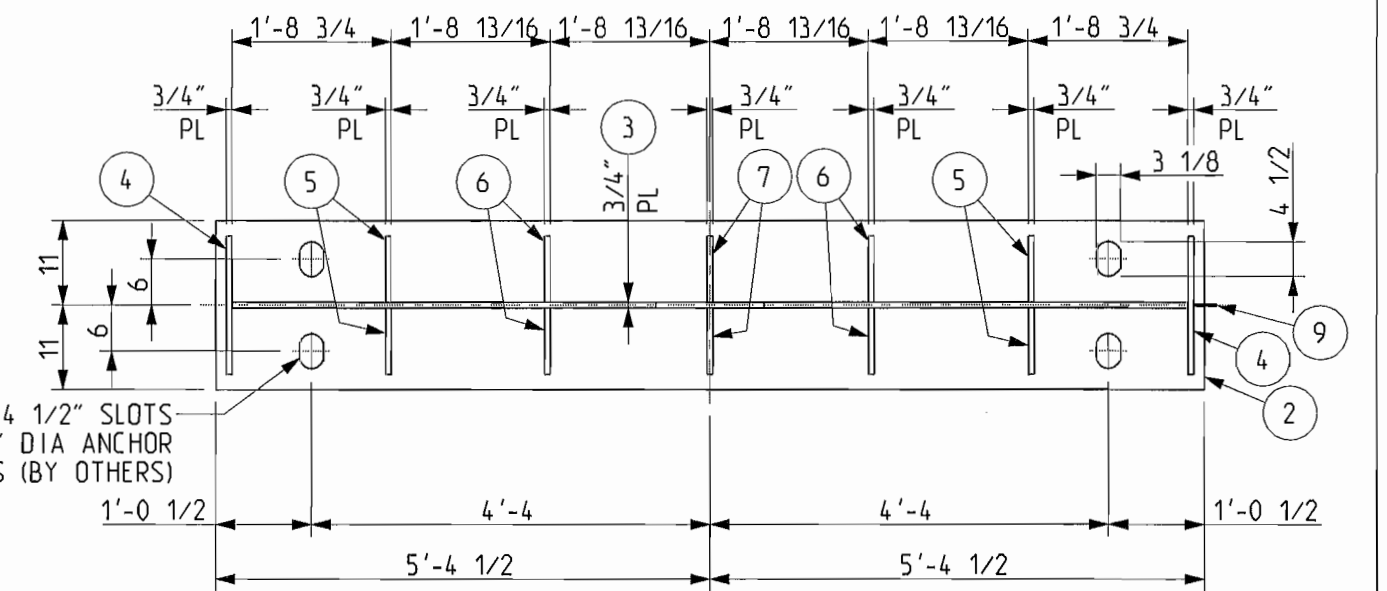
SADDLE BASE PLAN - FIXED END



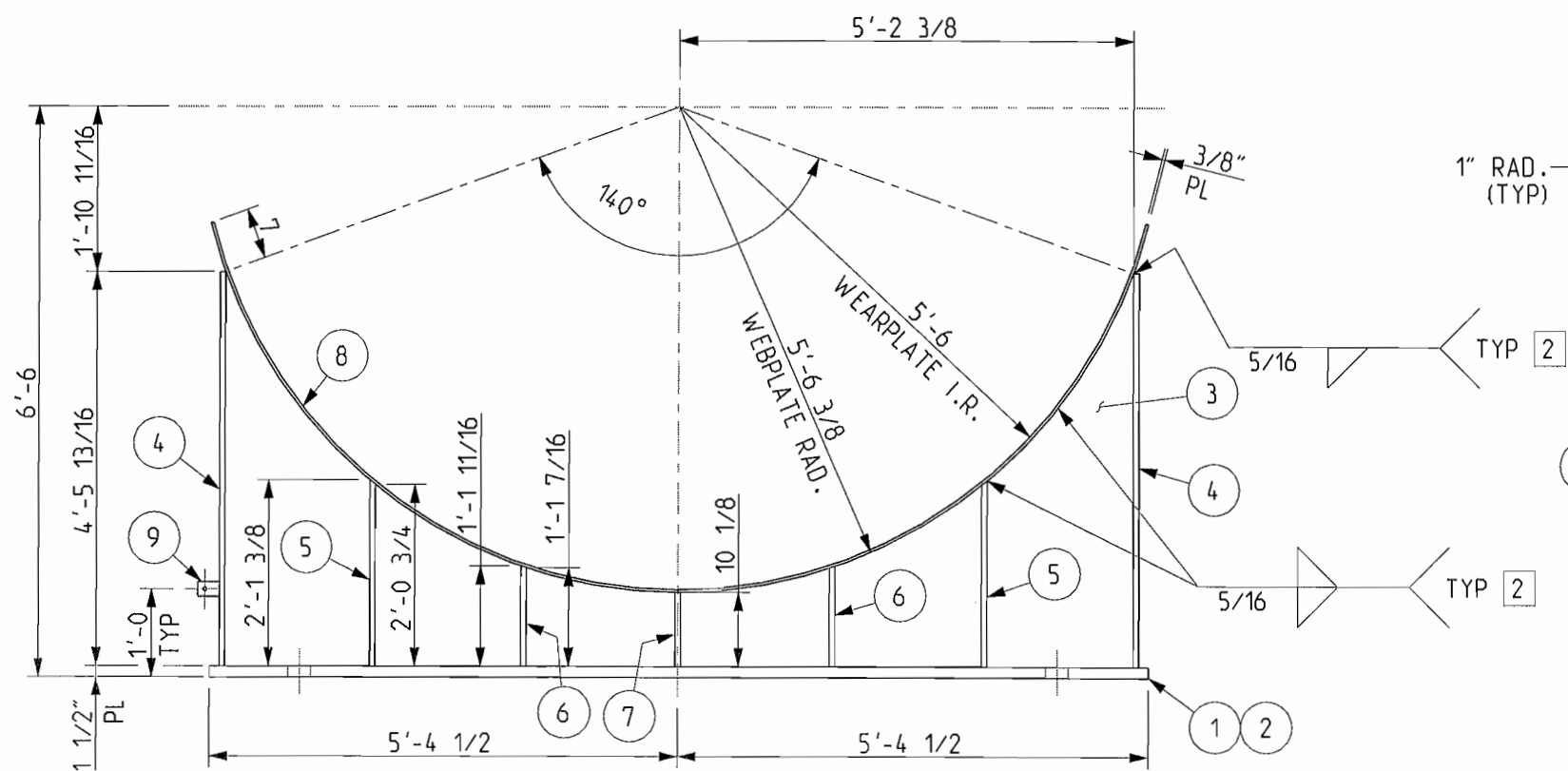
DETAIL 9

WELDING PROCEDURE KEY
 2 P1-P1-FCAW-AL
 P1-P1-GMAWP-AL

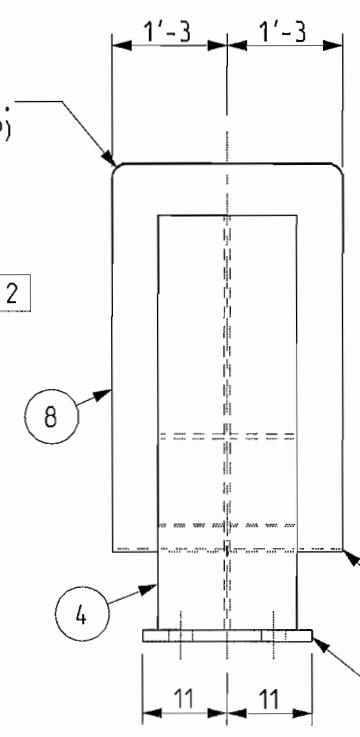
Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
	5361-1B-1	1	PLATE	1-1/2" BASEPLATE W/ HOLES	1.500	22	129	A-36			1194
	5361-1B-2	1	PLATE	1-1/2" BASEPLATE W/ SLOTS	1.500	22	129	A-36			1187
	5361-1B-3	2	PLATE	3/4" WEB PLATE SKETCH	0.750	53.813	124.75	A-36			1168
	5361-1B-4	4	PLATE	3/4" END PLATE	0.750	18	53.813	A-36			824
	5361-1B-5	8	PLATE	3/4" RIB PLATE	0.750	8.625	25.375	A-36			368
	5361-1B-6	8	PLATE	3/4" RIB PLATE	0.750	8.625	13.688	A-36			199
	5361-1B-7	4	PLATE	3/4" RIB PLATE	0.750	8.625	10.125	A-36			74
	5361-1B-8	2	PLATE	3/8" WEAR PLATE, ROLL	0.375	30	175.688	SA-516-70		X	1121
	5361-1B-9	2	PLATE	1/4" PLATE W/HOLE	0.250	2	3	A-36			-



SADDLE BASE PLAN - SLIDING END
 SEE FIXED END FOR WELDING DETAILS



SADDLE ELEVATION



END VIEW

WORK THIS DWG WITH D-5361-1 & -1A

- NOTES:
1. VESSEL TO BE LEVELED & PROPERLY SHIMMED UNDER BOTH BASEPLATES.
 2. ENTIRE BASEPLATE TO BE GROUTED USING HIGH QUALITY NON-SHRINK GROUT TO PROVIDE UNIFORM SUPPORT UNDER ENTIRE BASE. GROUT TO BE INSTALLED IN ACCORDANCE WITH GROUT MANUFACTURER'S INSTRUCTIONS.
 3. GROUT MUST BE FULLY CURED PRIOR TO LOADING VESSEL WITH CONTENTS.
 4. ADEQUATE SHIM AREA MUST BE PROVIDED TO KEEP CONCRETE STRESSES UNDER SHIMS BELOW THE ALLOWABLE PRIOR TO GROUTING.

APPROVED
 FOR CONSTRUCTION
 DATE 11/8/18 BY DB

No.	Date	By	Chk'd	Revision	Description
				1	EATON METAL PRODUCTS CO LLC
				2	DENVER -- SALT LAKE CITY
				3	SADDLE DETAILS
				4	132" OD x 82'-10" S/S INLET SLUG CATCHER
				5	P.O. # 4500100246 - TAG # V-1000
				6	Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
				7	Cust: ANADARKO E&P ONSHORE LLC
				8	EMP
				9	Job No. 5361-S01
				10	Dwg. No. D-5361-1B

SHOP NOTE: ALL INTERNAL WELDS MUST BE SUITABLY PREPPED FOR INTERNAL LINING. ALL SHARP EDGES & ROUGH WELD CONTOURS ARE TO BE ROUNDED/SMOOTHED OUT. POROSITY & WELD SPATTER SHALL BE REMOVED.

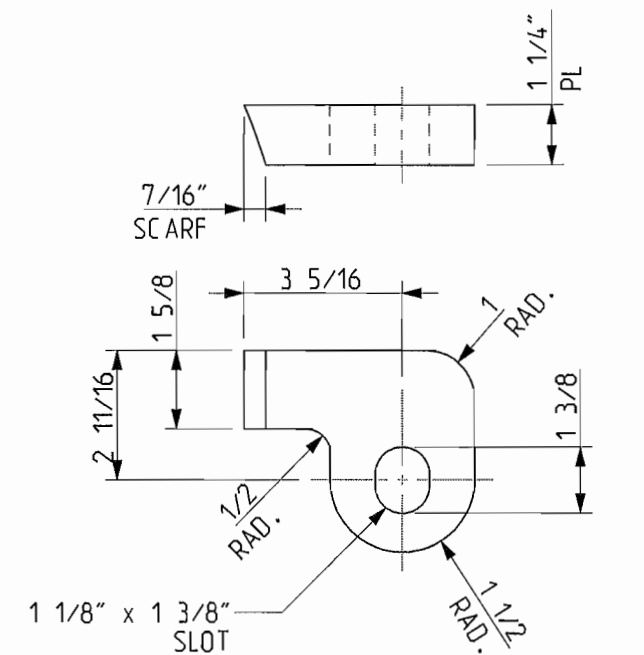
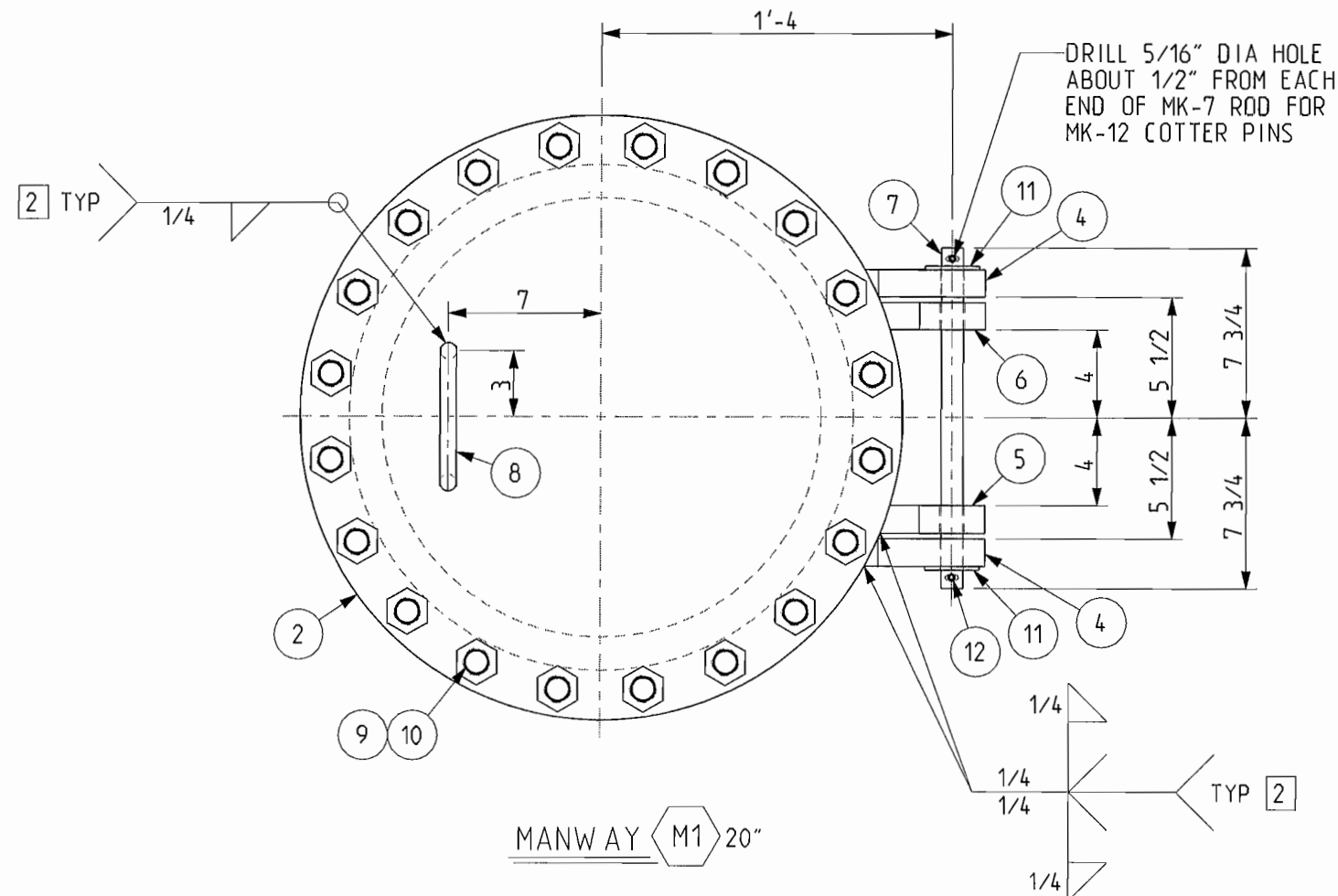
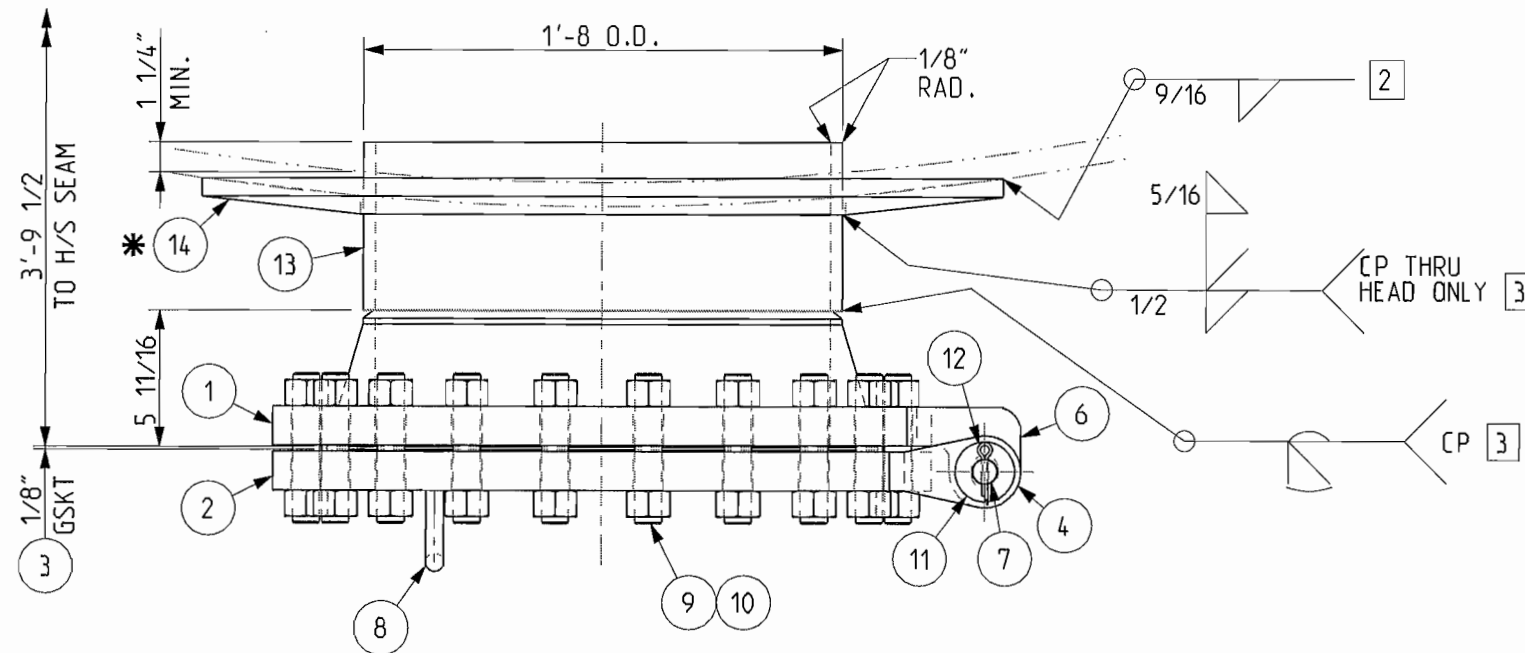
* REPAD NOTE:
1/4" NPT TELL-TALE HOLE
LOCATED AT LOWEST POINT
WHEN INSTALLED

WELDING PROCEDURE KEY

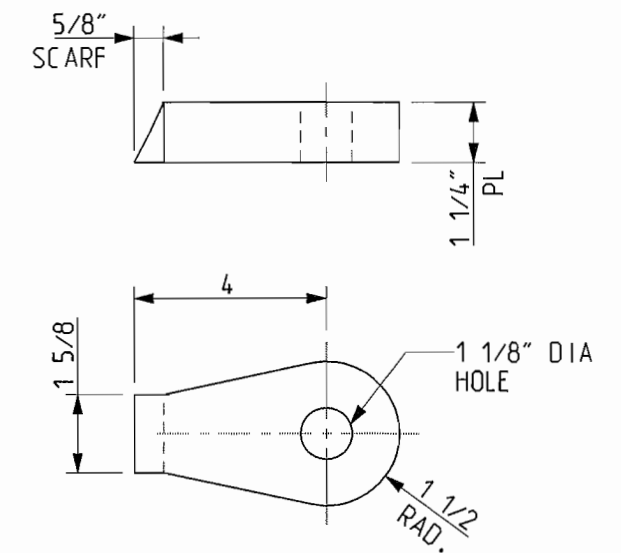
- 2 P1-P1-FCAW-AL
P1-P1-GMAWP-AL
- 3 P1-P1-GMAWP-AL
P1-P1-FCAW-AL
P1-P1-EM14K1-A

BILL OF MATERIAL

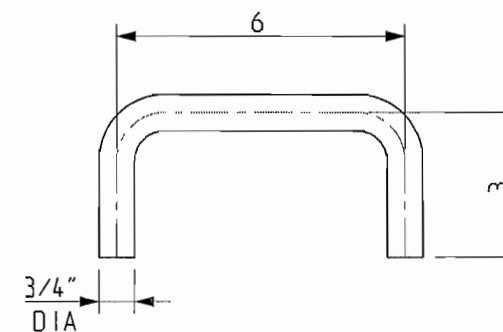
Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
	5361-1C-1	1	FLANGE	20" - 150# RFWN XH BORE				SA-105		X	199
	5361-1C-2	1	FLANGE	20" - 150# RF BLIND				SA-105		X	271
	5361-1C-3	1	GASKET	1/8" - 20" - 150# RING TYPE KLINGERSIL				KLINGERSIL			1
	5361-1C-4	2	PLATE	1-1/4" SKETCH PL W/ HOLE	1.250	3	5.5	A-36		X	8
	5361-1C-5	1	PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	5
	5361-1C-6	1	PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	5
	5361-1C-7	1	ROD	1" DIA ROD W/ HOLES			15.5	A-36			3
	5361-1C-8	1	ROD	3/4" DIA ROD, BEND			12	A-36		X	1
	5361-1C-9	20	STUD	1-1/8" DIA FULL THREAD			6.25	SA-193-B7			35
	5361-1C-10	40	NUT	1-1/8" HEAVY HEX				SA-194-2H			23
	5361-1C-11	2	WASHER	1" STANDARD ROUND				STEEL			-
	5361-1C-12	2	COTTER	1/4" DIA COTTER PIN			1.5	STEEL			-
	5361-1C-13	1	PIPE	20" NOM XH	0.500		8	SA-106-B		X	69
	5361-1C-14	1	PLATE	3/4" CIRC PL 20.25" ID x 33.5" DD	0.750	SHOP TO FORM		SA-516-70		X	119



DETAIL 5 (AS SHOWN)
DETAIL 6 (OPP HAND)



DETAIL 4

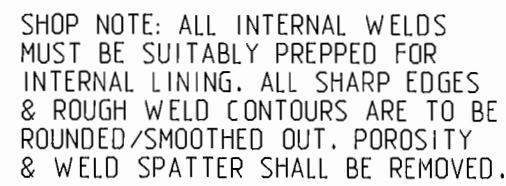
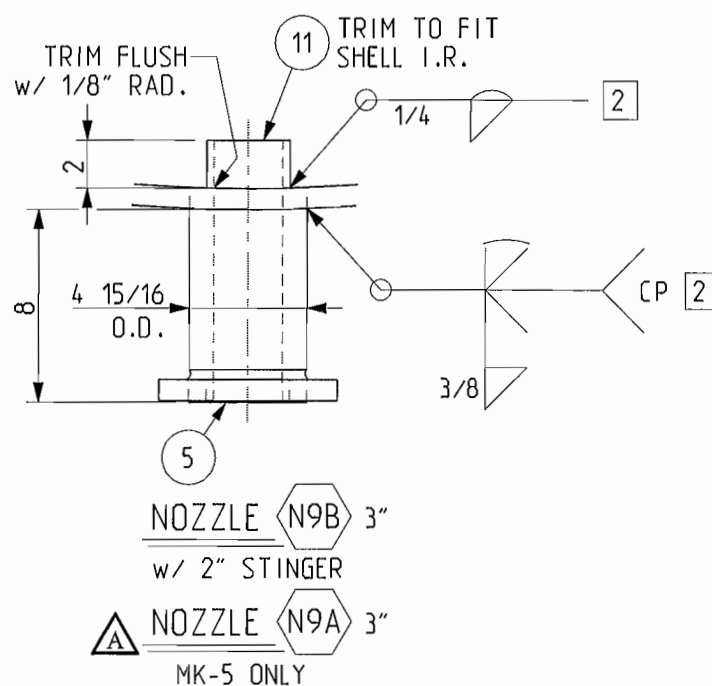


DETAIL 8



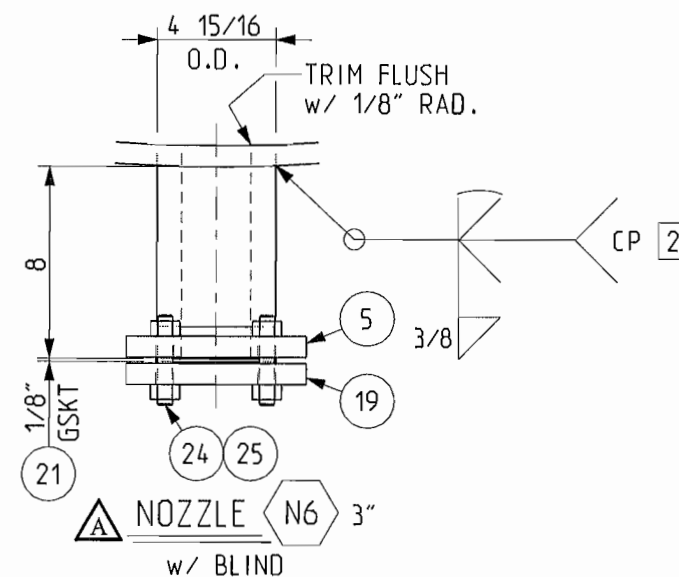
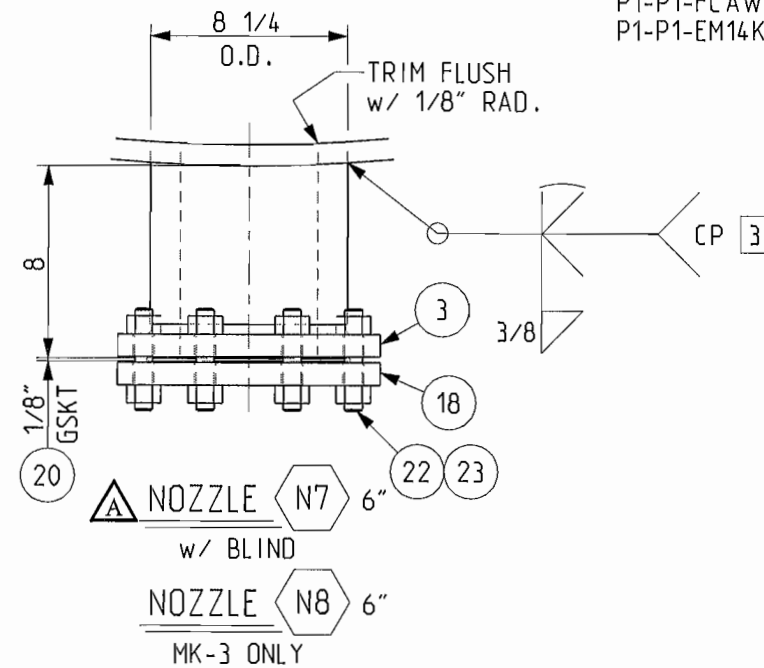
No.	Date	By	Chk'd	Revision Description
				EATON METAL PRODUCTS CO LLC
				DENVER -- SALT LAKE CITY
				MANWAY M1 DETAILS
				132" OD x 82'-10" S/S INLET SLUG CATCHER
				P.O. # 4500100246 - TAG # V-1000
				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
				Cust: ANADARKO E&P ONSHORE LLC
				EMP 5361-S01 Dwg. No. D-5361-1C
				Rev

WORK THIS DWG WITH D-5361-1 & -1A



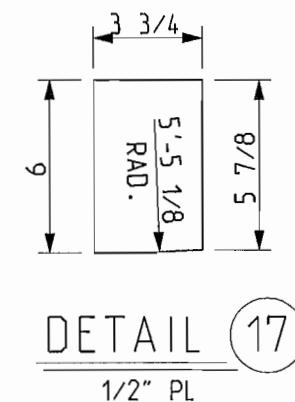
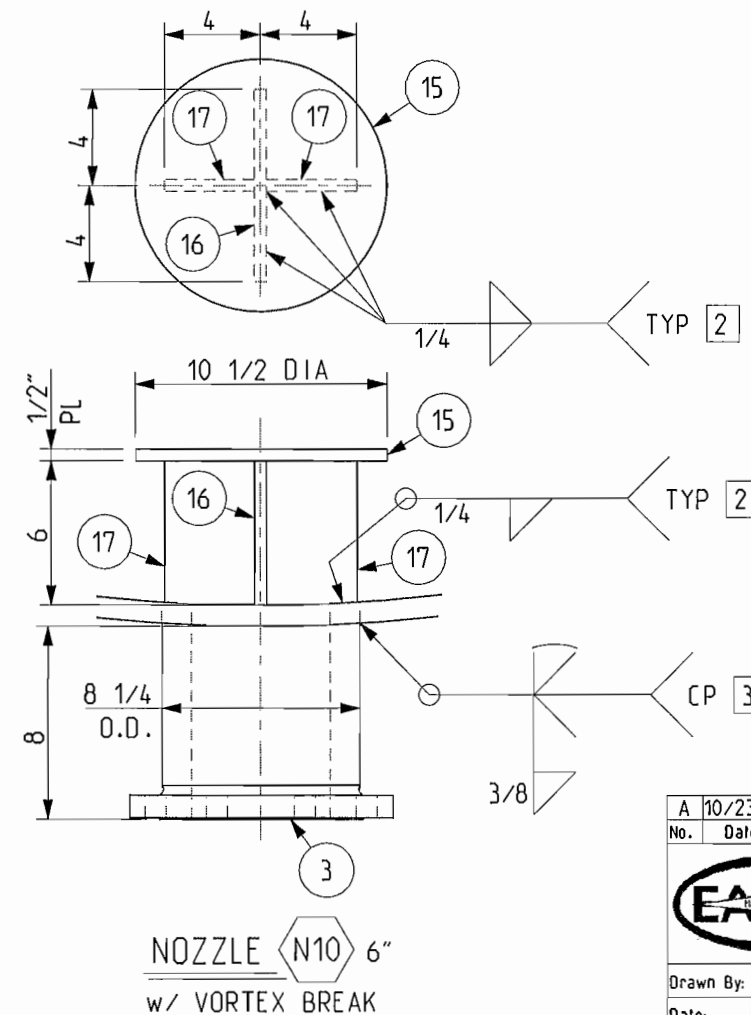
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P1-P1-GMAW P-AL

3 P1-P1-GMAW P-AL
P1-P1-FC AW -AL
P1-P1-EM14K1-A



* REPAD NOTE:
1/4" NPT TELL-TALE HOLE
LOCATED AT LOWEST POINT
WHEN INSTALLED

Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
	5361-10-1	1	FLANGE	36" - 150# SERIES "B" RFWN XH BORE (35" I.D.)				SA-105		X	270
	5361-10-2	2	FLANGE	24" - 150# RFWN XH BORE				SA-105		X	542
	5361-10-3	3	FLANGE	6" - 150# RF HB LWN NS			9	SA-105		X	239
	5361-10-4	1	FLANGE	4" - 150# RF HB LWN NS			12.25	SA-105		X	80
	5361-10-5	3	FLANGE	3" - 150# RF HB LWN NS			9	SA-105		X	114
	5361-10-6	1	FLANGE	3" - 150# RFWN XXH BORE				SA-105		X	13
	5361-10-7	3	FLANGE	2" - 150# RF LWN			9	SA-105		X	44
	5361-10-8	1	COUPLING	2" - 6000# FULL SCRD			3.375	SA-105		X	8
	5361-10-9	2	PIPE	24" NOM XH	0.500		9.5	SA-106-B		X	199
	5361-10-10	1	PIPE	3" NOM XXH	0.600		10	SA-106-B		X	16
	5361-10-11	1	PIPE	3" NOM XH, SKETCH	0.300		2	SA-106-B		X	2
	5361-10-12	1	PLATE	1/2" PLATE, ROLLED w/4" TANS	0.500	10.938	119.5	SA-516-70		X	173
	5361-10-13	1	PLATE	CIRC 36.25 ID x 63 OD ROLL	1.000			SA-516-70		X	616
	5361-10-14	2	PLATE	CIRC 24.25 ID x 44.5 OD ROLL	0.750			SA-516-70		X	474
	5361-10-15	1	PLATE	PLATE CIRC 10.50" DIA	0.500			A-36			12
	5361-10-16	1	PLATE	1/2" PLATE (VORTEX BRK)	0.500	6	8	SA-516-70		X	7
	5361-10-17	2	PLATE	1/2" SKETCH PL (VORTEX BRK)	0.500	3.75	6	SA-516-70		X	6
	5361-10-18	1	FLANGE	6" - 150# RF BLIND				SA-105		X	25
	5361-10-19	1	FLANGE	3" - 150# RF BLIND				SA-105		X	11
	5361-10-20	1	GASKET	1/8" - 6" - 150#, RING TYPE, C-4401				KLINGERSIL			1
	5361-10-21	1	GASKET	1/8" - 3" - 150#, RING TYPE, C-4401				KLINGERSIL			-
	5361-10-22	8	STUD	3/4" DIA, FULL THREAD			4.25	SA-193-B7			4
	5361-10-23	16	NUT	3/4" HEAVY HEX				SA-194-2H			3
	5361-10-24	4	STUD	5/8" DIA, FULL THREAD			3.75	SA-193-B7			1
	5361-10-25	8	NUT	5/8" HEAVY HEX				SA-194-2H			-



APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY DB

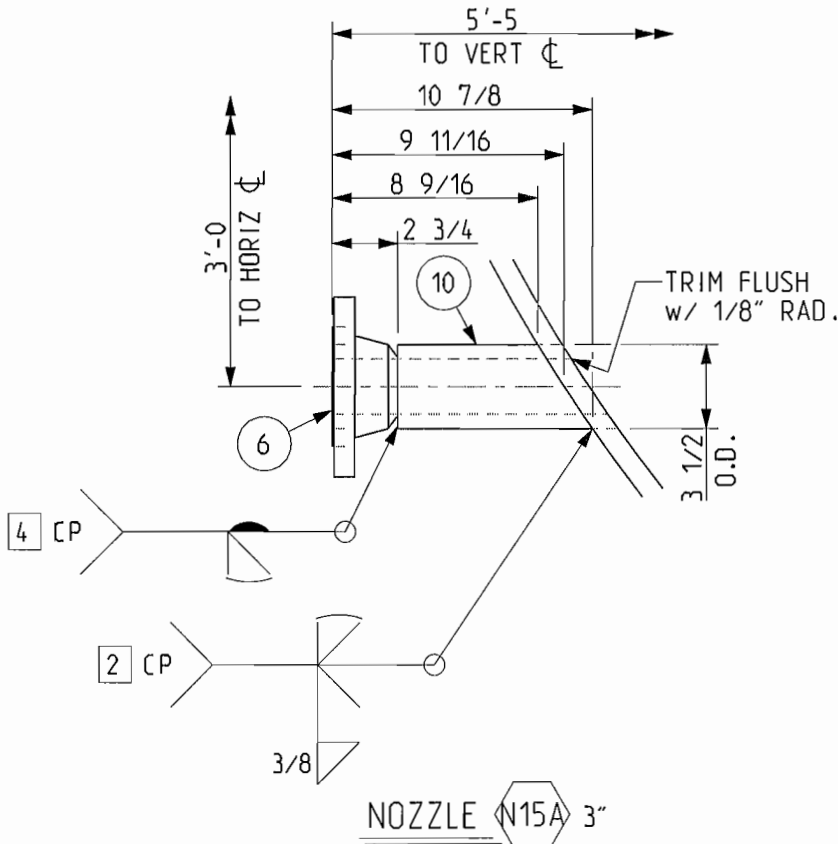
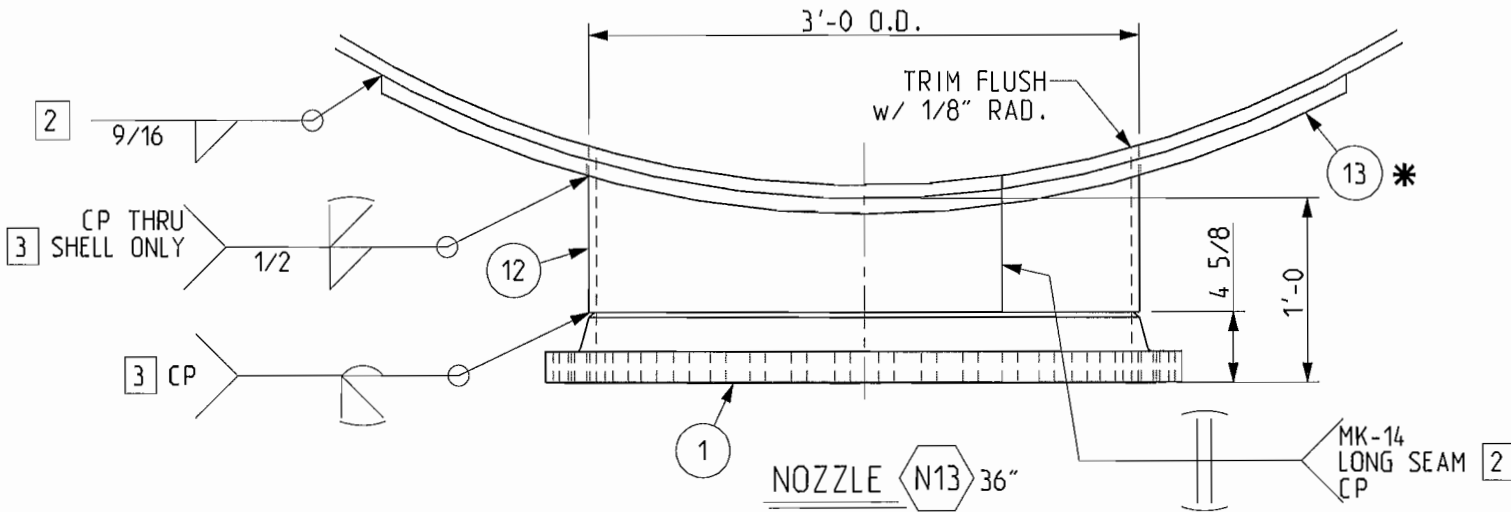
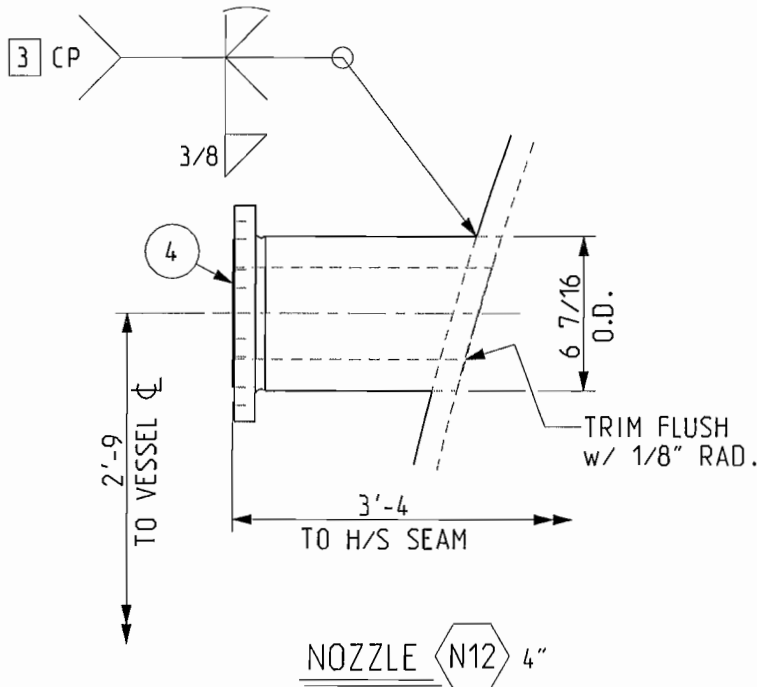
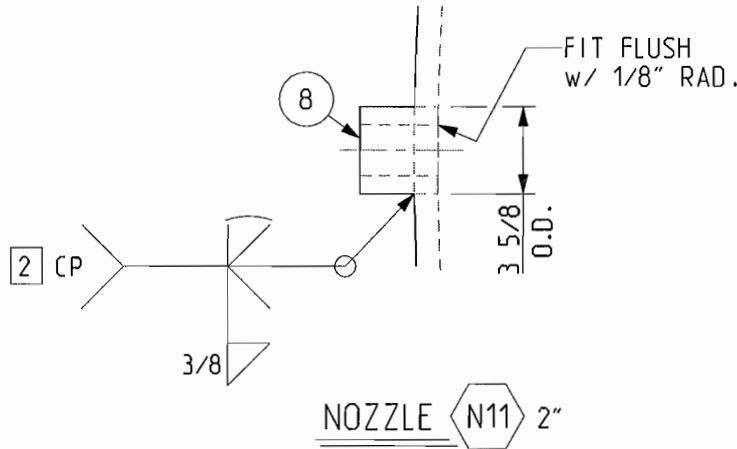
A	10/23/18	RT	25	ADDED BLIND FLANGES TO NOZZLES N6 & N7	
No.	Date	By	Chk'd	Revision Description	
				EATON METAL PRODUCTS CO LLC DENVER -- SALT LAKE CITY	
				NOZZLE DETAILS	
Drawn By:				RT	
Date:				9/18/2018	
Chk'd By:				DB	
Date:				10/5/18	
				132" OD x 82"-10" S/S INLET SLUG CATCHER	
				P.O. # 4500100246 - TAG # V-1000	
				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO	
				Cust: ANADARKO E&P ONSHORE LLC	
				EMP	REV
Inh. No.				5361-S01	0
				No.	D-5361-1D
					A

WORK THIS DWG WITH D-5361-1, -1A & -1DA

WELDING PROCEDURE KEY

- 2 P1-P1-FC AW -AL
P1-P1-GMAWP-AL
- 3 P1-P1-GMAWP-AL
P1-P1-FC AW -AL
P1-P1-EM14K1-A
- 4 P1-P1-FC AW -AL
P1-P1-GTAW -AL
P1-P1-GMAWP-AL
P1-P1-GMAWP-STT-A

* REPAD NOTE:
1/4" NPT TELL-TALE HOLE
LOCATED AT LOWEST POINT
WHEN INSTALLED



SHOP NOTE: ALL INTERNAL WELDS MUST BE
SUITABLY PREPPED FOR INTERNAL LINING.
ALL SHARP EDGES & ROUGH WELD CONTOURS
ARE TO BE ROUNDED/SMOOTHED OUT.
POROSITY & WELD SPATTER SHALL BE REMOVED.

APPROVED
FOR CONSTRUCTION
DATE 11/13/18 BY [Signature]

No.	Date	By	Chk'd	Revision	Description
				EATON METAL PRODUCTS CO LLC DENVER -- SALT LAKE CITY	
Drawn By: RT				NOZZLE DETAILS	
Date: 9/18/2018				132" OD x 82'-10" S/S INLET SLUG CATCHER	
Chk'd By: DB				P.O. # 4500100246 - TAG # V-1000	
Date: 10/5/18				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO	
				Cust: ANADARKO E&P ONSHORE LLC	
				EMP Job No. 5361-S01	
				Dwg No. D-5361-1DA	

WORK THIS DWG WITH D-5361-1, -1A & -1D

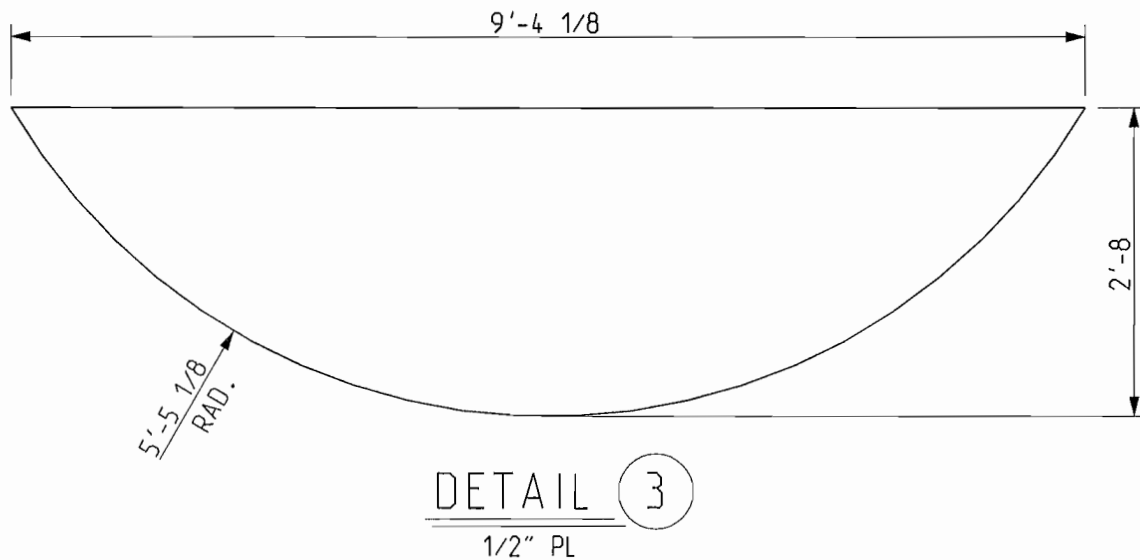
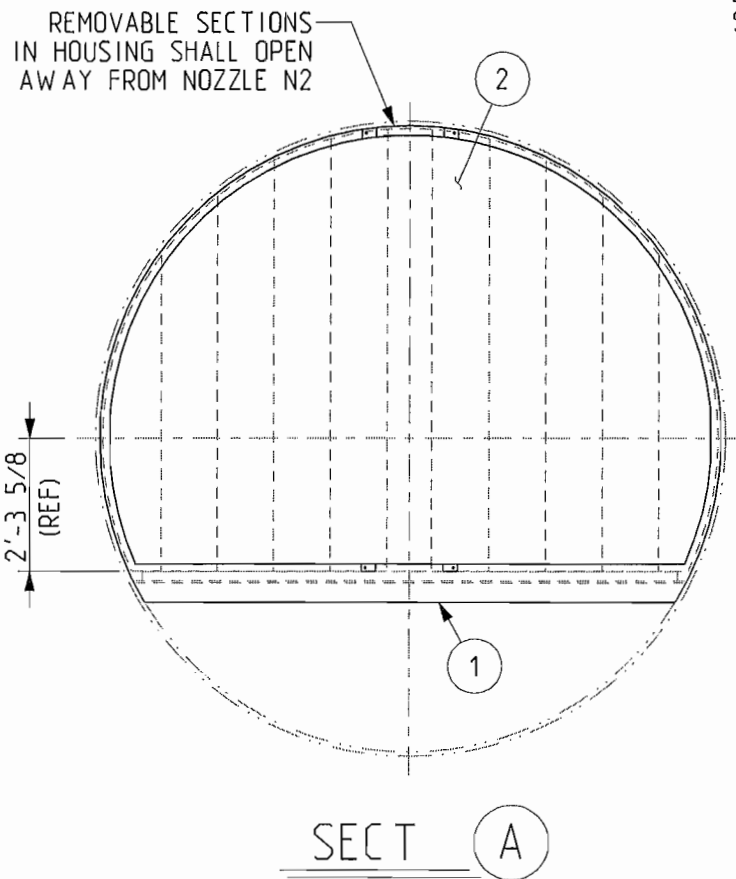
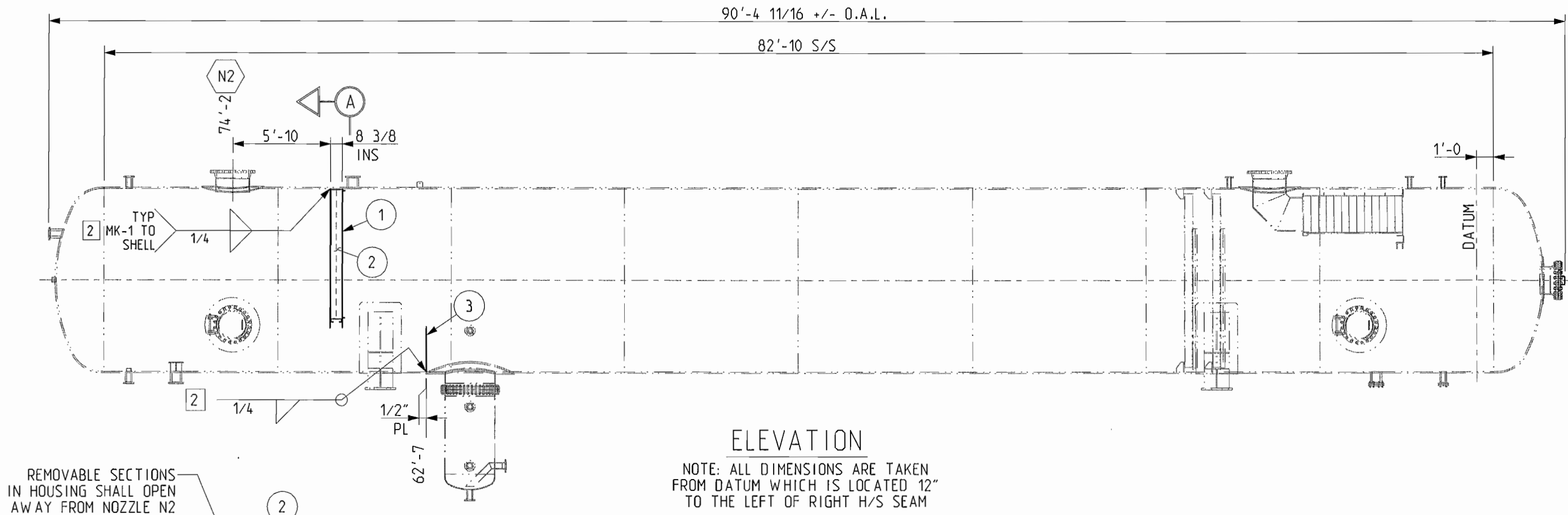
SHOP NOTE: INSTALL MK-2 VANE PAK
SO THAT FLOW DISTRIBUTOR IS
POINTED TOWARDS NOZZLE N2

WELDING PROCEDURE KEY

2 P1-P1-FCAW-AL
P1-P1-GMAWP-AL

BILL OF MATERIAL

Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
	5361-1E-1	1	HOUSING	VANE PAK HOUSING (BY AMACS)				SA-516-70		X	393
	5361-1E-2	1	VANE PAK	VANE PAK W / DISTRIBUTOR (BY AMACS)				304L SS			500
	5361-1E-3	1	PLATE	1/2" WEIR PLATE, SKETCH	0.500	32	112.125	SA-516-70		X	360



SHOP NOTE: ALL INTERNAL WELDS MUST BE SUITABLY PREPPED FOR INTERNAL LINING. ALL SHARP EDGES & ROUGH WELD CONTOURS ARE TO BE ROUNDED/SMOOTHED OUT. POROSITY & WELD SPATTER SHALL BE REMOVED.

APPROVED
FOR CONSTRUCTION
DATE 11/3/18 BY DB

No.	Date	By	Chk'd	Revision Description
				EATON METAL PRODUCTS CO LLC DENVER -- SALT LAKE CITY
Drawn By: RT				VANE PAK & WEIR DETAILS
Date: 9/18/2018				132" OD x 82'-10" S/S INLET SLUG CATCHER
Chk'd By: DB				P.O. # 4500100246 - TAG # V-1000
Date: 10/5/18				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
				Cust: ANADARKO E&P ONSHORE LLC
				EMP No. 5361-S01 Dwg. No. D-5361-1E

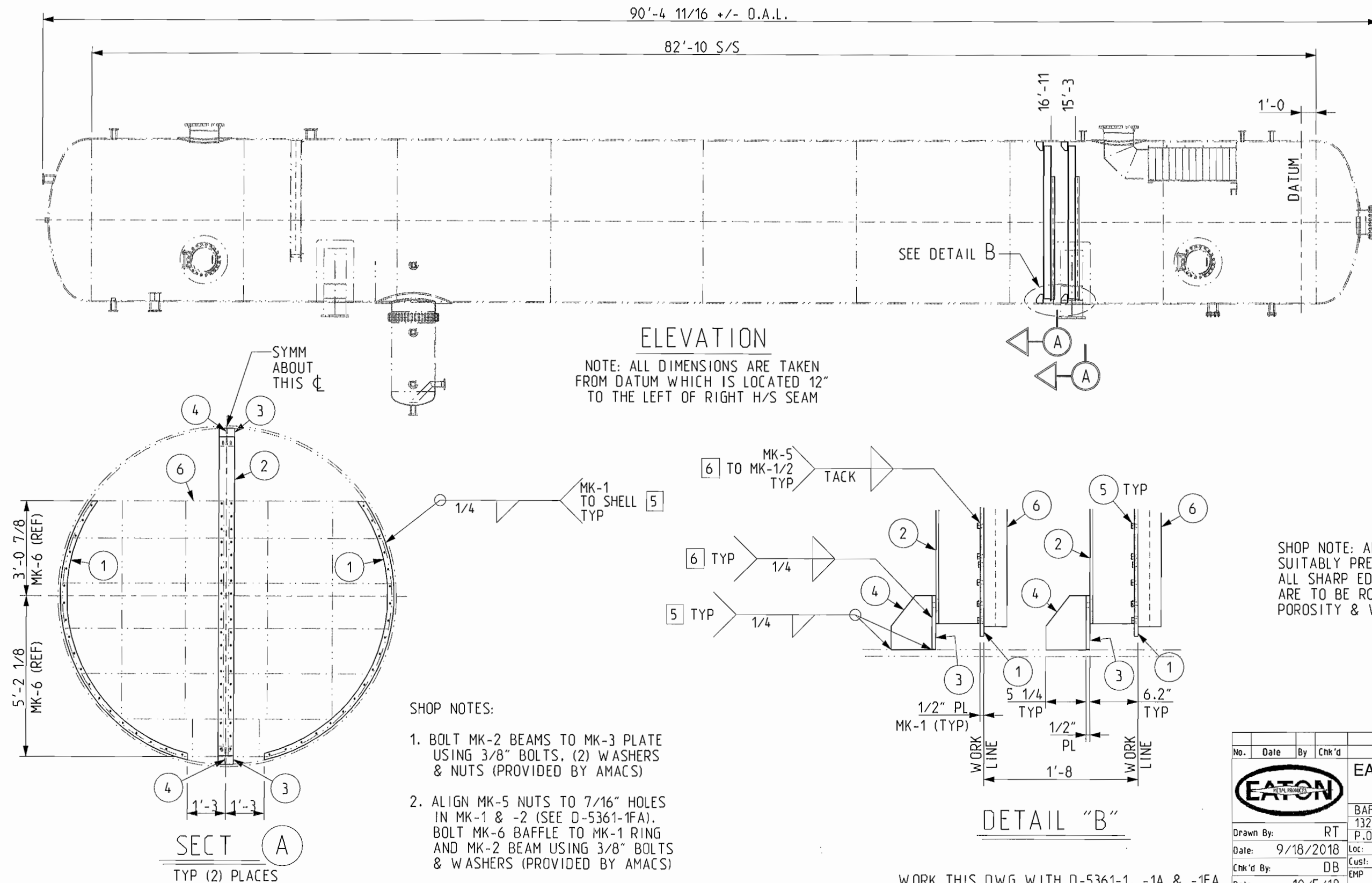
WORK THIS DWG WITH D-5361-1 & -1A

WELDING PROCEDURE KEY

- 5 P1-P8-FCAW -AL
P1-P8-GMAWP-A
P1-P8-GTAW -AL
- 6 P8-P8-GMAWP-A
P8-P8-GTAW -AL
P8-P8-SMAW -A

BILL OF MATERIAL

Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
	5361-1F-1	4	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	50.125	100.25	SA-240-304		X	175
	5361-1F-2	2	BEAM	W6 x 20 W/HOLES & SLOTS			123.5	304 SS			412
	5361-1F-3	4	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	6	7	SA-240-304		X	23
	5361-1F-4	4	PLATE	1/2" PLATE, SKETCH	0.500	5.25	7	SA-240-304		X	17
	5361-1F-5	156	NUT	3/8" HEAVY HEX				304 SS			5
	5361-1F-6	2	BAFFLE	DISTRIBUTION BAFFLE (BY AMACS)				304L SS			900

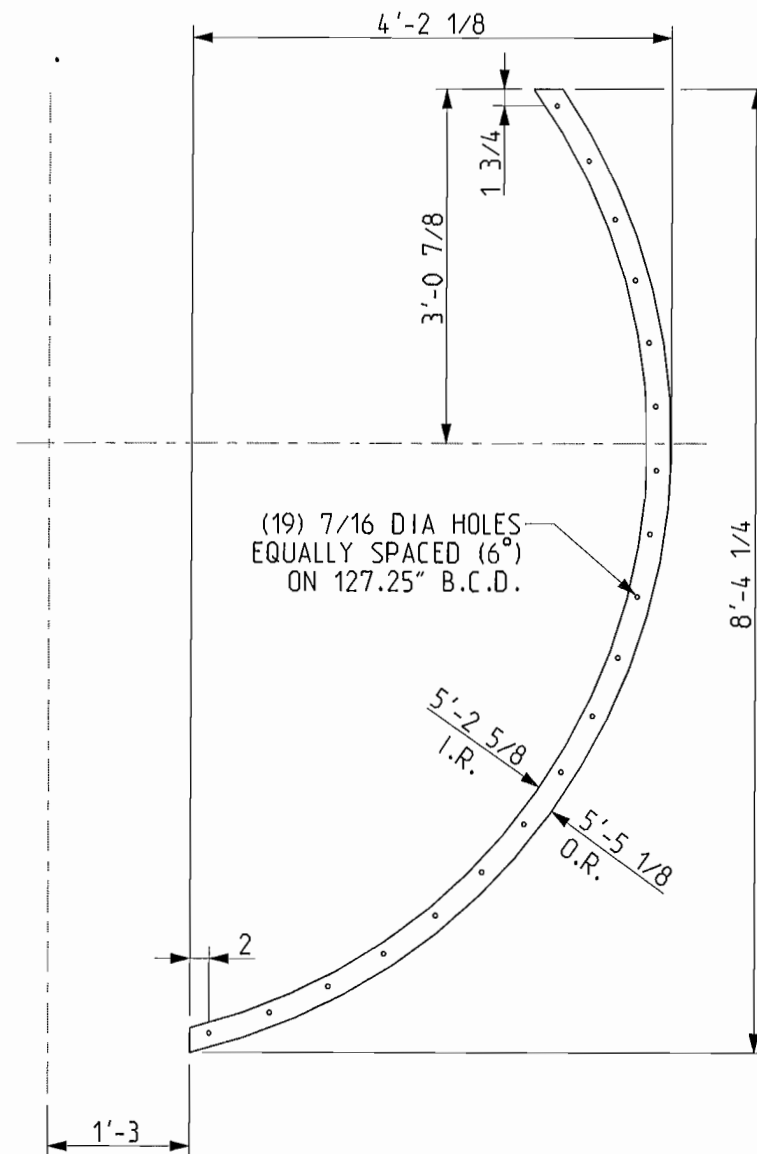


SHOP NOTE: ALL INTERNAL WELDS MUST BE SUITABLY PREPPED FOR INTERNAL LINING. ALL SHARP EDGES & ROUGH WELD CONTOURS ARE TO BE ROUNDED/SMOOTHED OUT. POROSITY & WELD SPATTER SHALL BE REMOVED.

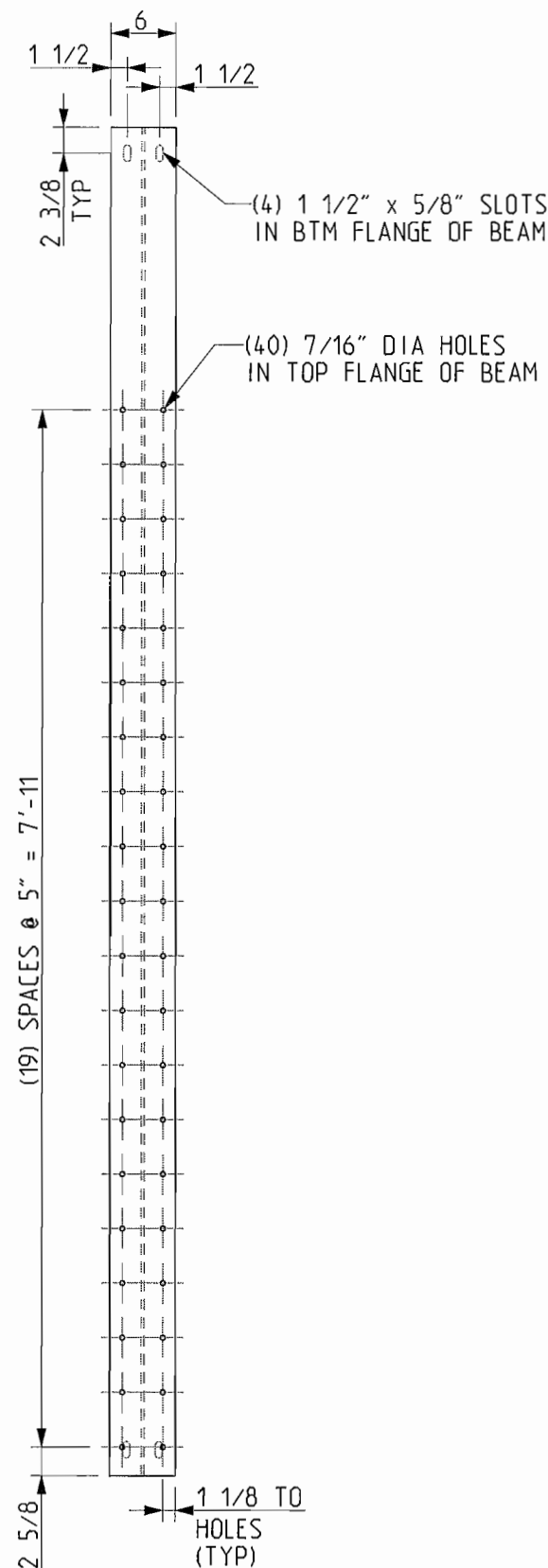
APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY DB

No.	Date	By	Chk'd	Revision Description
EATON				EATON METAL PRODUCTS CO LLC DENVER -- SALT LAKE CITY
BAFFLE DETAILS				132" OD x 82'-10" S/S INLET SLUG CATCHER
P.O. # 4500100246 - TAG # V-1000				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
Date: 9/18/2018				Cust: ANADARKO E&P ONSHORE LLC
Chk'd By: DB				EMP
Date: 10/5/18				Job No. 5361-S01 Dwg. No. D-5361-1F

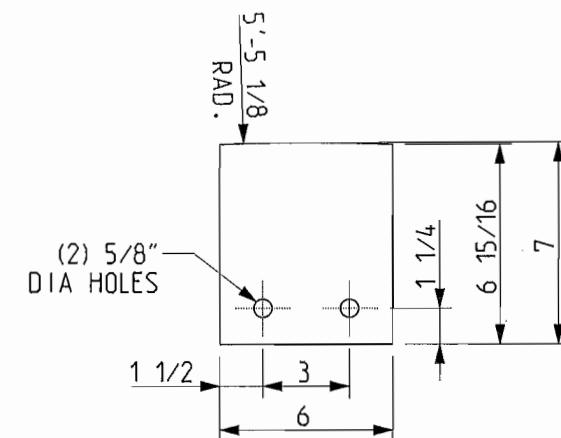
WORK THIS DWG WITH D-5361-1, -1A & -1FA



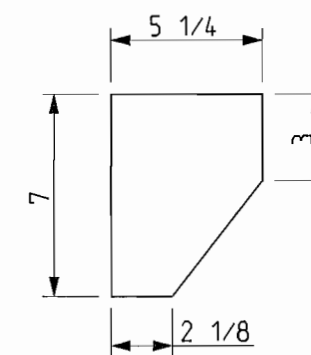
DETAIL 1
1/2" PL



DETAIL 2
1/2" PL



DETAIL 3
1/2" PL



DETAIL 4
1/2" PL

APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY [Signature]

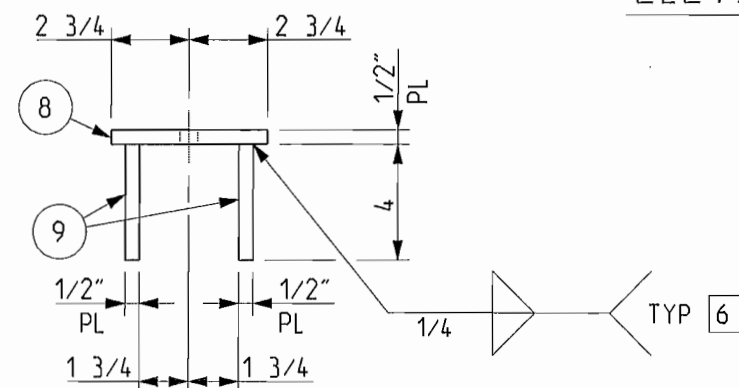
No.	Date	By	Chk'd	Revision Description
				EATON METAL PRODUCTS CO LLC
				DENVER -- SALT LAKE CITY
				BAFFLE DETAILS
				132" OD x 82'-10" S/S INLET SLUG CATCHER
				P.O. # 4500100246 - TAG # V-1000
				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
				Cust: ANADARKO E&P ONSHORE LLC
				EMP No. 5361-S01
				Dwg. No. D-5361-1FA
Drawn By:	RT			
Date:	9/18/2018			
Chk'd By:	DB			
Date:	10/5/18			

WORK THIS DWG WITH D-5361-1F

5 P1-P8-FCAW -AL
P1-P8-GMAWP-A
P1-P8-GTAW -AL

6 P8-P8-GMAWP-A
P8-P8-GTAW -AL
P8-P8-SMAW -A

Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
	5361-1G-1	1	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	30	36	SA-240-304			87
	5361-1G-2	1	PIPE	24" NOM XH, SKETCH	0.500		18.688	SA-312-TP304			144
	5361-1G-3	1	PIPE	24" NOM XH, SKETCH	0.500		23.75	SA-312-TP304			145
	5361-1G-4	1	PIPE	24" NOM XH, SKETCH	0.500		10.563	SA-312-TP304		X	59
	5361-1G-5	2	PLATE	1/2" PLATE W/HOLES	0.500	4	12	SA-240-304			13
	5361-1G-6	4	PLATE	1/2" PLATE, SKETCH	0.500	2.25	3.5	SA-240-304			4
	5361-1G-7	2	PLATE	1/2" PLATE W/HOLES	0.500	2.5	70	SA-240-304		X	49
	5361-1G-8	2	PLATE	1/2" PLATE W/HOLE	0.500	5.5	7.813	SA-240-304		X	12
	5361-1G-9	4	PLATE	1/2" PLATE, SKETCH	0.500	4	9.688	SA-240-304		X	20
	5361-1G-10	1	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	6	12	SA-240-304		X	10
	5361-1G-11	1	DIFFUSER	INLET DIFFUSER ASSY (BY AMACS)				304L SS			942



DIFFUSER BEAM SEAT
TYP (2) PLACES

Technical drawing of a ship's hull structure, showing a cross-section of a hull girder. The drawing includes various components labeled 1 through 10, and dimensions for distances to MK-7 and MK-8 holes.

Key dimensions and labels:

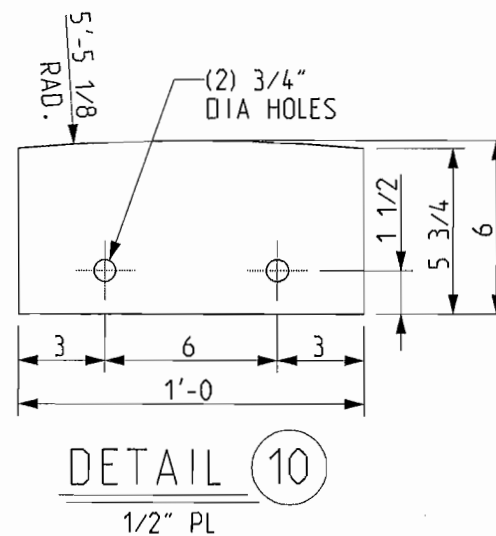
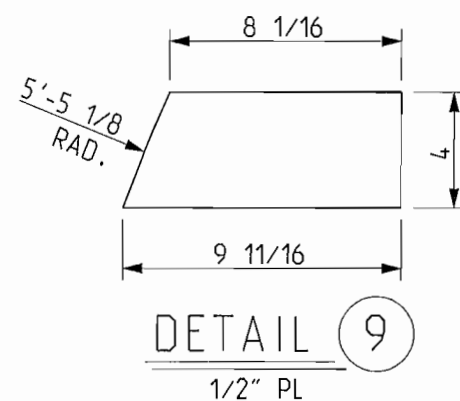
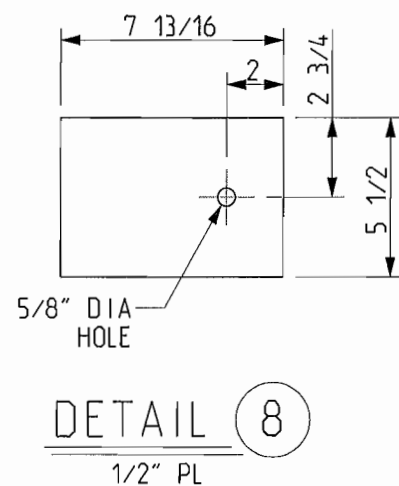
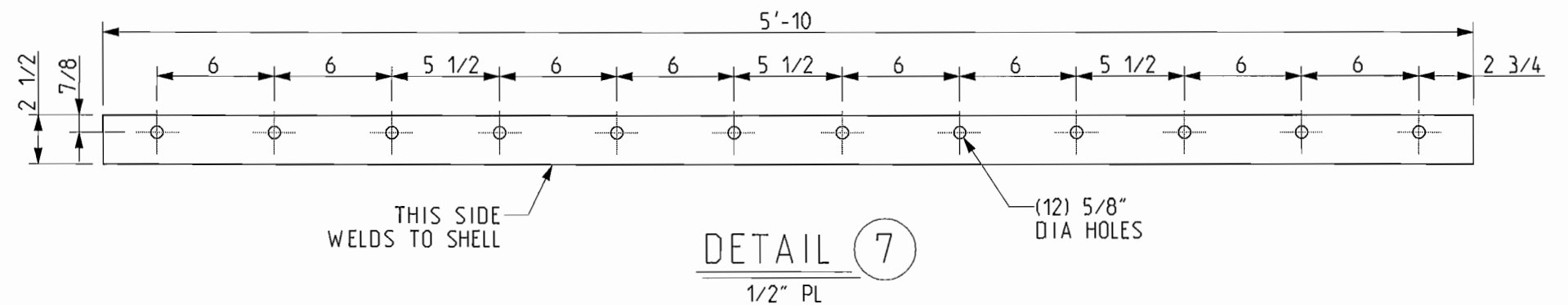
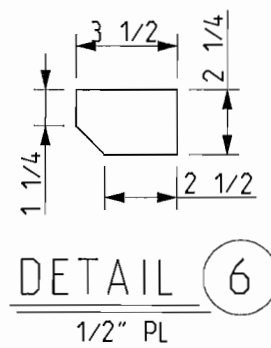
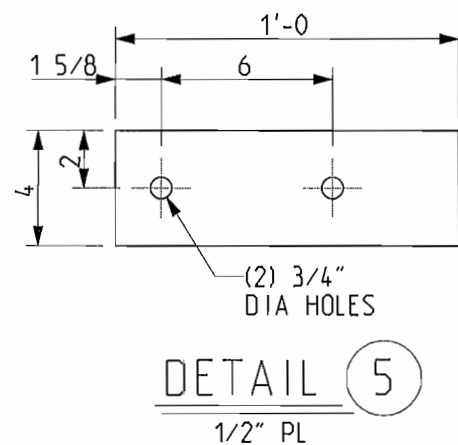
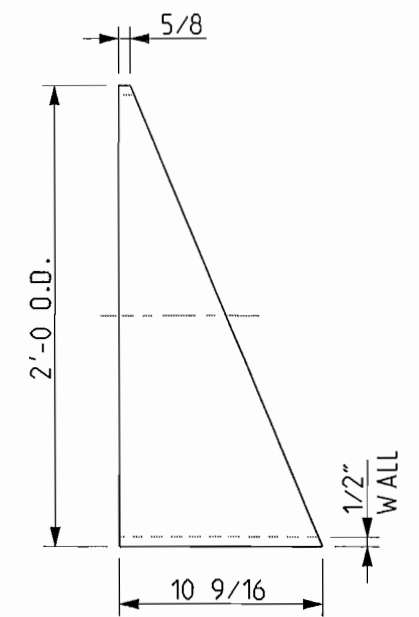
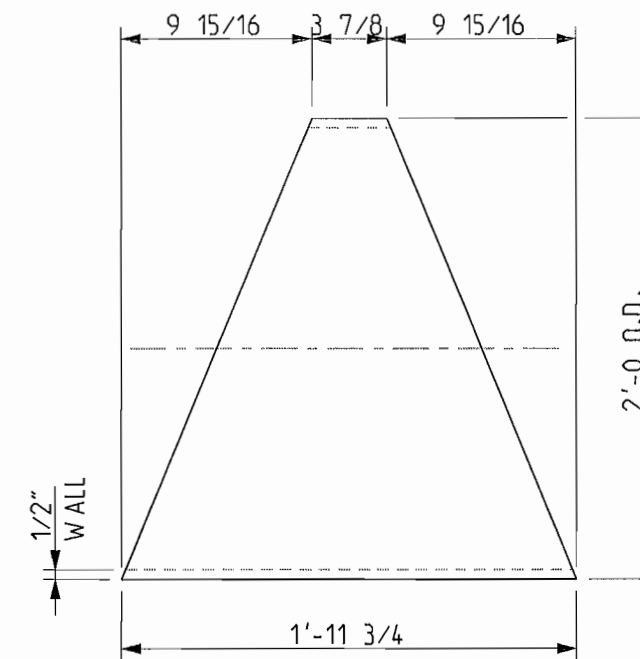
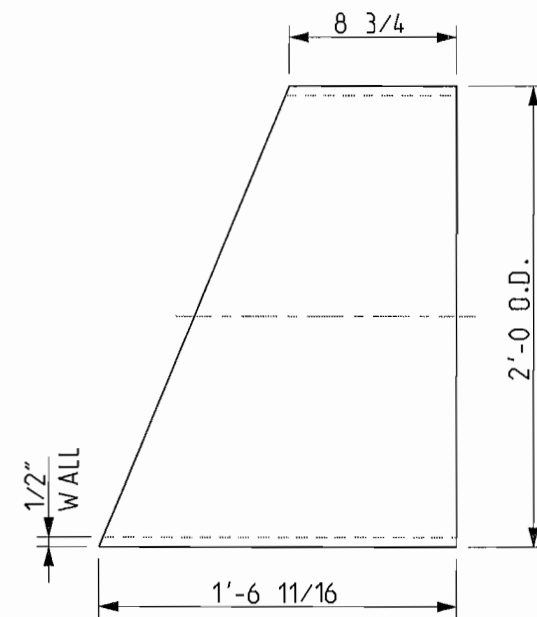
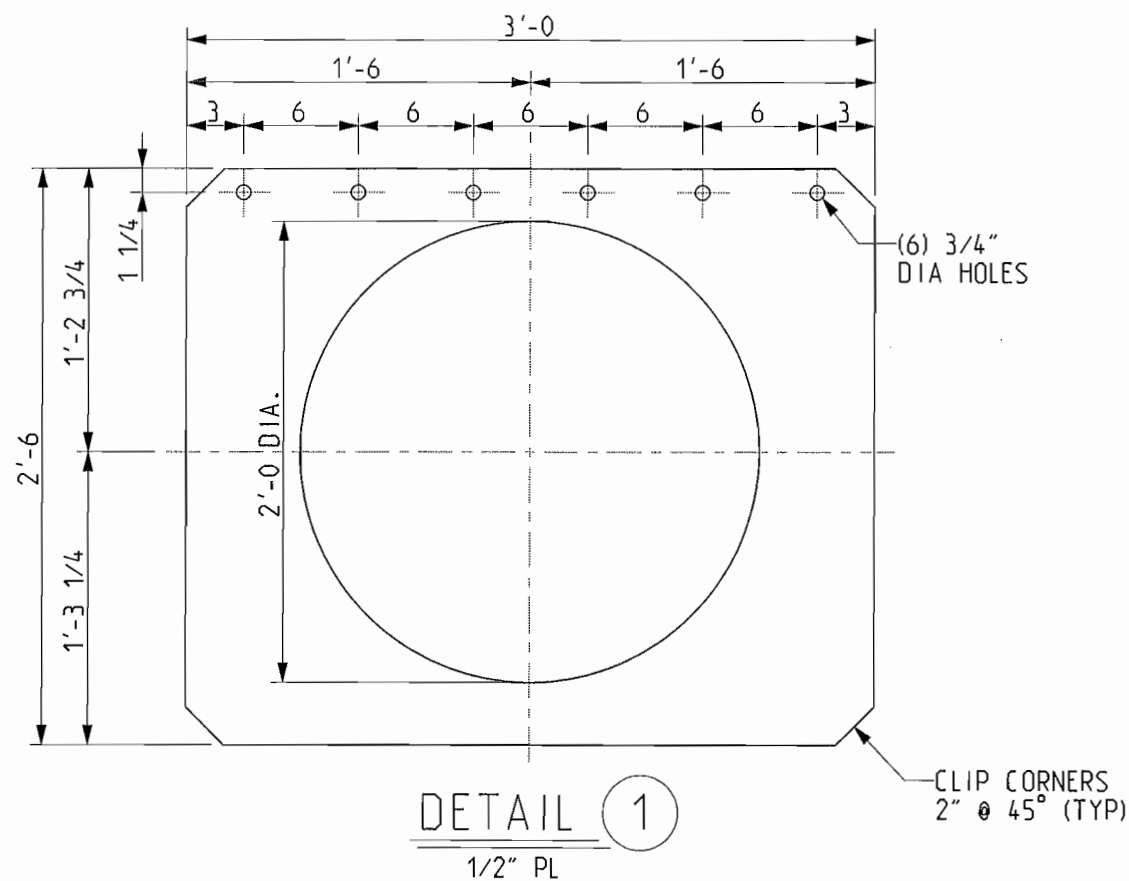
- 4'-6 TO MK-7 HOLES
- 4'-5 1/2 TO MK-8 HOLE
- 1'-1 1/2 TYP
- 1'-0 1/2 TYP
- 1'-0 TYP
- 1/2" PL
- 1'-0
- 1 3/8
- 6 1/2
- 5 1/2
- 2'-2 7/8 TYP
- 2'-9 7/8 TYP
- 1/2" PL
- 1/4
- 1/4
- SYM ABT
- N1
- 10
- 1
- 5
- 5
- 6
- 7
- 8
- 9 (2)
- 9
- 6
- 6

MK-11 HIDDEN
FOR CLARITY

APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY LB

No.	Date	By	Chk'd	Revision	Description
				EATON METAL PRODUCTS CO LLC	
				DENVER -- SALT LAKE CITY	
				INLET DIFFUSER DETAILS	
				132" OD x 82'-10" S/S INLET SLUG CATCHER	
Drawn By:	RT			P.O. # 4500100246 - TAG # V-1000	
Date:	9/18/2018			Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO	
Chk'd By:	DB			Cus: ANADARKO E&P ONSHORE LLC	
Date:	10/5/18			EMP Job No.	Dwg. D-5361-1G

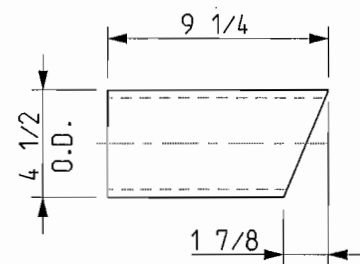
WORK THIS DWG WITH D-5361-1, -1A & -1GA



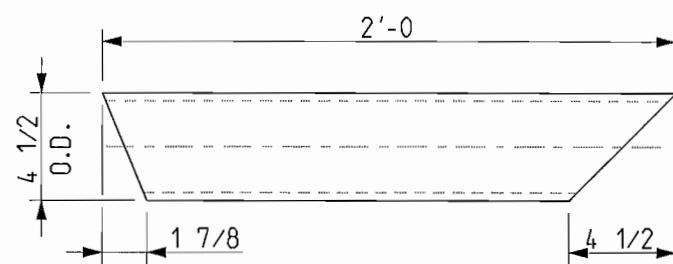
APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY DB

No.	Date	By	Chk'd	Revision Description
				EATON METAL PRODUCTS CO LLC
				DENVER -- SALT LAKE CITY
				INLET DIFFUSER DETAILS
				132" OD x 82'-10" S/S INLET SLUG CATCHER
				P.O. # 4500100246 - TAG # V-1000
				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
				Cust: ANADARKO E&P ONSHORE LLC
				EMP
				Job No. 5361-S01
				Dwg. No. D-5361-1GA
				REV

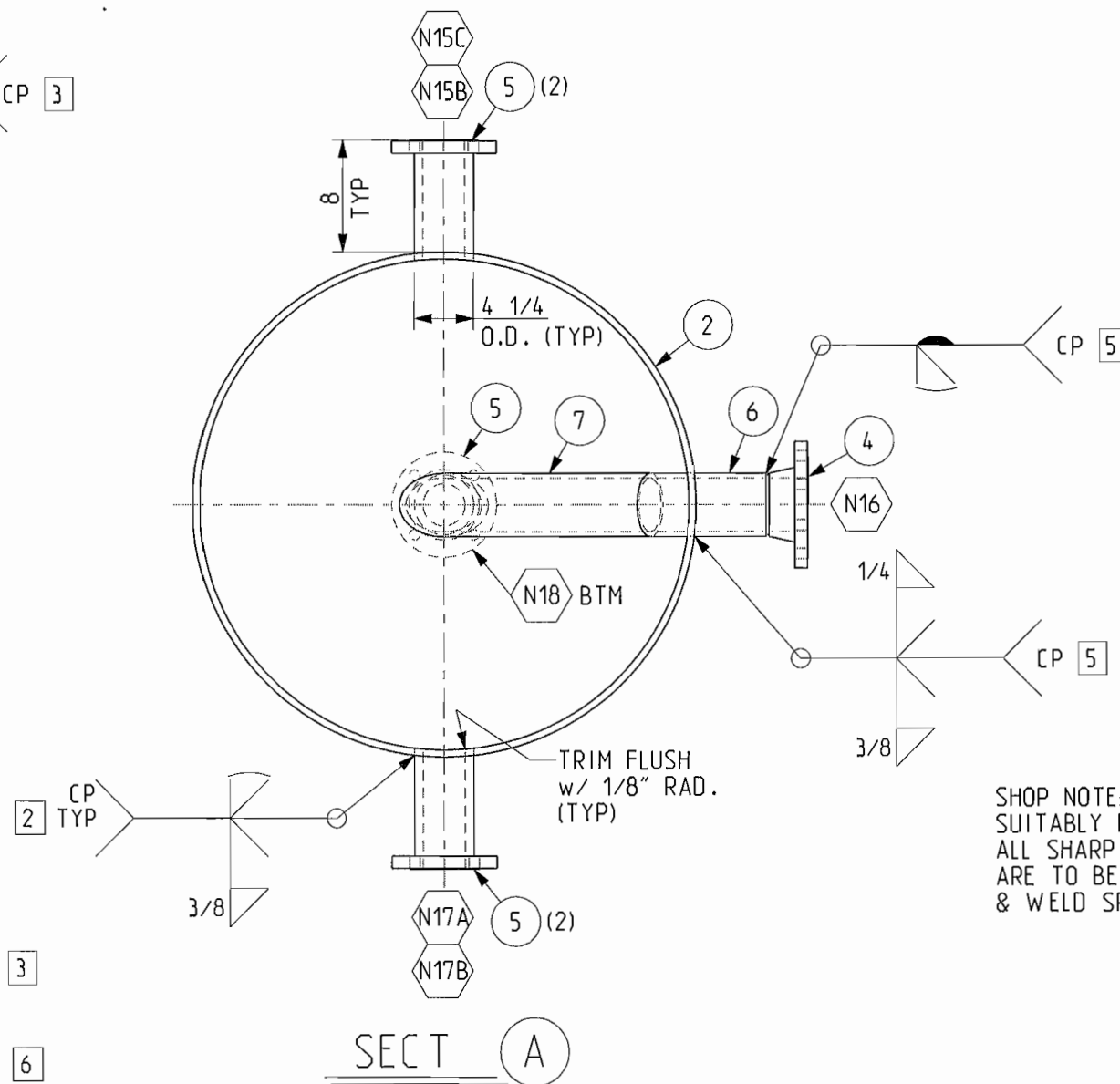
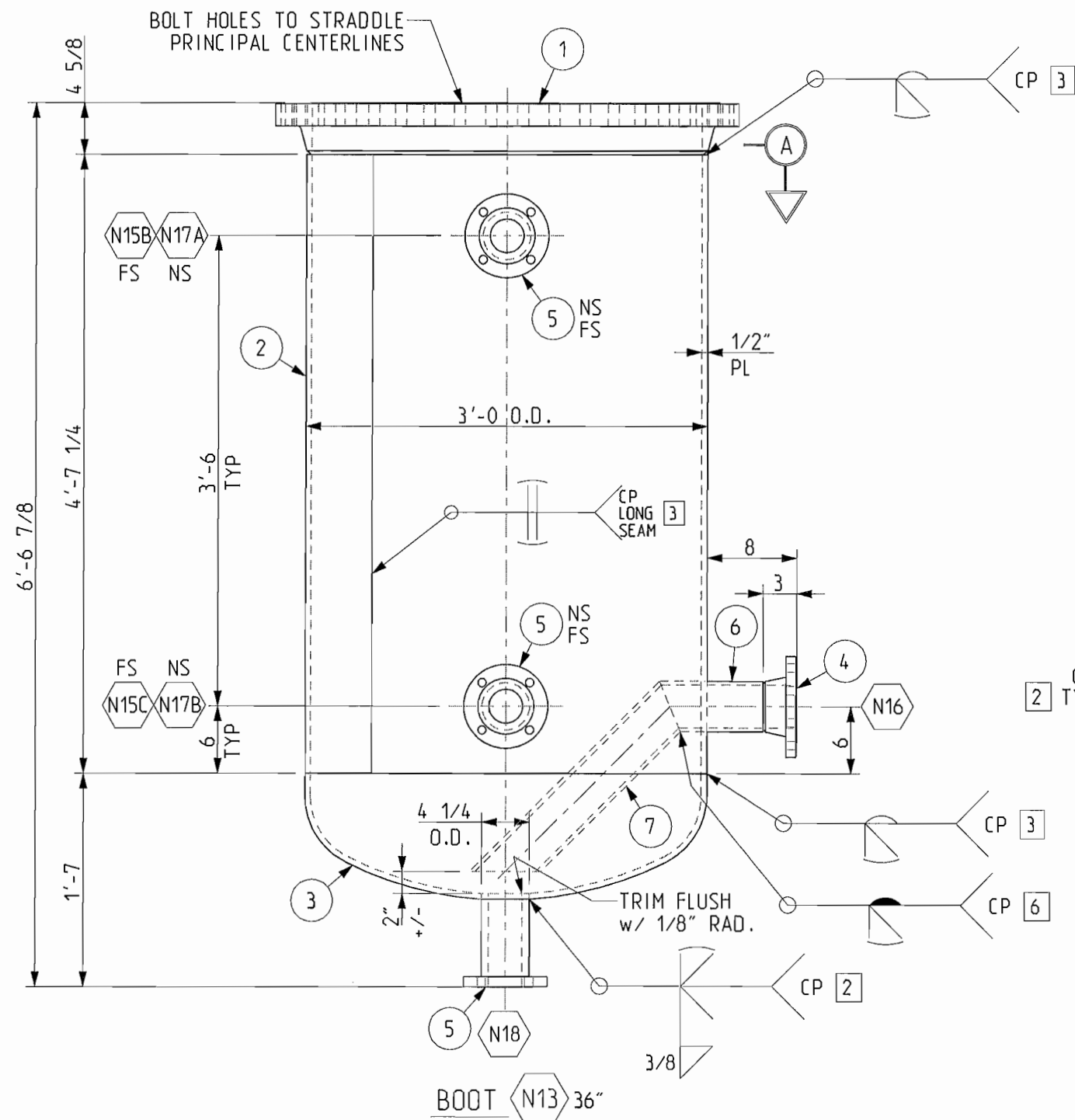
WORK THIS DWG WITH D-5361-1G



DETAIL 6



DETAIL 7



SHOP NOTE: ALL INTERNAL WELDS MUST BE SUITABLY PREPPED FOR INTERNAL LINING. ALL SHARP EDGES & ROUGH WELD CONTOURS ARE TO BE ROUNDED/SMOOTHED OUT. POROSITY & WELD SPATTER SHALL BE REMOVED.

APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY [Signature]

BILL OF MATERIAL

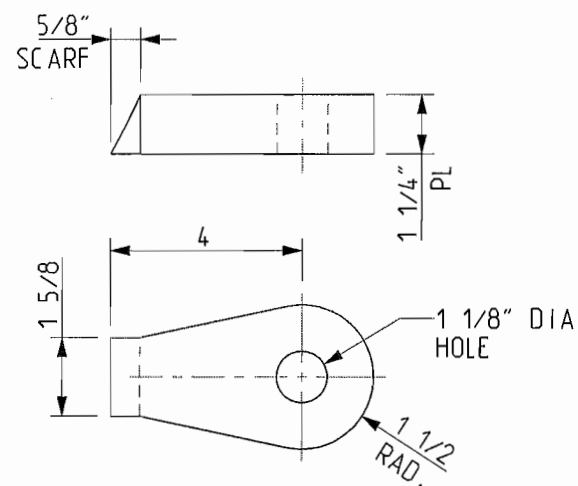
Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
1	5361-1H-A		BOOT	36" BOOT ASSEMBLY							1551#
	5361-1H-1	1	FLANGE	36" - 150# SERIES "B" RFWN XH BORE (35" I.O.)				SA-105		X	270
	5361-1H-2	1	PLATE	1/2" PLATE, ROLLED w/4" TANS	0.500	55.25	119.5	SA-516-70		X	874
	5361-1H-3	1	HEAD	0.375" MIN x 36" DD ASME 2:1 SF=2"				SA-516-70		X	228
	5361-1H-4	1	FLANGE	4" - 150# RFWN XH BORE				SA-105		X	16
	5361-1H-5	5	FLANGE	3" - 150# RF LWN			9	SA-105		X	127
	5361-1H-6	1	PIPE	4" NOM XH. SKETCH	0.337		9.25	SA-312-TP304		X	10
	5361-1H-7	1	PIPE	4" NOM XH. SKETCH	0.337		24	SA-312-TP304		X	26
1	5361-1H-B		GASKET	1/8" - 36" - 150# SERIES "B" RING TYPE C-4401				KLINGERSIL			1
44	5361-1H-C		STUD	7/8" DIA FULL THREAD			6.75	SA-193-B7			51
88	5361-1H-D		NUT	7/8" HEAVY HEX				SA-194-2H			26

WELDING PROCEDURE KEY

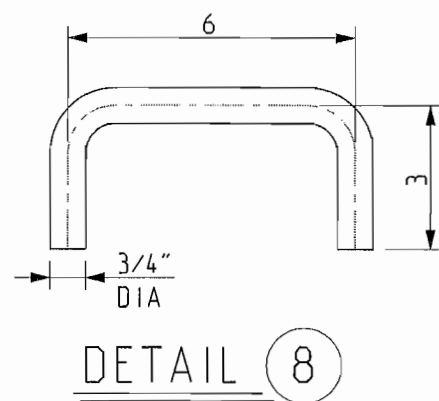
- 2 P1-P1-FCAW -AL
P1-P1-GMAWP -AL
- 3 P1-P1-GMAWP -AL
P1-P1-FCAW -AL
P1-P1-EM14K1-A
- 5 P1-P8-FCAW -AL
P1-P8-GMAWP -A
P1-P8-GTAW -AL
- 6 P8-P8-GMAWP -A
P8-P8-GTAW -AL
P8-P8-SMAW -A

No.	Date	By	Chk'd	Revision Description
				EATON METAL PRODUCTS CO LLC
				DENVER -- SALT LAKE CITY
				BOOT DETAILS
				132" OD x 82'-10" S/S INLET SLUG CATCHER
				P.O. # 4500100246 - TAG # V-1000
				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO
				Cust: ANADARKO E&P ONSHORE LLC
				EMP 5361-S01 Dwg. No. D-5361-1H

WORK THIS DWG WITH D-5361-1 & -1A



DETAIL 4



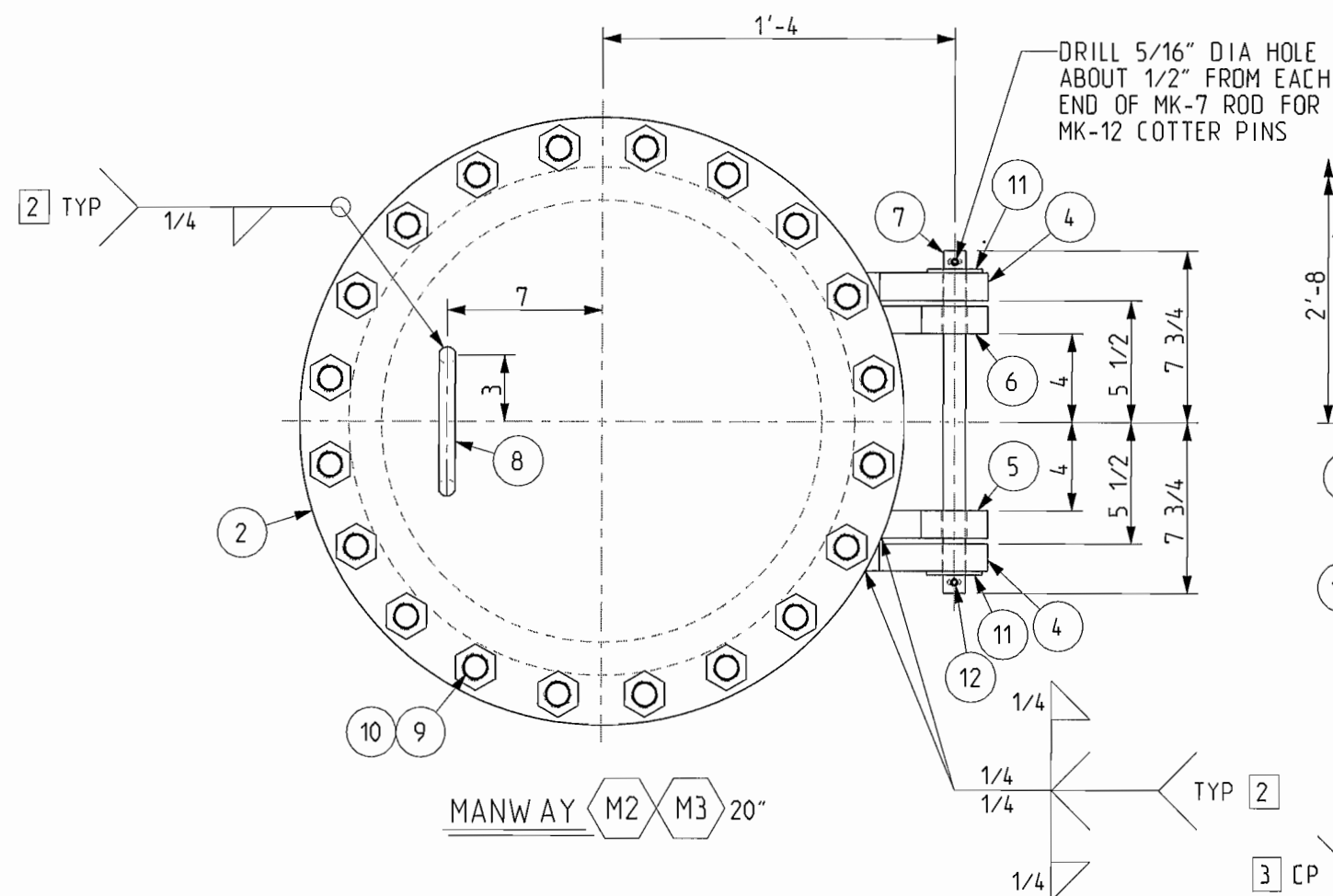
DETAIL 8

WELDING PROCEDURE KEY

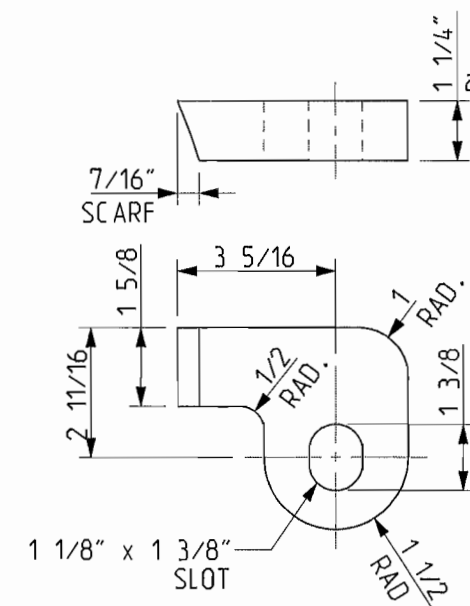
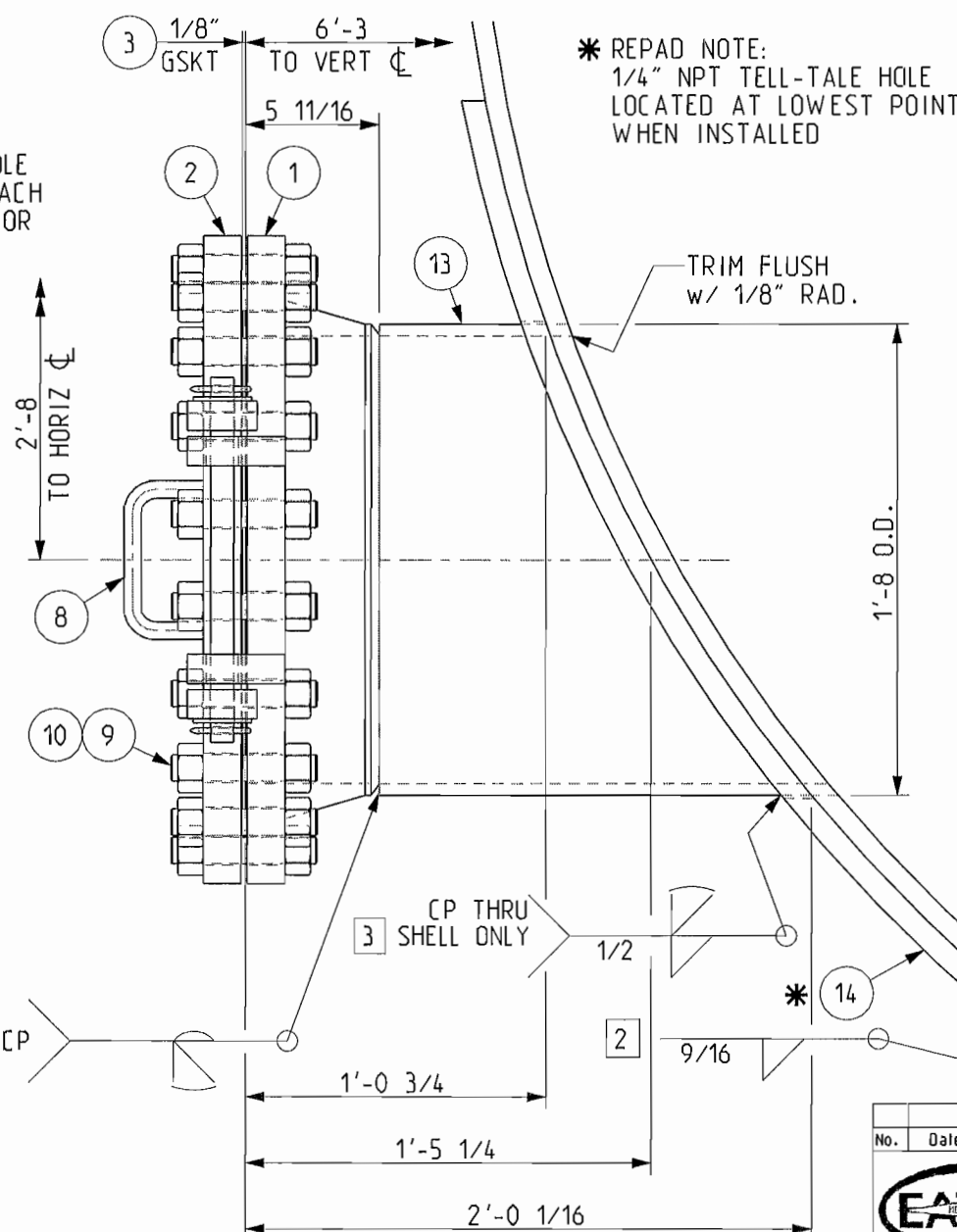
- 2 P1-P1-FCAW-AL
P1-P1-GMAWP-AL
- 3 P1-P1-GMAWP-AL
P1-P1-FCAW-AL
P1-P1-EM14K1-A

BILL OF MATERIAL

Ship Pcs	Mark	No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Spec	See Note	MTR	Weights
	5361-1J-1	2		FLANGE	20" - 150# RFWN XH BORE				SA-105		X	399
	5361-1J-2	2		FLANGE	20" - 150# RF BLIND				SA-105		X	541
	5361-1J-3	2		GASKET	1/8" - 20" - 150# RING TYPE KLINGERSIL C-4401				KLINGERSIL			2
	5361-1J-4	4		PLATE	1-1/4" SKETCH PL W/ HOLE	1.250	3	5.5	A-36		X	16
	5361-1J-5	2		PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	9
	5361-1J-6	2		PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	9
	5361-1J-7	2		ROD	1" DIA ROD W/ HOLES			15.5	A-36			7
	5361-1J-8	2		ROD	3/4" DIA ROD, BEND			12	A-36		X	3
	5361-1J-9	40		STUD	1-1/8" DIA FULL THREAD			6.25	SA-193-B7			70
	5361-1J-10	80		NUT	1-1/8" HEAVY HEX				SA-194-2H			46
	5361-1J-11	4		WASHER	1" STANDARD ROUND				STEEL			-
	5361-1J-12	4		COTTER	1/4" DIA COTTER PIN			1.5	STEEL			-
	5361-1J-13	2		PIPE	20" NOM XH	0.500		20.563	SA-106-B		X	357
	5361-1J-14	2		PLATE	CIRC 20.25 ID x 39" OD ROLL	1.000			SA-516-70		X	586



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DETAIL 5 (AS SHOWN)

DETAIL 6 (OPP HAND)

APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY DB

No.	Date	By	Chk'd	Revision	Description
				1	EATON METAL PRODUCTS CO LLC DENVER -- SALT LAKE CITY MANWAY M2 & M3 DETAILS 132" OD x 82'-10" S/S INLET SLUG CATCHER P.O. # 4500100246 - TAG # V-1000 Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO Cust: ANADARKO E&P ONSHORE LLC EMP 5361-S01 Dwg. No. D-5361-1J

WORK THIS DWG WITH D-5361-1 & -1A



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736

ASME Design Calculations

Eaton Metal Products

4800 York Street

Denver, Colorado 80216

(303) 296-4800 General

COMPRESS Pressure Vessel Design Calculations

Customer: Anadarko

Description: 132" OD x 82'-10" S/S Inlet Slug Catcher V-1000

P.O. # 4500100246

Job No.: 5361

By: RT

Date: 10/5/18

Check By:



Date:

10/5/18

Left Head

ASME Section VIII Division 1, 2017 Edition				
Component		Ellipsoidal Head		
Material		SA-516 70 (II-D p. 18, ln. 33)		
Attached To		Shell		
Impact Tested	Normalized	Fine Grain Practice	PWHT	Optimize MDMT/ Find MAWP
No	No	Yes	No	No
		Design Pressure (psi)	Design Temperature (°F)	Design MDMT (°F)
Internal		250	125	-20
Static Liquid Head				
Condition		P _s (psi)	H _s (in)	SG
Operating		4.7	130.275	1
Test horizontal		5.17	143.15	1
Dimensions				
Outer Diameter		132"		
Head Ratio		2		
Minimum Thickness		0.85"		
Corrosion	Inner	0"		
	Outer	0"		
Length L _{sf}		2"		
Nominal Thickness t _{sf}		1"		
Weight and Capacity				
		Weight (lb) ¹		Capacity (US gal) ¹
New		5,004.26		1,368.52
Corroded		5,004.26		1,368.52
Radiography				
Category A joints		Full UW-11(a) Type 1		
Head to shell seam		Spot UW-11(a)(5)(b) Type 1		

¹ includes straight flange

Results Summary	
Governing condition	internal pressure
Minimum thickness per UG-16	0.0625" + 0" = 0.0625"
Design thickness due to internal pressure (t)	<u>0.831</u> "
Rated MDMT	-20°F

UCS-66 Material Toughness Requirements

Governing thickness, $t_g =$	0.85"
MDMT =	-20°F
Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F.	

Factor K

$K = (1/6) * [2 + (D / (2 * h))^2]$		
Corroded	$K = (1/6) * [2 + (130.3 / (2 * 32.575))^2]$	1
New	$K = (1/6) * [2 + (130.3 / (2 * 32.575))^2]$	1

Design thickness for internal pressure, (Corroded at 125 °F) Appendix 1-4(c)

$$\begin{aligned}
 t &= P * D_o * K / (2 * S * E + 2 * P * (K - 0.1)) + \text{Corrosion} \\
 &= 254.7 * 132 * 1 / (2 * 20,000 * 1 + 2 * 254.7 * (1 - 0.1)) + 0 \\
 &= \underline{0.831"}
 \end{aligned}$$

% Extreme fiber elongation - UCS-79(d)

$$\begin{aligned}
 EFE &= (75 * t / R_f) * (1 - R_f / R_o) \\
 &= (75 * 1 / 22.651) * (1 - 22.651 / \infty) \\
 &= 3.3111\%
 \end{aligned}$$

The extreme fiber elongation does not exceed 5%.

Shell

ASME Section VIII Division I, 2017 Edition				
Component		Cylinder		
Material		SA-516 70 (II-D p. 18, ln. 33)		
Impact Tested	Normalized	Fine Grain Practice	PWHT	Optimize MDMT/ Find MAWP
No	No	Yes	No	No
		Design Pressure (psi)	Design Temperature (°F)	Design MDMT (°F)
Internal		250	125	-20
Static Liquid Head				
Condition		P _s (psi)	H _s (in)	SG
Operating		4.7	130.25	1
Test horizontal		5.17	143.125	1
Dimensions				
Outer Diameter		132"		
Length		994"		
Nominal Thickness		0.875"		
Corrosion	Inner	0"		
	Outer	0"		
Weight and Capacity				
		Weight (lb)	Capacity (US gal)	
New		100,929.05	57,334.99	
Corroded		100,929.05	57,334.99	
Radiography				
Longitudinal seam		Full UW-11(a) Type 1		
Left Circumferential seam		Spot UW-11(a)(5)(b) Type 1		
Right Circumferential seam		Spot UW-11(a)(5)(b) Type 1		

Results Summary	
Governing condition	Internal pressure
Minimum thickness per UG-16	0.0625" + 0" = 0.0625"
Design thickness due to internal pressure (t)	0.8363"
Rated MDMT	-20 °F

UCS-66 Material Toughness Requirements	
Governing thickness, t _g =	0.875"
MDMT =	-20°F

Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F.

Design thickness, (at 125 °F) Appendix 1-1

$$\begin{aligned} t &= P \cdot R_o / (S \cdot E + 0.40 \cdot P) + \text{Corrosion} \\ &= 254.7 \cdot 66 / (20,000 \cdot 1.00 + 0.40 \cdot 254.7) + 0 \\ &= \underline{0.8363"} \end{aligned}$$

% Extreme fiber elongation - UCS-79(d)

$$\begin{aligned} \text{EFE} &= (50 \cdot t / R_f) \cdot (1 - R_f / R_o) \\ &= (50 \cdot 0.875 / 65.5625) \cdot (1 - 65.5625 / \infty) \\ &= 0.6673\% \end{aligned}$$

The extreme fiber elongation does not exceed 5%.

Allowable Compressive Stress, Hot and Corroded- S_{cHC} , (table CS-2)

$$\begin{aligned} A &= 0.125 / (R_o / t) \\ &= 0.125 / (66 / 0.875) \\ &= 0.001657 \\ B &= 14,214 \text{ psi} \\ S &= 20,000 / 1.00 = 20,000 \text{ psi} \\ S_{cHC} &= \min(B, S) = 14,214 \text{ psi} \end{aligned}$$

Allowable Compressive Stress, Hot and New- S_{cHN}

$$\begin{aligned} S_{cHN} &= S_{cHC} \\ &= 14,214 \text{ psi} \end{aligned}$$

Allowable Compressive Stress, Cold and New- S_{cCN} , (table CS-2)

$$\begin{aligned} A &= 0.125 / (R_o / t) \\ &= 0.125 / (66 / 0.875) \\ &= 0.001657 \\ B &= 14,214 \text{ psi} \\ S &= 20,000 / 1.00 = 20,000 \text{ psi} \\ S_{cCN} &= \min(B, S) = 14,214 \text{ psi} \end{aligned}$$

Allowable Compressive Stress, Cold and Corroded- S_{cCC}

$$\begin{aligned} S_{cCC} &= S_{cCN} \\ &= 14,214 \text{ psi} \end{aligned}$$

Allowable Compressive Stress, Vacuum and Corroded- S_{cVC} , (table CS-2)

$$\begin{aligned} A &= 0.125 / (R_o / t) \\ &= 0.125 / (66 / 0.875) \\ &= 0.001657 \\ B &= 14,214 \text{ psi} \\ S &= 20,000 / 1.00 = 20,000 \text{ psi} \\ S_{cVC} &= \min(B, S) = 14,214 \text{ psi} \end{aligned}$$

Right Head

ASME Section VIII Division 1, 2017 Edition				
Component		Ellipsoidal Head		
Material		SA-516 70 (II-D p. 18, ln. 33)		
Attached To		Shell		
Impact Tested	Normalized	Fine Grain Practice	PWHT	Optimize MDMT/ Find MAWP
No	No	Yes	No	No
		Design Pressure (psi)	Design Temperature (°F)	Design MDMT (°F)
Internal		250	125	-20
Static Liquid Head				
Condition		P _s (psi)	H _s (in)	SG
Operating		4.7	130.275	1
Test horizontal		5.17	143.15	1
Dimensions				
Outer Diameter		132"		
Head Ratio		2		
Minimum Thickness		0.85"		
Corrosion	Inner	0"		
	Outer	0"		
Length L _{sf}		2"		
Nominal Thickness t _{sf}		1"		
Weight and Capacity				
		Weight (lb) ¹	Capacity (US gal) ¹	
New		4,939.01	1,368.52	
Corroded		4,939.01	1,368.52	
Radiography				
Category A joints		Full UW-11(a) Type 1		
Head to shell seam		Spot UW-11(a)(5)(b) Type 1		

¹ includes straight flange

Results Summary	
Governing condition	internal pressure
Minimum thickness per UG-16	0.0625" + 0" = 0.0625"
Design thickness due to internal pressure (t)	0.831"
Rated MDMT	-20°F

UCS-66 Material Toughness Requirements

Governing thickness, $t_g =$	0.85"
MDMT =	-20°F
Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F.	

Factor K

$$K = (1/6) * [2 + (D / (2 * h))^2]$$

Corroded	$K = (1/6) * [2 + (130.3 / (2 * 32.575))^2]$	1
New	$K = (1/6) * [2 + (130.3 / (2 * 32.575))^2]$	1

Design thickness for internal pressure, (Corroded at 125 °F) Appendix 1-4(c)

$$\begin{aligned}
 t &= P * D_o * K / (2 * S * E + 2 * P * (K - 0.1)) + \text{Corrosion} \\
 &= 254.7 * 132 * 1 / (2 * 20,000 * 1 + 2 * 254.7 * (1 - 0.1)) + 0 \\
 &= \underline{0.831"}
 \end{aligned}$$

% Extreme fiber elongation - UCS-79(d)

$$\begin{aligned}
 EFE &= (75 * t / R_f) * (1 - R_f / R_o) \\
 &= (75 * 1 / 22.651) * (1 - 22.651 / \infty) \\
 &= 3.3111\%
 \end{aligned}$$

The extreme fiber elongation does not exceed 5%.

Liquid Level

ASME Section VIII Division 1, 2017 Edition	
Location from Center Line (in)	65.125
Operating Liquid Specific Gravity	1

Wind Code

Building Code: ASCE 7-10	
Elevation of base above grade	1.00 ft
Increase effective outer diameter by	1.00 ft
Wind Force Coefficient, C_f	0.6000
Risk Category (Table 1.5-1)	III
Basic Wind Speed, V	120.0000 mph
Exposure Category	C
Wind Directionality Factor, K_d	0.9500
Topographic Factor, K_{zt}	1.0000
Enforce minimum design load of 16 psf per ASCE 29.8:	Yes
Hazardous, toxic, or explosive contents	No

Wind Pressure (WP) Calculations

$$\begin{aligned}
 K_z &= 2.01 * (Z/z_g)^{2/\alpha} \\
 &= 2.01 * (15.00 / 900.00)^{0.2105} \\
 &= 0.8489
 \end{aligned}$$

$$\begin{aligned}
 q_z &= 0.00256 * K_z * K_{zt} * K_d * V^2 \\
 &= 0.00256 * 0.8489 * 1.0000 * 0.9500 * 120.0000^2 \\
 &= 29.7286 \text{ psf}
 \end{aligned}$$

$$\begin{aligned}
 q_z &= 0.6 * \max[29.7286, 16.0000] \\
 &= 17.8372 \text{ psf}
 \end{aligned}$$

Note: The 0.6 factor is the wind load combination factor from Section 2.4.1.

Table Lookup Values	
$\alpha = 9.5000$, $z_g = 900.00$ ft	[Table 26.9-1, page 256]

Shear calculations are reported in the saddle report.

Saddles

ASME Section VIII Division 1, 2017 Edition		
Saddle Material	SA-36	
Saddle Construction	Centered web	
Welded to Vessel	Yes	
Saddle Allowable Stress, S_s	21,600 psi	
Saddle Yield Stress, S_y	36,000 psi	
Foundation Allowable Stress	1,350 psi	
Design Pressure	Left Saddle	Right Saddle
Operating	254.7 psi	
Test	330.17 psi	
Dimensions		
Right saddle distance to datum	186"	
Tangent To Tangent Length, L	998"	
Saddle separation, L_s	598"	
Vessel Radius, R	66"	
Tangent Distance Left, A_l	200"	
Tangent Distance Right, A_r	200"	
Saddle Height, H_s	78"	
Saddle Contact Angle, θ	140°	
Web Plate Thickness, t_s	0.75"	
Base Plate Length, E	129"	
Base Plate Width, F	22"	
Base Plate Thickness, t_b	1.5"	
Number of Stiffening Ribs, n	7	
Largest Stiffening Rib Spacing, d_i	20.9583"	
Stiffening Rib Thickness, t_w	0.75"	
Saddle Width, b	18"	
Reinforcing Plate		
Thickness, t_p	0.375"	
Width, W_p	30"	
Contact Angle, θ_w	152°	
Bolting		
Material	A-307	
Bolt Allowable Shear	10,000 psi	

Description	2.75" series 8 threaded	
Corrosion on root	0"	
Anchor Bolts per Saddle	4	
Base coefficient of friction, μ	0.45	
Weight		
	Operating, Corroded	Hydrotest
Weight on Left Saddle	308,872 lb	308,926 lb
Weight on Right Saddle	310,287 lb	310,325 lb
Weight of Saddle Pair	6,290 lb	

Notes

(1) Saddle calculations are based on the method presented in "Stresses in Large Cylindrical Pressure Vessels on Two Saddle Supports" by L.P. Zick.

Stress Summary										
Load	Condition	Saddle	Bending + pressure between saddles (psi)				Bending + pressure at the saddle (psi)			
			S ₁ (+)	allow (+)	S ₁ (-)	allow (-)	S ₂ (+)	allow (+)	S ₂ (-)	allow (-)
Seismic	Operating	Right Saddle	<u>10,905</u>	24,000	<u>1,426</u>	17,057	<u>18,763</u>	24,000	<u>9,285</u>	17,057
		Left Saddle	<u>10,905</u>	24,000	<u>1,426</u>	17,057	<u>18,763</u>	24,000	<u>9,285</u>	17,057
Wind	Operating	Right Saddle	<u>10,560</u>	24,000	<u>1,082</u>	17,057	<u>17,899</u>	24,000	<u>8,420</u>	17,057
		Left Saddle	<u>10,560</u>	24,000	<u>1,082</u>	17,057	<u>17,899</u>	24,000	<u>8,420</u>	17,057
	Test	Right Saddle	<u>13,355</u>	34,200	<u>1,068</u>	17,057	<u>20,708</u>	34,200	<u>8,421</u>	17,057
		Left Saddle	<u>13,355</u>	34,200	<u>1,068</u>	17,057	<u>20,708</u>	34,200	<u>8,421</u>	17,057
Weight	Operating	Right Saddle	<u>10,539</u>	20,000	<u>1,061</u>	14,214	<u>17,899</u>	20,000	<u>8,420</u>	14,214
		Left Saddle	<u>10,539</u>	20,000	<u>1,061</u>	14,214	<u>17,899</u>	20,000	<u>8,420</u>	14,214

Stress Summary											
Load	Condition	Saddle	Tangential shear (psi)		Circumferential stress (psi)			Stress over saddle (psi)		Splitting (psi)	
			S ₃	allow	S ₄ (horns)	S ₄ (Wear plate)	allow (+/-)	S ₅	allow	S ₆	allow
Seismic	Operating	Right Saddle	<u>4,264</u>	16,000	<u>-28,971</u>	<u>-28,927</u>	30,000	<u>15,597</u>	18,000	<u>5,323</u>	14,400
		Left Saddle	<u>4,234</u>	16,000	<u>-28,839</u>	<u>-28,795</u>	30,000	<u>15,526</u>	18,000	<u>5,299</u>	14,400
Wind	Operating	Right Saddle	<u>2,893</u>	16,000	<u>-21,966</u>	<u>-21,933</u>	30,000	<u>11,826</u>	18,000	<u>4,036</u>	14,400
		Left Saddle	<u>2,871</u>	16,000	<u>-21,868</u>	<u>-21,835</u>	30,000	<u>11,773</u>	18,000	<u>4,018</u>	14,400
	Test	Right Saddle	<u>2,830</u>	27,360	<u>-21,685</u>	<u>-21,653</u>	34,200	<u>11,675</u>	32,400	<u>3,985</u>	32,400
		Left Saddle	<u>2,808</u>	27,360	<u>-21,588</u>	<u>-21,556</u>	34,200	<u>11,623</u>	32,400	<u>3,967</u>	32,400
Weight	Operating	Right Saddle	<u>2,798</u>	16,000	<u>-21,543</u>	<u>-21,511</u>	30,000	<u>11,598</u>	18,000	<u>3,959</u>	14,400
		Left Saddle	<u>2,776</u>	16,000	<u>-21,445</u>	<u>-21,413</u>	30,000	<u>11,545</u>	18,000	<u>3,940</u>	14,400

Seismic base shear on vessel	
Vessel is assumed to be a rigid structure.	
Method of seismic analysis	ASCE 7-10 ground supported
Vertical seismic accelerations considered	Yes
Importance factor, I_e	1.25
Site Class	D
Short period spectral response acceleration as percent of g , S_s	100
1 second spectral response acceleration as percent of g , S_1	40
From Table 11.4-1, F_a	1.1
From Table 11.4-2, F_v	1.6
Risk Category (Table 1.5-1)	II
Hazardous, toxic, or explosive contents	No
Equations	
$S_{MS} = F_a * S_s$	
$S_{M1} = F_v * S_1$	
$S_{DS} = (2 / 3) * S_{MS}$	
$S_{D1} = (2 / 3) * S_{M1}$	
$F_p = 0.3 * S_{DS} * W * I_e * 0.7$	
Results	
$S_{MS} = 1.1 * 1$	1.1
$S_{M1} = 1.6 * 0.4$	0.64
$S_{DS} = (2 / 3) * 1.1$	0.7333
$S_{D1} = (2 / 3) * 0.64$	0.4267
Seismic Design Category (Section 11.6)	D
$F_p = 0.3 * 0.7333 * 619,159 * 1.25 * 0.7$	119,188.11 lb_f

Saddle reactions due to weight + seismic	
V_v = vertical seismic force acting on the saddle	
V = horizontal seismic shear acting on the saddle (worst case if not slotted)	
Seismic longitudinal reaction, Q_l	
Seismic transverse reaction, Q_t	
Equations	
$Q_l = V * H_s / L_s + V_v$	
$Q_t = V * H_s / (R_o * \sin(\theta / 2)) + V_v$	
$Q = W + \max[Q_t, Q_l]$	
Results	

Operating	Right Saddle	$Q_l = 119,188.11 * 78 / 598 + 0.14 * 0.7333 * 310,287$	47,402.41 lb _f
		$Q_t = 59,730.25 * 78 / (66 * \sin(140 / 2)) + 0.14 * 0.7333 * 310,287$	106,976.75 lb _f
		$Q = 310,287 + \max[106,976.75, 47,402.41]$	417,263.75 lb _f
	Left Saddle	$Q_l = 119,188.11 * 78 / 598 + 0.14 * 0.7333 * 308,872$	47,257.13 lb _f
		$Q_t = 59,457.86 * 78 / (66 * \sin(140 / 2)) + 0.14 * 0.7333 * 308,872$	106,488.91 lb _f
		$Q = 308,872 + \max[106,488.91, 47,257.13]$	415,360.91 lb _f

Saddle reactions due to weight + wind			
Wind longitudinal reaction, Q_l			
Wind transverse reaction, Q_t			
Wind pressure, P_w			17.8372 psf
Equations			
$V_{wt} = P_w * G * (C_{f(shell)} * (\text{Projected shell area}) + C_{f(saddle)} * (\text{Projected saddle area}))$			
$V_{we} = P_w * G * (C_{f(shell)} * \pi * R_o^2 / 144 + C_{f(saddle)} * (\text{Projected saddle area}))$			
$Q_t = V_{wt} * H_s / (R_o * \sin(\theta / 2))$			
$Q_l = V_{we} * H_s / L_s$			
$Q = W + \max[Q_t, Q_l]$			
Results			
Operating	Right Saddle	$V_{wt} = 17.84 * 0.85 * (0.6 * 527.2743 + 2 * 1.5)$	4,842.07 lb _f
		$V_{we} = 17.84 * 0.85 * (0.5 * \pi * 72^2 / 144 + 2 * 22.8069)$	1,548.95 lb _f
		$Q_t = 4,842.07 * 78 / (66 * \sin(140 / 2))$	6,089.71 lb _f
		$Q_l = 1,548.95 * 78 / 598$	202.04 lb _f
		$Q = 310,287 + \max[6,089.71, 202.04]$	316,376.71 lb _f
	Left Saddle	$V_{wt} = 17.84 * 0.85 * (0.6 * 527.2743 + 2 * 1.5)$	4,842.07 lb _f
		$V_{we} = 17.84 * 0.85 * (0.5 * \pi * 72^2 / 144 + 2 * 22.8069)$	1,548.95 lb _f
		$Q_t = 4,842.07 * 78 / (66 * \sin(140 / 2))$	6,089.71 lb _f
		$Q_l = 1,548.95 * 78 / 598$	202.04 lb _f
		$Q = 308,872 + \max[6,089.71, 202.04]$	314,961.71 lb _f
Test	Right Saddle	$V_{wt} = 5.89 * 0.85 * (0.6 * 527.2743 + 2 * 1.5)$	1,597.88 lb _f
		$V_{we} = 5.89 * 0.85 * (0.5 * \pi * 72^2 / 144 + 2 * 22.8069)$	511.15 lb _f
		$Q_t = 1,597.88 * 78 / (66 * \sin(140 / 2))$	2,009.6 lb _f
		$Q_l = 511.15 * 78 / 598$	66.67 lb _f
		$Q = 310,325 + \max[2,009.6, 66.67]$	312,334.6 lb _f
		$V_{wt} = 5.89 * 0.85 * (0.6 * 527.2743 + 2 * 1.5)$	1,597.88 lb _f

	Left Saddle	$V_{wc} = 5.89 * 0.85 * (0.5 * \pi * 72^2 / 144 + 2 * 22.8069)$	511.15 lbf
		$Q_t = 1,597.88 * 78 / (66 * \sin(140 / 2))$	2,009.6 lbf
		$Q_l = 511.15 * 78 / 598$	66.67 lbf
		$Q = 308,926 + \max[2,009.6, 66.67]$	310,935.6 lbf

Load Case 1: Seismic, Operating

Longitudinal stress between saddles (Seismic, Operating, right saddle loading and geometry govern)

$$\begin{aligned}
 S_1 &= \pm 3 * K_1 * Q * (L / 12) / (\pi * R^2 * t) \\
 &= 3 * 0.1619 * 417,263.75 * (998 / 12) / (\pi * 65.5625^2 * 0.875) \\
 &= 1,426 \text{ psi}
 \end{aligned}$$

$$\begin{aligned}
 S_p &= P * R / (2 * t) \\
 &= 254.7 * 65.125 / (2 * 0.875) \\
 &= 9,479 \text{ psi}
 \end{aligned}$$

Maximum tensile stress $S_{1t} = S_1 + S_p = 10,905 \text{ psi}$

Maximum compressive stress (shut down) $S_{1c} = S_1 = 1,426 \text{ psi}$

Tensile stress is acceptable ($\leq 1.2 * S * E = 24,000 \text{ psi}$)

Compressive stress is acceptable ($\leq 1.2 * S_c = 17,057 \text{ psi}$)

Longitudinal stress at the right saddle (Seismic, Operating)

$$\begin{aligned}
 L_e &= 2 * (\text{Left head depth}) / 3 + L + 2 * (\text{Right head depth}) / 3 \\
 &= 2 * 33.425 / 3 + 998 + 2 * 33.425 / 3 \\
 &= 1,042.5667 \text{ in}
 \end{aligned}$$

Seismic vertical acceleration coefficient $m = 0.5333 * 0.1925 = 0.1027$

$$w = W_t * (1 + m) / L_e = 619,159 * (1 + 0.1027) / 1,042.5667 = 654.85 \text{ lbf/in}$$

Bending moment at the right saddle:

$$\begin{aligned}
 M_q &= w * (2 * H * A_r / 3 + A_r^2 / 2 - (R^2 - H^2) / 4) \\
 &= 654.85 * (2 * 33.425 * 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4) \\
 &= 15,485,248.6 \text{ lbf-in}
 \end{aligned}$$

$$\begin{aligned}
 S_2 &= \pm M_q * K_1' / (\pi * R^2 * t) \\
 &= 15,485,248.6 * 7.0845 / (\pi * 65.5625^2 * 0.875) \\
 &= 9,285 \text{ psi}
 \end{aligned}$$

$$\begin{aligned}
 S_p &= P * R / (2 * t) \\
 &= 254.7 * 65.125 / (2 * 0.875) \\
 &= 9,479 \text{ psi}
 \end{aligned}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = 18,763 \text{ psi}$

Maximum compressive stress (shut down) $S_{2c} = S_2 = 9,285 \text{ psi}$

Tensile stress is acceptable ($\leq 1.2 * S = 24,000 \text{ psi}$)

Compressive stress is acceptable ($\leq 1.2 * S_c = 17,057 \text{ psi}$)

Tangential shear stress in the shell (right saddle, Seismic, Operating)

$$\begin{aligned}
 Q_{\text{shear}} &= Q - w * (a + 2 * H / 3) \\
 &= 417,263.75 - 654.85 * (200 + 2 * 33.425 / 3) \\
 &= 271,701.25 \text{ lbf}
 \end{aligned}$$

$$\begin{aligned}
 S_3 &= K_{2.2} * Q_{\text{shear}} / (R * t) \\
 &= 0.9003 * 271,701.25 / (65.5625 * 0.875) \\
 &= 4,264 \text{ psi}
 \end{aligned}$$

Tangential shear stress is acceptable ($\leq 0.8 \cdot S = 16,000$ psi)

Circumferential stress at the right saddle horns (Seismic, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot (t + t_p) \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot (t^2 + t_p^2)) \\ &= -417,263.75 / (4 \cdot (0.875 + 0.375) \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0379 \cdot 417,263.75 / (2 \cdot (0.875^2 + 0.375^2)) \\ &= \underline{-28,971 \text{ psi}} \end{aligned}$$

Circumferential stress at saddle horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Circumferential stress at the right saddle wear plate horns (Seismic, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot t \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot t^2) \\ &= -417,263.75 / (4 \cdot 0.875 \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0305 \cdot 417,263.75 / (2 \cdot 0.875^2) \\ &= \underline{-28,927 \text{ psi}} \end{aligned}$$

Circumferential stress at wear plate horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Ring compression in shell over right saddle (Seismic, Operating)

$$\begin{aligned} S_5 &= K_5 \cdot Q / ((t + t_p) \cdot (t_s + 1.56 \cdot \text{Sqr}(R_o \cdot t_c))) \\ &= 0.6971 \cdot 417,263.75 / ((0.875 + 0.375) \cdot (0.75 + 1.56 \cdot \text{Sqr}(66 \cdot 1.25))) \\ &= \underline{15,597 \text{ psi}} \end{aligned}$$

Ring compression in shell is acceptable ($\leq 0.5 \cdot S_y = 18,000$ psi)

Saddle splitting load (right, Seismic, Operating)

Area resisting splitting force = Web area + wear plate area

$$\begin{aligned} A_e &= H_{eff} \cdot t_s + t_p \cdot W_p \\ &= 10.125 \cdot 0.75 + 0.375 \cdot 30 \\ &= 18.8438 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} S_6 &= K_8 \cdot Q / A_e \\ &= 0.2404 \cdot 417,263.75 / 18.8438 \\ &= \underline{5,323 \text{ psi}} \end{aligned}$$

Stress in saddle is acceptable ($\leq (2/3) \cdot S_s = 14,400$ psi)

Longitudinal stress at the left saddle (Seismic, Operating)

$$\begin{aligned} L_e &= 2 \cdot (\text{Left head depth}) / 3 + L + 2 \cdot (\text{Right head depth}) / 3 \\ &= 2 \cdot 33.425 / 3 + 998 + 2 \cdot 33.425 / 3 \\ &= 1,042.5667 \text{ in} \end{aligned}$$

Seismic vertical acceleration coefficient $m = 0.5333 \cdot 0.1925 = 0.1027$

$$w = W_t \cdot (1 + m) / L_e = 619,159 \cdot (1 + 0.1027) / 1,042.5667 = 654.85 \text{ lb/in}$$

Bending moment at the left saddle:

$$\begin{aligned} M_q &= w \cdot (2 \cdot H \cdot A_l / 3 + A_l^2 / 2 - (R^2 - H^2) / 4) \\ &= 654.85 \cdot (2 \cdot 33.425 \cdot 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4) \\ &= 15,485,248.6 \text{ lb-in} \end{aligned}$$

$$\begin{aligned} S_2 &= \pm M_q \cdot K_l' / (\pi \cdot R^2 \cdot t) \\ &= 15,485,248.6 \cdot 7.0845 / (\pi \cdot 65.5625^2 \cdot 0.875) \\ &= 9,285 \text{ psi} \end{aligned}$$

$$\begin{aligned} S_p &= P \cdot R / (2 \cdot t) \\ &= 254.7 \cdot 65.125 / (2 \cdot 0.875) \\ &= 9,479 \text{ psi} \end{aligned}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = \underline{18,763 \text{ psi}}$

Maximum compressive stress (shut down) $S_{2c} = S_2 = \underline{9,285 \text{ psi}}$

Tensile stress is acceptable ($\leq 1.2 \cdot S = 24,000$ psi)

Compressive stress is acceptable ($\leq 1.2 \cdot S_c = 17,057$ psi)

Tangential shear stress in the shell (left saddle, Seismic, Operating)

$$\begin{aligned} Q_{\text{shear}} &= Q - w \cdot (a + 2 \cdot H / 3) \\ &= 415,360.91 - 654.85 \cdot (200 + 2 \cdot 33.425 / 3) \\ &= 269,798.41 \text{ lbf} \end{aligned}$$

$$\begin{aligned} S_3 &= K_{2.2} \cdot Q_{\text{shear}} / (R \cdot t) \\ &= 0.9003 \cdot 269,798.41 / (65.5625 \cdot 0.875) \\ &= \underline{4,234} \text{ psi} \end{aligned}$$

Tangential shear stress is acceptable ($\leq 0.8 \cdot S = 16,000$ psi)

Circumferential stress at the left saddle horns (Seismic, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot (t + t_p) \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot (t^2 + t_p^2)) \\ &= -415,360.91 / (4 \cdot (0.875 + 0.375) \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0379 \cdot 415,360.91 / (2 \cdot (0.875^2 + 0.375^2)) \\ &= \underline{-28,839} \text{ psi} \end{aligned}$$

Circumferential stress at saddle horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Circumferential stress at the left saddle wear plate horns (Seismic, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot t \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot t^2) \\ &= -415,360.91 / (4 \cdot 0.875 \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0305 \cdot 415,360.91 / (2 \cdot 0.875^2) \\ &= \underline{-28,795} \text{ psi} \end{aligned}$$

Circumferential stress at wear plate horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Ring compression in shell over left saddle (Seismic, Operating)

$$\begin{aligned} S_5 &= K_5 \cdot Q / ((t + t_p) \cdot (t_s + 1.56 \cdot \text{Sqr}(R_o \cdot t_c))) \\ &= 0.6971 \cdot 415,360.91 / ((0.875 + 0.375) \cdot (0.75 + 1.56 \cdot \text{Sqr}(66 \cdot 1.25))) \\ &= \underline{15,526} \text{ psi} \end{aligned}$$

Ring compression in shell is acceptable ($\leq 0.5 \cdot S_y = 18,000$ psi)

Saddle splitting load (left, Seismic, Operating)

Area resisting splitting force = Web area + wear plate area

$$\begin{aligned} A_e &= H_{\text{eff}} \cdot t_s + t_p \cdot W_p \\ &= 10.125 \cdot 0.75 + 0.375 \cdot 30 \\ &= 18.8438 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} S_6 &= K_8 \cdot Q / A_e \\ &= 0.2404 \cdot 415,360.91 / 18.8438 \\ &= \underline{5,299} \text{ psi} \end{aligned}$$

Stress in saddle is acceptable ($\leq (2/3) \cdot S_s = 14,400$ psi)

Load Case 2: Wind, Operating

Longitudinal stress between saddles (Wind, Operating, right saddle loading and geometry govern)

$$\begin{aligned} S_1 &= \pm 3 \cdot K_1 \cdot Q \cdot (L / 12) / (\pi \cdot R^2 \cdot t) \\ &= 3 \cdot 0.1619 \cdot 316,376.71 \cdot (998 / 12) / (\pi \cdot 65.5625^2 \cdot 0.875) \\ &= 1,082 \text{ psi} \end{aligned}$$

$$\begin{aligned} S_p &= P \cdot R / (2 \cdot t) \\ &= 254.7 \cdot 65.125 / (2 \cdot 0.875) \\ &= 9,479 \text{ psi} \end{aligned}$$

Maximum tensile stress $S_{1t} = S_1 + S_p = \underline{10,560}$ psi

Maximum compressive stress (shut down) $S_{1c} = S_1 = \underline{1,082}$ psi

Tensile stress is acceptable ($\leq 1.2 \cdot S \cdot E = 24,000$ psi)

Compressive stress is acceptable ($\leq 1.2 \cdot S_c = 17,057$ psi)

Longitudinal stress at the right saddle (Wind, Operating)

$$\begin{aligned} L_e &= 2 \cdot (\text{Left head depth}) / 3 + L + 2 \cdot (\text{Right head depth}) / 3 \\ &= 2 \cdot 33.425 / 3 + 998 + 2 \cdot 33.425 / 3 \\ &= 1,042.5667 \text{ in} \end{aligned}$$

$$w = W_t / L_e = 619,159 / 1,042.5667 = 593.88 \text{ lb/in}$$

Bending moment at the right saddle:

$$\begin{aligned} M_q &= w \cdot (2 \cdot H \cdot A_r / 3 + A_r^2 / 2 - (R^2 - H^2) / 4) \\ &= 593.88 \cdot (2 \cdot 33.425 \cdot 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4) \\ &= 14,043,454 \text{ lb-in} \end{aligned}$$

$$\begin{aligned} S_2 &= \pm M_q \cdot K_1' / (\pi \cdot R^2 \cdot t) \\ &= 14,043,454 \cdot 7.0845 / (\pi \cdot 65.5625^2 \cdot 0.875) \\ &= 8,420 \text{ psi} \end{aligned}$$

$$\begin{aligned} S_p &= P \cdot R / (2 \cdot t) \\ &= 254.7 \cdot 65.125 / (2 \cdot 0.875) \\ &= 9,479 \text{ psi} \end{aligned}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = \underline{17,899}$ psi

Maximum compressive stress (shut down) $S_{2c} = S_2 = \underline{8,420}$ psi

Tensile stress is acceptable ($\leq 1.2 \cdot S = 24,000$ psi)

Compressive stress is acceptable ($\leq 1.2 \cdot S_c = 17,057$ psi)

Tangential shear stress in the shell (right saddle, Wind, Operating)

$$\begin{aligned} Q_{\text{shear}} &= Q - w \cdot (a + 2 \cdot H / 3) \\ &= 316,376.71 - 593.88 \cdot (200 + 2 \cdot 33.425 / 3) \\ &= 184,367.18 \text{ lb}_f \end{aligned}$$

$$\begin{aligned} S_3 &= K_{2.2} \cdot Q_{\text{shear}} / (R \cdot t) \\ &= 0.9003 \cdot 184,367.18 / (65.5625 \cdot 0.875) \\ &= \underline{2,893} \text{ psi} \end{aligned}$$

Tangential shear stress is acceptable ($\leq 0.8 \cdot S = 16,000$ psi)

Circumferential stress at the right saddle horns (Wind, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot (t + t_p) \cdot (b + 1.56 \cdot \text{Sqr}(R_0 \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot (t^2 + t_p^2)) \\ &= -316,376.71 / (4 \cdot (0.875 + 0.375) \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0379 \cdot 316,376.71 / (2 \cdot (0.875^2 + 0.375^2)) \\ &= \underline{-21,966} \text{ psi} \end{aligned}$$

Circumferential stress at saddle horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Circumferential stress at the right saddle wear plate horns (Wind, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot t \cdot (b + 1.56 \cdot \text{Sqr}(R_0 \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot t^2) \\ &= -316,376.71 / (4 \cdot 0.875 \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0305 \cdot 316,376.71 / (2 \cdot 0.875^2) \\ &= \underline{-21,933} \text{ psi} \end{aligned}$$

Circumferential stress at wear plate horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Ring compression in shell over right saddle (Wind, Operating)

$$\begin{aligned} S_5 &= K_5 \cdot Q / ((t + t_p) \cdot (t_s + 1.56 \cdot \text{Sqr}(R_0 \cdot t_c))) \\ &= 0.6971 \cdot 316,376.71 / ((0.875 + 0.375) \cdot (0.75 + 1.56 \cdot \text{Sqr}(66 \cdot 1.25))) \\ &= \underline{11,826} \text{ psi} \end{aligned}$$

Ring compression in shell is acceptable ($\leq 0.5 \cdot S_y = 18,000$ psi)

Saddle splitting load (right, Wind, Operating)

Area resisting splitting force = Web area + wear plate area

$$\begin{aligned} A_e &= H_{eff} \cdot t_s + t_p \cdot W_p \\ &= 10.125 \cdot 0.75 + 0.375 \cdot 30 \\ &= 18.8438 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} S_6 &= K_8 \cdot Q / A_e \\ &= 0.2404 \cdot 316,376.71 / 18.8438 \\ &= \underline{4,036} \text{ psi} \end{aligned}$$

Stress in saddle is acceptable ($\leq (2/3) \cdot S_s = 14,400$ psi)

Longitudinal stress at the left saddle (Wind, Operating)

$$\begin{aligned} L_e &= 2 \cdot (\text{Left head depth}) / 3 + L + 2 \cdot (\text{Right head depth}) / 3 \\ &= 2 \cdot 33.425 / 3 + 998 + 2 \cdot 33.425 / 3 \\ &= 1,042.5667 \text{ in} \end{aligned}$$

$$w = W_t / L_e = 619,159 / 1,042.5667 = 593.88 \text{ lb/in}$$

Bending moment at the left saddle:

$$\begin{aligned} M_q &= w \cdot (2 \cdot H \cdot A_1 / 3 + A_1^2 / 2 - (R^2 - H^2) / 4) \\ &= 593.88 \cdot (2 \cdot 33.425 \cdot 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4) \\ &= 14,043,454 \text{ lb-in} \end{aligned}$$

$$\begin{aligned} S_2 &= \pm M_q \cdot K_1' / (\pi \cdot R^2 \cdot t) \\ &= 14,043,454 \cdot 7.0845 / (\pi \cdot 65.5625^2 \cdot 0.875) \\ &= 8,420 \text{ psi} \end{aligned}$$

$$\begin{aligned} S_p &= P \cdot R / (2 \cdot t) \\ &= 254.7 \cdot 65.125 / (2 \cdot 0.875) \\ &= 9,479 \text{ psi} \end{aligned}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = \underline{17,899}$ psi

Maximum compressive stress (shut down) $S_{2c} = S_2 = \underline{8,420}$ psi

Tensile stress is acceptable ($\leq 1.2 \cdot S = 24,000$ psi)

Compressive stress is acceptable ($\leq 1.2 \cdot S_c = 17,057$ psi)

Tangential shear stress in the shell (left saddle, Wind, Operating)

$$\begin{aligned} Q_{\text{shear}} &= Q - w \cdot (a + 2 \cdot H / 3) \\ &= 314,961.71 - 593.88 \cdot (200 + 2 \cdot 33.425 / 3) \\ &= 182,952.18 \text{ lb}_f \end{aligned}$$

$$\begin{aligned} S_3 &= K_{2.2} \cdot Q_{\text{shear}} / (R \cdot t) \\ &= 0.9003 \cdot 182,952.18 / (65.5625 \cdot 0.875) \\ &= \underline{2,871} \text{ psi} \end{aligned}$$

Tangential shear stress is acceptable ($\leq 0.8 \cdot S = 16,000$ psi)

Circumferential stress at the left saddle horns (Wind, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot (t + t_p) \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot (t^2 + t_p^2)) \\ &= -314,961.71 / (4 \cdot (0.875 + 0.375) \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0379 \cdot 314,961.71 / (2 \cdot (0.875^2 + 0.375^2)) \\ &= \underline{-21,868} \text{ psi} \end{aligned}$$

Circumferential stress at saddle horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Circumferential stress at the left saddle wear plate horns (Wind, Operating)

$$S_4 = -Q / (4 \cdot t \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot t^2)$$

$$= -314,961.71 / (4 * 0.875 * (18 + 1.56 * \text{Sqr}(66 * 0.875))) - 3 * 0.0305 * 314,961.71 / (2 * 0.875^2)$$

$$= \underline{-21,835} \text{ psi}$$

Circumferential stress at wear plate horns is acceptable ($\leq 1.5 * S_a = 30,000 \text{ psi}$)

Ring compression in shell over left saddle (Wind, Operating)

$$S_5 = K_5 * Q / ((t + t_p) * (t_s + 1.56 * \text{Sqr}(R_o * t_c)))$$

$$= 0.6971 * 314,961.71 / ((0.875 + 0.375) * (0.75 + 1.56 * \text{Sqr}(66 * 1.25)))$$

$$= \underline{11,773} \text{ psi}$$

Ring compression in shell is acceptable ($\leq 0.5 * S_y = 18,000 \text{ psi}$)

Saddle splitting load (left, Wind, Operating)

Area resisting splitting force = Web area + wear plate area

$$A_e = H_{\text{eff}} * t_s + t_p * W_p$$

$$= 10.125 * 0.75 + 0.375 * 30$$

$$= 18.8438 \text{ in}^2$$

$$S_6 = K_8 * Q / A_e$$

$$= 0.2404 * 314,961.71 / 18.8438$$

$$= \underline{4,018} \text{ psi}$$

Stress in saddle is acceptable ($\leq (2 / 3) * S_s = 14,400 \text{ psi}$)

Load Case 3: Wind, Test

Longitudinal stress between saddles (Wind, Test, right saddle loading and geometry govern)

$$S_1 = \pm 3 * K_1 * Q * (L / 12) / (\pi * R^2 * t)$$

$$= 3 * 0.1619 * 312,334.6 * (998 / 12) / (\pi * 65.5625^2 * 0.875)$$

$$= \underline{1,068} \text{ psi}$$

$$S_p = P * R / (2 * t)$$

$$= 330.17 * 65.125 / (2 * 0.875)$$

$$= \underline{12,287} \text{ psi}$$

Maximum tensile stress $S_{1t} = S_1 + S_p = \underline{13,355} \text{ psi}$

Maximum compressive stress (shut down) $S_{1c} = S_1 = \underline{1,068} \text{ psi}$

Tensile stress is acceptable ($\leq 0.9 * S_y * E = 34,200 \text{ psi}$)

Compressive stress is acceptable ($\leq 1.2 * S_c = 17,057 \text{ psi}$)

Longitudinal stress at the right saddle (Wind, Test)

$$L_e = 2 * (\text{Left head depth}) / 3 + L + 2 * (\text{Right head depth}) / 3$$

$$= 2 * 33.425 / 3 + 998 + 2 * 33.425 / 3$$

$$= \underline{1,042.5667} \text{ in}$$

$$w = W_t / L_e = 619,251 / 1,042.5667 = 593.97 \text{ lb/in}$$

Bending moment at the right saddle:

$$M_q = w * (2 * H * A_r / 3 + A_r^2 / 2 - (R^2 - H^2) / 4)$$

$$= 593.97 * (2 * 33.425 * 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4)$$

$$= \underline{14,045,540.6} \text{ lb-in}$$

$$S_2 = \pm M_q * K_1' / (\pi * R^2 * t)$$

$$= 14,045,540.6 * 7.0845 / (\pi * 65.5625^2 * 0.875)$$

$$= \underline{8,421} \text{ psi}$$

$$S_p = P * R / (2 * t)$$

$$= 330.17 * 65.125 / (2 * 0.875)$$

$$= \underline{12,287} \text{ psi}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = 20,708$ psi

Maximum compressive stress (shut down) $S_{2c} = S_2 = 8,421$ psi

Tensile stress is acceptable ($\leq 0.9 \cdot S_y = 34,200$ psi)

Compressive stress is acceptable ($\leq 1.2 \cdot S_c = 17,057$ psi)

Tangential shear stress in the shell (right saddle, Wind, Test)

$$\begin{aligned} Q_{\text{shear}} &= Q - w \cdot (a + 2 \cdot H / 3) \\ &= 312,334.6 - 593.97 \cdot (200 + 2 \cdot 33.425 / 3) \\ &= 180,305.47 \text{ lb}_f \end{aligned}$$

$$\begin{aligned} S_3 &= K_{2.2} \cdot Q_{\text{shear}} / (R \cdot t) \\ &= 0.9003 \cdot 180,305.47 / (65.5625 \cdot 0.875) \\ &= 2,830 \text{ psi} \end{aligned}$$

Tangential shear stress is acceptable ($\leq 0.8 \cdot (0.9 \cdot S_y) = 27,360$ psi)

Circumferential stress at the right saddle horns (Wind, Test)

$$\begin{aligned} S_4 &= -Q / (4 \cdot (t + t_p) \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot (t^2 + t_p^2)) \\ &= -312,334.6 / (4 \cdot (0.875 + 0.375) \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0379 \cdot 312,334.6 / (2 \cdot (0.875^2 + 0.375^2)) \\ &= -21,685 \text{ psi} \end{aligned}$$

Circumferential stress at saddle horns is acceptable ($\leq 0.9 \cdot S_y = 34,200$ psi)

Circumferential stress at the right saddle wear plate horns (Wind, Test)

$$\begin{aligned} S_4 &= -Q / (4 \cdot t \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot t^2) \\ &= -312,334.6 / (4 \cdot 0.875 \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0305 \cdot 312,334.6 / (2 \cdot 0.875^2) \\ &= -21,653 \text{ psi} \end{aligned}$$

Circumferential stress at wear plate horns is acceptable ($\leq 0.9 \cdot S_y = 34,200$ psi)

Ring compression in shell over right saddle (Wind, Test)

$$\begin{aligned} S_5 &= K_5 \cdot Q / ((t + t_p) \cdot (t_s + 1.56 \cdot \text{Sqr}(R_o \cdot t_c))) \\ &= 0.6971 \cdot 312,334.6 / ((0.875 + 0.375) \cdot (0.75 + 1.56 \cdot \text{Sqr}(66 \cdot 1.25))) \\ &= 11,675 \text{ psi} \end{aligned}$$

Ring compression in shell is acceptable ($\leq 0.9 \cdot S_y = 32,400$ psi)

Saddle splitting load (right, Wind, Test)

Area resisting splitting force = Web area + wear plate area

$$\begin{aligned} A_e &= H_{\text{eff}} \cdot t_s + t_p \cdot W_p \\ &= 10.125 \cdot 0.75 + 0.375 \cdot 30 \\ &= 18.8438 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} S_6 &= K_8 \cdot Q / A_e \\ &= 0.2404 \cdot 312,334.6 / 18.8438 \\ &= 3,985 \text{ psi} \end{aligned}$$

Stress in saddle is acceptable ($\leq 0.9 \cdot S_y = 32,400$ psi)

Longitudinal stress at the left saddle (Wind, Test)

$$\begin{aligned} L_e &= 2 \cdot (\text{Left head depth}) / 3 + L + 2 \cdot (\text{Right head depth}) / 3 \\ &= 2 \cdot 33.425 / 3 + 998 + 2 \cdot 33.425 / 3 \\ &= 1,042.5667 \text{ in} \end{aligned}$$

$$w = W_t / L_e = 619,251 / 1,042.5667 = 593.97 \text{ lb}_f/\text{in}$$

Bending moment at the left saddle:

$$\begin{aligned}
 M_q &= w \cdot (2 \cdot H \cdot A_l / 3 + A_l^2 / 2 - (R^2 - H^2) / 4) \\
 &= 593.97 \cdot (2 \cdot 33.425 \cdot 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4) \\
 &= 14,045,540.6 \text{ lb}\cdot\text{in}
 \end{aligned}$$

$$\begin{aligned}
 S_2 &= \pm M_q \cdot K_1' / (\pi \cdot R^2 \cdot t) \\
 &= 14,045,540.6 \cdot 7.0845 / (\pi \cdot 65.5625^2 \cdot 0.875) \\
 &= 8,421 \text{ psi}
 \end{aligned}$$

$$\begin{aligned}
 S_p &= P \cdot R / (2 \cdot t) \\
 &= 330.17 \cdot 65.125 / (2 \cdot 0.875) \\
 &= 12,287 \text{ psi}
 \end{aligned}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = 20,708 \text{ psi}$

Maximum compressive stress (shut down) $S_{2c} = S_2 = 8,421 \text{ psi}$

Tensile stress is acceptable ($\leq 0.9 \cdot S_y = 34,200 \text{ psi}$)

Compressive stress is acceptable ($\leq 1.2 \cdot S_c = 17,057 \text{ psi}$)

Tangential shear stress in the shell (left saddle, Wind, Test)

$$\begin{aligned}
 Q_{\text{shear}} &= Q - w \cdot (a + 2 \cdot H / 3) \\
 &= 310,935.6 - 593.97 \cdot (200 + 2 \cdot 33.425 / 3) \\
 &= 178,906.47 \text{ lb}_f
 \end{aligned}$$

$$\begin{aligned}
 S_3 &= K_{2.2} \cdot Q_{\text{shear}} / (R \cdot t) \\
 &= 0.9003 \cdot 178,906.47 / (65.5625 \cdot 0.875) \\
 &= 2,808 \text{ psi}
 \end{aligned}$$

Tangential shear stress is acceptable ($\leq 0.8 \cdot (0.9 \cdot S_y) = 27,360 \text{ psi}$)

Circumferential stress at the left saddle horns (Wind, Test)

$$\begin{aligned}
 S_4 &= -Q / (4 \cdot (t + t_p) \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot (t^2 + t_p^2)) \\
 &= -310,935.6 / (4 \cdot (0.875 + 0.375) \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0379 \cdot 310,935.6 / (2 \cdot (0.875^2 + 0.375^2)) \\
 &= -21,588 \text{ psi}
 \end{aligned}$$

Circumferential stress at saddle horns is acceptable ($\leq 0.9 \cdot S_y = 34,200 \text{ psi}$)

Circumferential stress at the left saddle wear plate horns (Wind, Test)

$$\begin{aligned}
 S_4 &= -Q / (4 \cdot t \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot t^2) \\
 &= -310,935.6 / (4 \cdot 0.875 \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0305 \cdot 310,935.6 / (2 \cdot 0.875^2) \\
 &= -21,556 \text{ psi}
 \end{aligned}$$

Circumferential stress at wear plate horns is acceptable ($\leq 0.9 \cdot S_y = 34,200 \text{ psi}$)

Ring compression in shell over left saddle (Wind, Test)

$$\begin{aligned}
 S_5 &= K_5 \cdot Q / ((t + t_p) \cdot (t_s + 1.56 \cdot \text{Sqr}(R_o \cdot t_c))) \\
 &= 0.6971 \cdot 310,935.6 / ((0.875 + 0.375) \cdot (0.75 + 1.56 \cdot \text{Sqr}(66 \cdot 1.25))) \\
 &= 11,623 \text{ psi}
 \end{aligned}$$

Ring compression in shell is acceptable ($\leq 0.9 \cdot S_y = 32,400 \text{ psi}$)

Saddle splitting load (left, Wind, Test)

Area resisting splitting force = Web area + wear plate area

$$\begin{aligned}
 A_e &= H_{\text{eff}} \cdot t_s + t_p \cdot W_p \\
 &= 10.125 \cdot 0.75 + 0.375 \cdot 30 \\
 &= 18.8438 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 S_6 &= K_8 \cdot Q / A_e \\
 &= 0.2404 \cdot 310,935.6 / 18.8438 \\
 &= 3,967 \text{ psi}
 \end{aligned}$$

Stress in saddle is acceptable ($\leq 0.9 \cdot S_y = 32,400$ psi)

Load Case 4: Weight, Operating

Longitudinal stress between saddles (Weight, Operating, right saddle loading and geometry govern)

$$\begin{aligned} S_1 &= \pm 3 \cdot K_1 \cdot Q \cdot (L / 12) / (\pi \cdot R^2 \cdot t) \\ &= 3 \cdot 0.1619 \cdot 310,287 \cdot (998 / 12) / (\pi \cdot 65.5625^2 \cdot 0.875) \\ &= 1,061 \text{ psi} \end{aligned}$$

$$\begin{aligned} S_p &= P \cdot R / (2 \cdot t) \\ &= 254.7 \cdot 65.125 / (2 \cdot 0.875) \\ &= 9,479 \text{ psi} \end{aligned}$$

Maximum tensile stress $S_{1t} = S_1 + S_p = 10,539$ psi

Maximum compressive stress (shut down) $S_{1c} = S_1 = 1,061$ psi

Tensile stress is acceptable ($\leq S \cdot E = 20,000$ psi)

Compressive stress is acceptable ($\leq S_c = 14,214$ psi)

Longitudinal stress at the right saddle (Weight, Operating)

$$\begin{aligned} L_e &= 2 \cdot (\text{Left head depth}) / 3 + L + 2 \cdot (\text{Right head depth}) / 3 \\ &= 2 \cdot 33.425 / 3 + 998 + 2 \cdot 33.425 / 3 \\ &= 1,042.5667 \text{ in} \end{aligned}$$

$$w = W_t / L_e = 619,159 / 1,042.5667 = 593.88 \text{ lbf/in}$$

Bending moment at the right saddle:

$$\begin{aligned} M_q &= w \cdot (2 \cdot H \cdot A_r / 3 + A_r^2 / 2 - (R^2 - H^2) / 4) \\ &= 593.88 \cdot (2 \cdot 33.425 \cdot 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4) \\ &= 14,043,454 \text{ lbf-in} \end{aligned}$$

$$\begin{aligned} S_2 &= \pm M_q \cdot K_1' / (\pi \cdot R^2 \cdot t) \\ &= 14,043,454 \cdot 7.0845 / (\pi \cdot 65.5625^2 \cdot 0.875) \\ &= 8,420 \text{ psi} \end{aligned}$$

$$\begin{aligned} S_p &= P \cdot R / (2 \cdot t) \\ &= 254.7 \cdot 65.125 / (2 \cdot 0.875) \\ &= 9,479 \text{ psi} \end{aligned}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = 17,899$ psi

Maximum compressive stress (shut down) $S_{2c} = S_2 = 8,420$ psi

Tensile stress is acceptable ($\leq S = 20,000$ psi)

Compressive stress is acceptable ($\leq S_c = 14,214$ psi)

Tangential shear stress in the shell (right saddle, Weight, Operating)

$$\begin{aligned} Q_{\text{shear}} &= Q - w \cdot (a + 2 \cdot H / 3) \\ &= 310,287 - 593.88 \cdot (200 + 2 \cdot 33.425 / 3) \\ &= 178,277.48 \text{ lbf} \end{aligned}$$

$$\begin{aligned} S_3 &= K_{2.2} \cdot Q_{\text{shear}} / (R \cdot t) \\ &= 0.9003 \cdot 178,277.48 / (65.5625 \cdot 0.875) \\ &= 2,798 \text{ psi} \end{aligned}$$

Tangential shear stress is acceptable ($\leq 0.8 \cdot S = 16,000$ psi)

Circumferential stress at the right saddle horns (Weight, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot (t + t_p) \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot (t^2 + t_p^2)) \\ &= -310,287 / (4 \cdot (0.875 + 0.375) \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0379 \cdot 310,287 / (2 \cdot (0.875^2 + 0.375^2)) \\ &= -21,543 \text{ psi} \end{aligned}$$

Circumferential stress at saddle horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Circumferential stress at the right saddle wear plate horns (Weight, Operating)

$$\begin{aligned} S_4 &= -Q / (4 \cdot t \cdot (b + 1.56 \cdot \text{Sqr}(R_o \cdot t))) - 3 \cdot K_3 \cdot Q / (2 \cdot t^2) \\ &= -310,287 / (4 \cdot 0.875 \cdot (18 + 1.56 \cdot \text{Sqr}(66 \cdot 0.875))) - 3 \cdot 0.0305 \cdot 310,287 / (2 \cdot 0.875^2) \\ &= \underline{-21,511} \text{ psi} \end{aligned}$$

Circumferential stress at wear plate horns is acceptable ($\leq 1.5 \cdot S_a = 30,000$ psi)

Ring compression in shell over right saddle (Weight, Operating)

$$\begin{aligned} S_5 &= K_5 \cdot Q / ((t + t_p) \cdot (t_s + 1.56 \cdot \text{Sqr}(R_o \cdot t_c))) \\ &= 0.6971 \cdot 310,287 / ((0.875 + 0.375) \cdot (0.75 + 1.56 \cdot \text{Sqr}(66 \cdot 1.25))) \\ &= \underline{11,598} \text{ psi} \end{aligned}$$

Ring compression in shell is acceptable ($\leq 0.5 \cdot S_y = 18,000$ psi)

Saddle splitting load (right, Weight, Operating)

Area resisting splitting force = Web area + wear plate area

$$\begin{aligned} A_e &= H_{eff} \cdot t_s + t_p \cdot W_p \\ &= 10.125 \cdot 0.75 + 0.375 \cdot 30 \\ &= 18.8438 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} S_6 &= K_8 \cdot Q / A_e \\ &= 0.2404 \cdot 310,287 / 18.8438 \\ &= \underline{3,959} \text{ psi} \end{aligned}$$

Stress in saddle is acceptable ($\leq (2/3) \cdot S_s = 14,400$ psi)

Longitudinal stress at the left saddle (Weight, Operating)

$$\begin{aligned} L_e &= 2 \cdot (\text{Left head depth}) / 3 + L + 2 \cdot (\text{Right head depth}) / 3 \\ &= 2 \cdot 33.425 / 3 + 998 + 2 \cdot 33.425 / 3 \\ &= 1,042.5667 \text{ in} \end{aligned}$$

$$w = W_t / L_e = 619,159 / 1,042.5667 = 593.88 \text{ lb/in}$$

Bending moment at the left saddle:

$$\begin{aligned} M_q &= w \cdot (2 \cdot H \cdot A_l / 3 + A_l^2 / 2 - (R^2 - H^2) / 4) \\ &= 593.88 \cdot (2 \cdot 33.425 \cdot 200 / 3 + 200^2 / 2 - (66^2 - 33.425^2) / 4) \\ &= 14,043,454 \text{ lb-in} \end{aligned}$$

$$\begin{aligned} S_2 &= \pm M_q \cdot K_1' / (\pi \cdot R^2 \cdot t) \\ &= 14,043,454 \cdot 7.0845 / (\pi \cdot 65.5625^2 \cdot 0.875) \\ &= 8,420 \text{ psi} \end{aligned}$$

$$\begin{aligned} S_p &= P \cdot R / (2 \cdot t) \\ &= 254.7 \cdot 65.125 / (2 \cdot 0.875) \\ &= 9,479 \text{ psi} \end{aligned}$$

Maximum tensile stress $S_{2t} = S_2 + S_p = \underline{17,899}$ psi

Maximum compressive stress (shut down) $S_{2c} = S_2 = \underline{8,420}$ psi

Tensile stress is acceptable ($\leq S = 20,000$ psi)

Compressive stress is acceptable ($\leq S_c = 14,214$ psi)

Tangential shear stress in the shell (left saddle, Weight, Operating)

$$\begin{aligned} Q_{\text{shear}} &= Q - w \cdot (a + 2 \cdot H / 3) \\ &= 308,872 - 593.88 \cdot (200 + 2 \cdot 33.425 / 3) \\ &= 176,862.48 \text{ lb}_f \end{aligned}$$

$$S_3 = K_{2.2} \cdot Q_{\text{shear}} / (R \cdot t)$$

$$= 0.9003 * 176,862.48 / (65.5625 * 0.875)$$

$$= \underline{2,776} \text{ psi}$$

Tangential shear stress is acceptable ($\leq 0.8 * S = 16,000 \text{ psi}$)

Circumferential stress at the left saddle horns (Weight, Operating)

$$S_4 = -Q / (4 * (t + t_p) * (b + 1.56 * \text{Sqr}(R_o * t))) - 3 * K_3 * Q / (2 * (t^2 + t_p^2))$$

$$= -308,872 / (4 * (0.875 + 0.375) * (18 + 1.56 * \text{Sqr}(66 * 0.875))) - 3 * 0.0379 * 308,872 / (2 * (0.875^2 + 0.375^2))$$

$$= \underline{-21,445} \text{ psi}$$

Circumferential stress at saddle horns is acceptable ($\leq 1.5 * S_a = 30,000 \text{ psi}$)

Circumferential stress at the left saddle wear plate horns (Weight, Operating)

$$S_4 = -Q / (4 * t * (b + 1.56 * \text{Sqr}(R_o * t))) - 3 * K_3 * Q / (2 * t^2)$$

$$= -308,872 / (4 * 0.875 * (18 + 1.56 * \text{Sqr}(66 * 0.875))) - 3 * 0.0305 * 308,872 / (2 * 0.875^2)$$

$$= \underline{-21,413} \text{ psi}$$

Circumferential stress at wear plate horns is acceptable ($\leq 1.5 * S_a = 30,000 \text{ psi}$)

Ring compression in shell over left saddle (Weight, Operating)

$$S_5 = K_5 * Q / ((t + t_p) * (t_s + 1.56 * \text{Sqr}(R_o * t_c)))$$

$$= 0.6971 * 308,872 / ((0.875 + 0.375) * (0.75 + 1.56 * \text{Sqr}(66 * 1.25)))$$

$$= \underline{11,545} \text{ psi}$$

Ring compression in shell is acceptable ($\leq 0.5 * S_y = 18,000 \text{ psi}$)

Saddle splitting load (left, Weight, Operating)

Area resisting splitting force = Web area + wear plate area

$$A_e = H_{eff} * t_s + t_p * W_p$$

$$= 10.125 * 0.75 + 0.375 * 30$$

$$= 18.8438 \text{ in}^2$$

$$S_6 = K_8 * Q / A_e$$

$$= 0.2404 * 308,872 / 18.8438$$

$$= \underline{3,940} \text{ psi}$$

Stress in saddle is acceptable ($\leq (2 / 3) * S_s = 14,400 \text{ psi}$)

Shear stress in anchor bolting, one end slotted

Maximum seismic or wind base shear = 119,188.11 lb_F

Thermal expansion base shear = $W * \mu = 313,432 * 0.45 = 141,044.4 \text{ lb}_F$

Corroded root area for a 2.75" series 8 threaded bolt = 5.259 in² (4 per saddle)

Bolt shear stress = $141,044.4 / (5.259 * 1 * 4) = 6,705 \text{ psi}$

Anchor bolt stress is acceptable ($\leq 10,000 \text{ psi}$)

Shear stress in anchor bolting, transverse

Maximum seismic or wind base shear = 119,188.11 lb_F

Corroded root area for a 2.75" series 8 threaded bolt = 5.259 in² (4 per saddle)

Bolt shear stress = $119,188.11 / (5.259 * 2 * 4) = 2,833 \text{ psi}$

Anchor bolt stress is acceptable ($\leq 10,000 \text{ psi}$)

Web plate buckling check (Escanoe pg 251)

Allowable compressive stress S_c is the lesser of 21,600 or 42,963 psi: (21,600)

$$S_c = K_1 * \pi^2 * E / (12 * (1 - 0.3^2) * (d_i / t_s)^2)$$

$$= 1.28 * \pi^2 * 29E+06 / (12 * (1 - 0.3^2) * (20.9583 / 0.75)^2)$$

$$= 42,963 \text{ psi}$$

Allowable compressive load on the saddle

$$b_c = d_i * t_s / (d_i * t_s + 2 * t_w * (b - 1))$$

$$= 20.9583 * 0.75 / (20.9583 * 0.75 + 2 * 0.75 * (18 - 1))$$

$$= 0.3814$$

$$F_b = n * (A_s + 2 * b_c * t_s) * S_c$$

$$= 7 * (12.9375 + 2 * 0.3814 * 0.75) * 21,600$$

$$= 2,042,640.07 \text{ lb}_f$$

Saddle loading of 420,408.75 lb_f is $\leq F_b$; satisfactory.

Primary bending + axial stress in the saddle due to end loads (assumes one saddle slotted)

$$\sigma_b = V * (H_s - x_o) * y / I + Q / A$$

$$= 119,188.11 * (78 - 50.7638) * 9 / 2,553.35 + 417,263.75 / 183.5921$$

$$= 13,715 \text{ psi}$$

The primary bending + axial stress in the saddle $\leq S_s = 21,600$ psi; satisfactory.

Secondary bending + axial stress in the saddle due to end loads (includes thermal expansion, assumes one saddle slotted)

$$\sigma_b = V * (H_s - x_o) * y / I + Q / A$$

$$= 260,232.51 * (78 - 50.7638) * 9 / 2,553.35 + 417,263.75 / 183.5921$$

$$= 27,256 \text{ psi}$$

The secondary bending + axial stress in the saddle $\leq 2 * S_y = 72,000$ psi; satisfactory.

Saddle base plate thickness check (Roark sixth edition, Table 26, case 7a)

where $a = 20.9583$, $b = 10.625$ in

$$t_b = (\beta_1 * q * b^2 / (1.5 * S_a))^{0.5}$$

$$= (1.7753 * 148 * 10.625^2 / (1.5 * 21,600))^{0.5}$$

$$= 0.9572 \text{ in}$$

The base plate thickness of 1.5 in is adequate.

Foundation bearing check

$$S_f = Q_{\max} / (F * E)$$

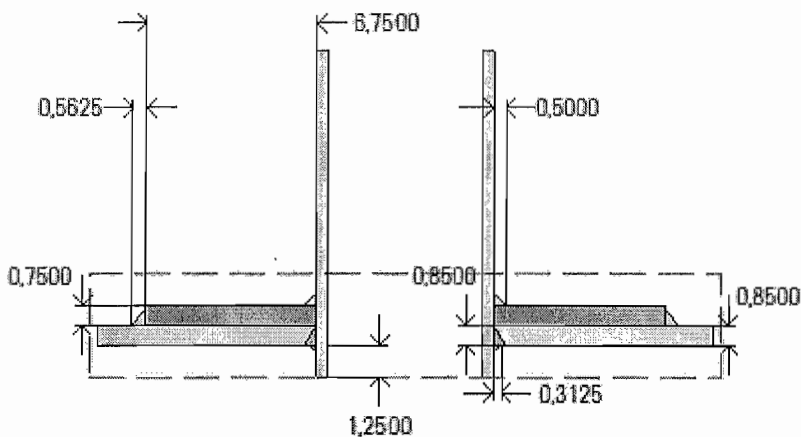
$$= 420,408.75 / (22 * 129)$$

$$= 148 \text{ psi}$$

Concrete bearing stress $\leq 1,350$ psi ; satisfactory.

Nozzle M1 - 20" 150# Manway (M1)

ASME Section VIII Division 1, 2017 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Right Head
Orientation	0°
End of nozzle to datum line	-57.5"
Calculated as hillside	No
Distance to head center, R	0"
Passes through a Category A joint	No

Nozzle

Description	NPS 20 Sch 30 (XS)
Access opening	Yes
Material specification	SA-106 B Smls pipe (II-D p. 14, ln. 10)
Inside diameter, new	19"
Pipe nominal wall thickness	0.5"
Pipe minimum wall thickness ¹	0.4375"
Corrosion allowance	0"
Projection available outside vessel, L _{pr}	4.7709"
Internal projection, h _{new}	1.25"
Projection available outside vessel to flange face, L _f	10.4609"
Local vessel minimum thickness	0.85"
Liquid static head included	2.35 psi
Longitudinal joint efficiency	0.85

Reinforcing Pad

Material specification	SA-516 70 (II-D p. 18, ln. 33)
------------------------	--------------------------------

Diameter, D_p	33.5"
Thickness, t_c	0.75"
Is split	No
Welds	
Inner fillet, Leg ₄₁	0.5"
Outer fillet, Leg ₄₂	0.5625"
Lower fillet, Leg ₄₃	0.3125"
Nozzle to vessel groove weld	0.85"
Pad groove weld	0"

¹Pipe minimum thickness = nominal thickness times pipe tolerance factor of 0.875.

ASME B16.5-2013 Flange	
Description	NPS 20 Class 150 WN A105
Bolt Material	SA-193 B7 Bolt $\leq 2 \frac{1}{2}$ (II-D p. 388, ln. 32)
Blind included	Yes
Rated MDMT	-31.5°F
Liquid static head	2.35 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Circumferential joint radiography	None UW-11(c) Type 1
Bore diameter, B (specified by purchaser)	19"
Gasket	
Description	Klingsil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -31.5°F (Coincident ratio = 0.8854) Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle	
$t_r = 252.35 * 9.5 / (17,100 * 0.85 - 0.6 * 252.35) =$	0.1667"
Stress ratio = $t_r * E^* / (t_n - c) = 0.1667 * 0.85 / (0.4375 - 0) =$	0.3238
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

UCS-66 Material Toughness Requirements Pad	
Governing thickness, $t_g =$	0.75"

MDMT =

-20°F

Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F.

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 252.35 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
14.2768	15.0001	1.9662	1.2264	1.0688	10.125	0.6137	0.1667	0.4375

UG-41 Weld Failure Path Analysis Summary (lb _f)						
All failure paths are stronger than the applicable weld loads						
Weld load W	Weld load W ₁₋₁	Path 1-1 strength	Weld load W ₂₋₂	Path 2-2 strength	Weld load W ₃₋₃	Path 3-3 strength
247,995.38	237,632	473,400.7	66,384	609,090.02	275,212	767,549.99

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to pad fillet (Leg ₄₁)	0.35	0.35	weld size is adequate
Pad to shell fillet (Leg ₄₂)	0.375	0.3938	weld size is adequate

Calculations for internal pressure 252.35 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(19, 9.5 + (0.5 - 0) + (0.85 - 0)) \\
 &= 19 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.85 - 0), 2.5*(0.5 - 0) + 0.75) \\
 &= 2 \text{ in}
 \end{aligned}$$

Inner Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_I &= \text{MIN}(h, 2.5*(t - C), 2.5*(t_i - C_n - C)) \\
 &= \text{MIN}(1.25, 2.5*(0.85 - 0), 2.5*(0.5 - 0 - 0)) \\
 &= 1.25 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_m &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 252.3508 \cdot 9.5 / (17,100 \cdot 1 - 0.6 \cdot 252.3508) \\
 &= 0.1414 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)(c)

$$\begin{aligned}
 t_r &= P \cdot K_1 \cdot D_o / (2 \cdot S \cdot E + 0.8 \cdot P) \\
 &= 252.3508 \cdot 0.9 \cdot 132 / (2 \cdot 20,000 \cdot 1 + 0.8 \cdot 252.3508) \\
 &= 0.7457 \text{ in}
 \end{aligned}$$

Required thickness t_r per Interpretation VIII-1-07-50

$$\begin{aligned}
 t_r &= P \cdot D_o \cdot K / (2 \cdot S \cdot E + 2 \cdot P \cdot (K - 0.1)) \\
 &= 252.35 \cdot 132 \cdot 1 / (2 \cdot 20,000 \cdot 1 + 2 \cdot 252.35 \cdot (1 - 0.1)) \\
 &= 0.8234"
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: $S_n = 17,100$, $S_v = 20,000$, $S_p = 20,000$ psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 0.855$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 0.855$$

$$f_{r3} = \text{lesser of } f_{r2} \text{ or } S_p / S_v = 0.855$$

$$f_{r4} = \text{lesser of } 1 \text{ or } S_p / S_v = 1$$

$$\begin{aligned}
 A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\
 &= 19 \cdot 0.7457 \cdot 1 + 2 \cdot 0.5 \cdot 0.7457 \cdot 1 \cdot (1 - 0.855) \\
 &= \underline{14.2768} \text{ in}^2
 \end{aligned}$$

Area available from FIG. UG-37.1

$$A_1 = \text{larger of the following} = \underline{1.9662} \text{ in}^2$$

$$\begin{aligned}
 &= d \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\
 &= 19 \cdot (1 \cdot 0.85 - 1 \cdot 0.7457) - 2 \cdot 0.5 \cdot (1 \cdot 0.85 - 1 \cdot 0.7457) \cdot (1 - 0.855) \\
 &= 1.9662 \text{ in}^2 \\
 &= 2 \cdot (t + t_n) \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\
 &= 2 \cdot (0.85 + 0.5) \cdot (1 \cdot 0.85 - 1 \cdot 0.7457) - 2 \cdot 0.5 \cdot (1 \cdot 0.85 - 1 \cdot 0.7457) \cdot (1 - 0.855) \\
 &= 0.2664 \text{ in}^2
 \end{aligned}$$

$$A_2 = \text{smaller of the following} = \underline{1.2264} \text{ in}^2$$

$$\begin{aligned}
 &= 5 \cdot (t_n - t_{rn}) \cdot f_{r2} \cdot t \\
 &= 5 \cdot (0.5 - 0.1414) \cdot 0.855 \cdot 0.85 \\
 &= 1.3031 \text{ in}^2 \\
 &= 2 \cdot (t_n - t_{rn}) \cdot (2.5 \cdot t_n + t_c) \cdot f_{r2} \\
 &= 2 \cdot (0.5 - 0.1414) \cdot (2.5 \cdot 0.5 + 0.75) \cdot 0.855 \\
 &= 1.2264 \text{ in}^2
 \end{aligned}$$

$$A_3 = \text{smaller of the following} = \underline{1.0688} \text{ in}^2$$

$$\begin{aligned}
 &= 5 \cdot t \cdot t_i \cdot f_{r2} \\
 &= 5 \cdot 0.85 \cdot 0.5 \cdot 0.855 \\
 &= \underline{1.8169} \text{ in}^2 \\
 &= 5 \cdot t_i \cdot t_j \cdot f_{r2} \\
 &= 5 \cdot 0.5 \cdot 0.5 \cdot 0.855 \\
 &= \underline{1.0688} \text{ in}^2 \\
 &= 2 \cdot h \cdot t_i \cdot f_{r2} \\
 &= 2 \cdot 1.25 \cdot 0.5 \cdot 0.855 \\
 &= \underline{1.0688} \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 A_{41} &= \text{Leg}^2 \cdot f_{r3} \\
 &= 0.5^2 \cdot 0.855 \\
 &= \underline{0.2138} \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 A_{42} &= \text{Leg}^2 * f_{r4} \\
 &= 0.5625^2 * 1 \\
 &= \underline{0.3164} \text{ in}^2 \\
 A_{43} &= \text{Leg}^2 * f_{r2} \\
 &= 0.3125^2 * 0.855 \\
 &= \underline{0.0835} \text{ in}^2 \\
 A_5 &= (D_p - d - 2 * t_n) * t_e * f_{r4} \\
 &= (33.5 - 19 - 2 * 0.5) * 0.75 * 1 \\
 &= \underline{10.125} \text{ in}^2 \\
 \text{Area} &= A_1 + A_2 + A_3 + A_{41} + A_{42} + A_{43} + A_5 \\
 &= 1.9662 + 1.2264 + 1.0688 + 0.2138 + 0.3164 + 0.0835 + 10.125 \\
 &= \underline{15.0001} \text{ in}^2
 \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c)(2) Weld Check

$$\begin{aligned}
 \text{Inner fillet: } t_{\min} &= \text{lesser of } 0.75 \text{ or } t_n \text{ or } t_e = 0.5 \text{ in} \\
 t_{w(\min)} &= 0.7 * t_{\min} = \underline{0.35} \text{ in} \\
 t_{w(\text{actual})} &= 0.7 * \text{Leg} = 0.7 * 0.5 = 0.35 \text{ in} \\
 \text{Outer fillet: } t_{\min} &= \text{lesser of } 0.75 \text{ or } t_e \text{ or } t = 0.75 \text{ in} \\
 t_{w(\min)} &= 0.5 * t_{\min} = \underline{0.375} \text{ in} \\
 t_{w(\text{actual})} &= 0.7 * \text{Leg} = 0.7 * 0.5625 = 0.3938 \text{ in}
 \end{aligned}$$

UG-45 Nozzle Neck Thickness Check (Access Opening)

Interpretation VIII-1-83-66 has been applied.

$$\begin{aligned}
 t_a \text{ UG-27} &= P * R_n / (S_n * E - 0.6 * P) + \text{Corrosion} \\
 &= 252.3508 * 9.5 / (17,100 * 0.85 - 0.6 * 252.3508) + 0 \\
 &= 0.1667 \text{ in} \\
 t_a &= \max[t_a \text{ UG-27}, t_a \text{ UG-22}] \\
 &= \max[0.1667, 0] \\
 &= 0.1667 \text{ in}
 \end{aligned}$$

$$\text{Available nozzle wall thickness new, } t_n = 0.875 * 0.5 = 0.4375 \text{ in}$$

The nozzle neck thickness is adequate.

Allowable stresses in joints UG-45 and UW-15(c)

$$\begin{aligned}
 \text{Groove weld in tension: } &0.74 * 20,000 = 14,800 \text{ psi} \\
 \text{Nozzle wall in shear: } &0.7 * 17,100 = 11,970 \text{ psi} \\
 \text{Inner fillet weld in shear: } &0.49 * 17,100 = 8,379 \text{ psi} \\
 \text{Outer fillet weld in shear: } &0.49 * 20,000 = 9,800 \text{ psi} \\
 \text{Lower fillet weld in shear: } &0.49 * 17,100 = 8,379 \text{ psi}
 \end{aligned}$$

Strength of welded joints:

$$(1) \text{ Inner fillet weld in shear}$$

$$(\pi / 2) * \text{Nozzle OD} * \text{Leg} * S_i = (\pi / 2) * 20 * 0.5 * 8,379 = 131,617.02 \text{ lb}_f$$

$$(2) \text{ Outer fillet weld in shear}$$

$$(\pi / 2) * \text{Pad OD} * \text{Leg} * S_o = (\pi / 2) * 33.5 * 0.5625 * 9,800 = 290,076.99 \text{ lb}_f$$

(3) Nozzle wall in shear

$$(\pi / 2) * \text{Mean nozzle dia} * t_n * S_n = (\pi / 2) * 19.5 * 0.5 * 11,970 = 183,323.71 \text{ lb}_f$$

(4) Groove weld in tension

$$(\pi / 2) * \text{Nozzle OD} * t_w * S_g = (\pi / 2) * 20 * 0.85 * 14,800 = 395,212.35 \text{ lb}_f$$

(5) Lower fillet weld in shear

$$(\pi / 2) * \text{Nozzle OD} * \text{Leg} * S_l = (\pi / 2) * 20 * 0.3125 * 8,379 = 82,260.64 \text{ lb}_f$$

Loading on welds per UG-41(b)(1)

$$\begin{aligned} W &= (A - A_1 + 2 * t_n * f_{r1} * (E_1 * t - F * t_r)) * S_v \\ &= (14.2768 - 1.9662 + 2 * 0.5 * 0.855 * (1 * 0.85 - 1 * 0.7457)) * 20,000 \\ &= \underline{247,995.38 \text{ lb}_f} \end{aligned}$$

$$\begin{aligned} W_{1-1} &= (A_2 + A_5 + A_{41} + A_{42}) * S_v \\ &= (1.2264 + 10.125 + 0.2138 + 0.3164) * 20,000 \\ &= \underline{237,632 \text{ lb}_f} \end{aligned}$$

$$\begin{aligned} W_{2-2} &= (A_2 + A_3 + A_{41} + A_{43} + 2 * t_n * t * f_{r1}) * S_v \\ &= (1.2264 + 1.0688 + 0.2138 + 0.0835 + 2 * 0.5 * 0.85 * 0.855) * 20,000 \\ &= \underline{66,384 \text{ lb}_f} \end{aligned}$$

$$\begin{aligned} W_{3-3} &= (A_2 + A_3 + A_5 + A_{41} + A_{42} + A_{43} + 2 * t_n * t * f_{r1}) * S_v \\ &= (1.2264 + 1.0688 + 10.125 + 0.2138 + 0.3164 + 0.0835 + 2 * 0.5 * 0.85 * 0.855) * 20,000 \\ &= \underline{275,212 \text{ lb}_f} \end{aligned}$$

Load for path 1-1 lesser of W or $W_{1-1} = 237,632 \text{ lb}_f$

Path 1-1 through (2) & (3) = $290,076.99 + 183,323.71 = \underline{473,400.7 \text{ lb}_f}$

Path 1-1 is stronger than W_{1-1} so it is acceptable per UG-41(b)(1).

Load for path 2-2 lesser of W or $W_{2-2} = 66,384 \text{ lb}_f$

Path 2-2 through (1), (4), (5) = $131,617.02 + 395,212.35 + 82,260.64 = \underline{609,090.02 \text{ lb}_f}$

Path 2-2 is stronger than W_{2-2} so it is acceptable per UG-41(b)(1).

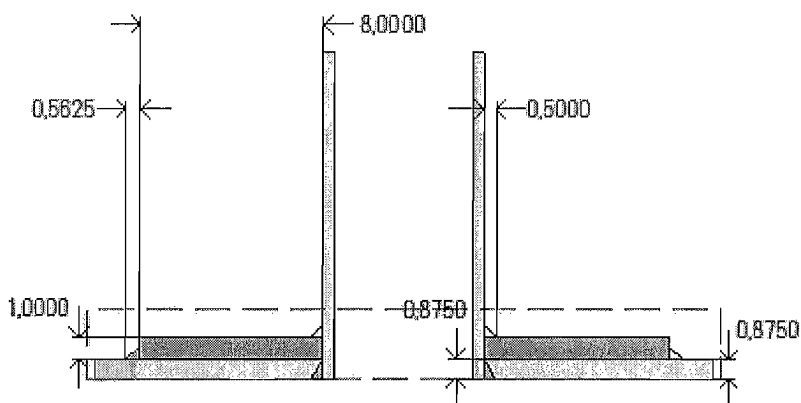
Load for path 3-3 lesser of W or $W_{3-3} = 247,995.38 \text{ lb}_f$

Path 3-3 through (2), (4), (5) = $290,076.99 + 395,212.35 + 82,260.64 = \underline{767,549.99 \text{ lb}_f}$

Path 3-3 is stronger than W so it is acceptable per UG-41(b)(2).

Nozzle M2 - 20" 150# Manway (Nozzle M3 similar) (M2)

ASME Section VIII Division 1, 2017 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Shell
Orientation	270°
Nozzle center line offset to datum line	84"
End of nozzle to shell center	75"
Offset from center, Lo	-32"
Passes through a Category A joint	No

Nozzle

Description	NPS 20 Sch 30 (XS)
Access opening	Yes
Material specification	SA-106 B Smls pipe (II-D p. 14, ln. 10)
Inside diameter, new	19"
Pipe nominal wall thickness	0.5"
Pipe minimum wall thickness ¹	0.4375"
Corrosion allowance	0"
Opening chord length	21.8695"
Projection available outside vessel, L _{pr}	7.0846"
Projection available outside vessel to flange face, L _f	12.7746"
Local vessel minimum thickness	0.875"
Liquid static head included	3.51 psi
Longitudinal joint efficiency	0.85

Reinforcing Pad

Material specification	SA-516 70 (II-D p. 18, ln. 33)
------------------------	--------------------------------

Diameter, D_p	38.9783"
Thickness, t_c	1"
Is split	No
Welds	
Inner fillet, Leg ₄₁	0.5"
Outer fillet, Leg ₄₂	0.5625"
Nozzle to vessel groove weld	0.875"
Pad groove weld	0"

¹Pipe minimum thickness = nominal thickness times pipe tolerance factor of 0.875.

ASME B16.5-2013 Flange	
Description	NPS 20 Class 150 WN A105
Bolt Material	SA-193 B7 Bolt $\leq 2 \frac{1}{2}$ (II-D p. 388, ln. 32)
Blind included	Yes
Rated MDMT	-31.1°F
Liquid static head	3.51 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Circumferential joint radiography	None UW-11(c) Type 1
Bore diameter, B (specified by purchaser)	19"
Gasket	
Description	Klingsil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -31.1°F (Coincident ratio = 0.8895) Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle	
$t_r = 253.51 \times 9.5 / (17,100 \times 0.85 - 0.6 \times 253.51) =$	0.1674"
Stress ratio = $t_r \times E^* / (t_n - c) = 0.1674 \times 0.85 / (0.4375 - 0) =$	0.3253
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

UCS-66 Material Toughness Requirements Pad	
Governing thickness, $t_g =$	0.875"
MDMT =	-20°F

Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F.

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 253.51 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
18.3238	18.7955	0.9265	1.3388	--	16	0.5302	0.1674	0.4375

UG-41 Weld Failure Path Analysis Summary (lb _f)						
All failure paths are stronger than the applicable weld loads						
Weld load W	Weld load W ₁₋₁	Path 1-1 strength	Weld load W ₂₋₂	Path 2-2 strength	Weld load W ₃₋₃	Path 3-3 strength
348,674.7	357,380	520,837.38	46,014.5	538,453.27	372,342.5	744,349.92

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to pad fillet (Leg ₄₁)	0.35	0.35	weld size is adequate
Pad to shell fillet (Leg ₄₂)	0.375	0.3938	weld size is adequate

Calculations for internal pressure 253.51 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(21.8695, 10.9348 + (0.5 - 0) + (0.875 - 0)) \\
 &= 21.8695 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(0.5 - 0) + 1) \\
 &= 2.1875 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 253.5059 \cdot 9.5 / (17,100 \cdot 1 - 0.6 \cdot 253.5059) \\
 &= 0.1421 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 253.5059 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 253.5059) \\
 &= 0.8323 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: S_n = 17,100, S_y = 20,000, S_p = 20,000 psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_y = 0.855$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_p = 0.855$$

$$f_{r3} = \text{lesser of } f_{r2} \text{ or } S_p / S_v = 0.855$$

$$f_{r4} = \text{lesser of } 1 \text{ or } S_p / S_v = 1$$

$$\begin{aligned} A &= d * t_r * F + 2 * t_n * t_r * F * (1 - f_{r1}) \\ &= 21.8695 * 0.8324 * 1 + 2 * 0.5 * 0.8324 * 1 * (1 - 0.855) \\ &= \underline{18.3238 \text{ in}^2} \end{aligned}$$

Area available from FIG. UG-37.1

$$A_1 = \text{larger of the following} = \underline{0.9265 \text{ in}^2}$$

$$\begin{aligned} &= d * (E_1 * t - F * t_r) - 2 * t_n * (E_1 * t - F * t_r) * (1 - f_{r1}) \\ &= 21.8695 * (1 * 0.875 - 1 * 0.8324) - 2 * 0.5 * (1 * 0.875 - 1 * 0.8324) * (1 - 0.855) \\ &= 0.9265 \text{ in}^2 \\ &= 2 * (t + t_n) * (E_1 * t - F * t_r) - 2 * t_n * (E_1 * t - F * t_r) * (1 - f_{r1}) \\ &= 2 * (0.875 + 0.5) * (1 * 0.875 - 1 * 0.8324) - 2 * 0.5 * (1 * 0.875 - 1 * 0.8324) * (1 - 0.855) \\ &= 0.1111 \text{ in}^2 \end{aligned}$$

$$A_2 = \text{smaller of the following} = \underline{1.3388 \text{ in}^2}$$

$$\begin{aligned} &= 5 * (t_n - t_{rn}) * f_{r2} * t \\ &= 5 * (0.5 - 0.1421) * 0.855 * 0.875 \\ &= 1.3388 \text{ in}^2 \\ &= 2 * (t_n - t_{rn}) * (2.5 * t_n + t_e) * f_{r2} \\ &= 2 * (0.5 - 0.1421) * (2.5 * 0.5 + 1) * 0.855 \\ &= 1.377 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} A_{41} &= \text{Leg}^2 * f_{r3} \\ &= 0.52^2 * 0.855 \\ &= \underline{0.2138 \text{ in}^2} \end{aligned}$$

$$\begin{aligned} A_{42} &= \text{Leg}^2 * f_{r4} \\ &= 0.5625^2 * 1 \\ &= \underline{0.3164 \text{ in}^2} \end{aligned}$$

$$\begin{aligned} A_5 &= (D_p - d - 2 * t_n) * t_e * f_{r4} \\ &= (38.9783 - 22.9783) * 1 * 1 \\ &= \underline{16 \text{ in}^2} \end{aligned}$$

$$\begin{aligned} \text{Area} &= A_1 + A_2 + A_{41} + A_{42} + A_5 \\ &= 0.9265 + 1.3388 + 0.2138 + 0.3164 + 16 \\ &= \underline{18.7955 \text{ in}^2} \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c)(2) Weld Check

$$\begin{aligned} \text{Inner fillet: } t_{\min} &= \text{lesser of } 0.75 \text{ or } t_n \text{ or } t_e = 0.5 \text{ in} \\ t_{w(\min)} &= 0.7 * t_{\min} = \underline{0.35 \text{ in}} \\ t_{w(\text{actual})} &= 0.7 * \text{Leg} = 0.7 * 0.5 = 0.35 \text{ in} \end{aligned}$$

$$\begin{aligned} \text{Outer fillet: } t_{\min} &= \text{lesser of } 0.75 \text{ or } t_e \text{ or } t = 0.75 \text{ in} \\ t_{w(\min)} &= 0.5 * t_{\min} = \underline{0.375 \text{ in}} \\ t_{w(\text{actual})} &= 0.7 * \text{Leg} = 0.7 * 0.5625 = 0.3938 \text{ in} \end{aligned}$$

UG-45 Nozzle Neck Thickness Check (Access Opening)

$$\begin{aligned}
 t_a \text{ UG-27} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 253.5059 \cdot 9.5 / (17,100 \cdot 0.85 - 0.6 \cdot 253.5059) + 0 \\
 &= 0.1674 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \max[t_a \text{ UG-27}, t_a \text{ UG-22}] \\
 &= \max[0.1674, 0] \\
 &= 0.1674 \text{ in}
 \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.875 \cdot 0.5 = 0.4375 \text{ in}$

The nozzle neck thickness is adequate.

Allowable stresses in joints UG-45 and UW-15(c)

Groove weld in tension: $0.74 \cdot 20,000 = 14,800 \text{ psi}$

Nozzle wall in shear: $0.7 \cdot 17,100 = 11,970 \text{ psi}$

Inner fillet weld in shear: $0.49 \cdot 17,100 = 8,379 \text{ psi}$

Outer fillet weld in shear: $0.49 \cdot 20,000 = 9,800 \text{ psi}$

Strength of welded joints:

(1) Inner fillet weld in shear

$$(\pi / 2) \cdot \text{Nozzle OD} \cdot \text{Leg} \cdot S_i = (\pi / 2) \cdot 20 \cdot 0.5 \cdot 8,379 = 131,617.02 \text{ lbf}$$

(2) Outer fillet weld in shear

$$(\pi / 2) \cdot \text{Pad OD} \cdot \text{Leg} \cdot S_o = (\pi / 2) \cdot 38.9783 \cdot 0.5625 \cdot 9,800 = 337,513.67 \text{ lbf}$$

(3) Nozzle wall in shear

$$(\pi / 2) \cdot \text{Mean nozzle dia} \cdot t_n \cdot S_n = (\pi / 2) \cdot 19.5 \cdot 0.5 \cdot 11,970 = 183,323.71 \text{ lbf}$$

(4) Groove weld in tension

$$(\pi / 2) \cdot \text{Nozzle OD} \cdot t_w \cdot S_g = (\pi / 2) \cdot 20 \cdot 0.875 \cdot 14,800 = 406,836.25 \text{ lbf}$$

Loading on welds per UG-41(b)(1)

$$\begin{aligned}
 W &= (A - A_1 + 2 \cdot t_n \cdot f_{r1} \cdot (E_1 \cdot t - F \cdot t_r)) \cdot S_v \\
 &= (18.3238 - 0.9265 + 2 \cdot 0.5 \cdot 0.855 \cdot (1 \cdot 0.875 - 1 \cdot 0.8324)) \cdot 20,000 \\
 &= \underline{348,674.7 \text{ lbf}}
 \end{aligned}$$

$$\begin{aligned}
 W_{1-1} &= (A_2 + A_5 + A_{41} + A_{42}) \cdot S_v \\
 &= (1.3388 + 16 + 0.2138 + 0.3164) \cdot 20,000 \\
 &= \underline{357,380 \text{ lbf}}
 \end{aligned}$$

$$\begin{aligned}
 W_{2-2} &= (A_2 + A_3 + A_{41} + A_{43} + 2 \cdot t_n \cdot t \cdot f_{r1}) \cdot S_v \\
 &= (1.3388 + 0 + 0.2138 + 0 + 2 \cdot 0.5 \cdot 0.875 \cdot 0.855) \cdot 20,000 \\
 &= \underline{46,014.5 \text{ lbf}}
 \end{aligned}$$

$$\begin{aligned}
 W_{3-3} &= (A_2 + A_3 + A_5 + A_{41} + A_{42} + A_{43} + 2 \cdot t_n \cdot t \cdot f_{r1}) \cdot S_v \\
 &= (1.3388 + 0 + 16 + 0.2138 + 0.3164 + 0 + 2 \cdot 0.5 \cdot 0.875 \cdot 0.855) \cdot 20,000 \\
 &= \underline{372,342.5 \text{ lbf}}
 \end{aligned}$$

Load for path 1-1 lesser of W or $W_{1-1} = 348,674.7 \text{ lbf}$

Path 1-1 through (2) & (3) = $337,513.67 + 183,323.71 = \underline{520,837.38 \text{ lbf}}$

Path 1-1 is stronger than W so it is acceptable per UG-41(b)(2).

Load for path 2-2 lesser of W or $W_{2-2} = 46,014.5 \text{ lbf}$

Path 2-2 through (1), (4) = $131,617.02 + 406,836.25 = \underline{538,453.27}$ lb_f

Path 2-2 is stronger than W_{2-2} so it is acceptable per UG-41(b)(1).

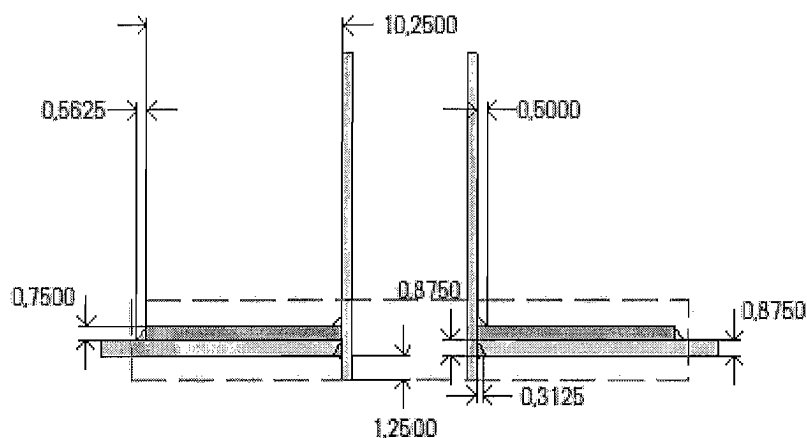
Load for path 3-3 lesser of W or $W_{3-3} = 348,674.7$ lb_f

Path 3-3 through (2), (4) = $337,513.67 + 406,836.25 = \underline{744,349.92}$ lb_f

Path 3-3 is stronger than W so it is acceptable per UG-41(b)(2).

Nozzle N1 - 24" 150# Inlet (Nozzle N2 similar) (N1)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Shell
Orientation	0°
Nozzle center line offset to datum line	148"
End of nozzle to shell center	78"
Passes through a Category A joint	No

Nozzle

Description	NPS 24 XS
Access opening	No
Material specification	SA-106 B Smls pipe (II-D p. 14, ln. 10)
Inside diameter, new	23"
Pipe nominal wall thickness	0.5"
Pipe minimum wall thickness ¹	0.4375"
Corrosion allowance	0"
Projection available outside vessel, L _{pr}	6"
Internal projection, h _{new}	1.25"
Projection available outside vessel to flange face, L _f	12"
Local vessel minimum thickness	0.875"
Liquid static head included	0 psi
Longitudinal joint efficiency	0.85

Reinforcing Pad

Material specification	SA-516 70 (II-D p. 18, ln. 33)
Diameter, D _p	44.5"

Thickness, t_c	0.75"
Is split	No
Welds	
Inner fillet, Leg ₄₁	0.5"
Outer fillet, Leg ₄₂	0.5625"
Lower fillet, Leg ₄₃	0.3125"
Nozzle to vessel groove weld	0.875"
Pad groove weld	0"

¹Pipe minimum thickness = nominal thickness times pipe tolerance factor of 0.875.

ASME B16.5-2013 Flange	
Description	NPS 24 Class 150 WN A105
Bolt Material	SA-193 B7 Bolt $\leq 2 \frac{1}{2}$ (II-D p. 388, ln. 32)
Blind included	No
Rated MDMT	-32.3°F
Liquid static head	0 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Circumferential joint radiography	None UW-11(c) Type 1
Bore diameter, B (specified by purchaser)	23"
Gasket	
Description	Klingersil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -32.3°F (Coincident ratio = 0.8772) Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle	
Governing thickness, t_g =	0.4375"
Exemption temperature from Fig UCS-66 Curve B =	-13°F
$t_r = 250 * 11.5 / (17,100 * 0.85 - 0.6 * 250) =$	0.1999"
Stress ratio = $t_r * E^* / (t_n - c) = 0.1999 * 0.85 / (0.4375 - 0) =$	0.3883
Reduction in MDMT, T_R from Fig UCS-66.1 =	101.6°F
MDMT = $\max[\text{MDMT} - T_R, -55] = \max[-13 - 101.6, -55] =$	-55°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

UCS-66 Material Toughness Requirements Pad

Governing thickness, t_g =	0.75"
MDMT =	-20°F
Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 250 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
18.9997	19.424	1.2365	1.13	1.0688	15.375	0.6137	0.3281	0.4375

UG-41 Weld Failure Path Analysis Summary (lb _f)						
All failure paths are stronger than the applicable weld loads						
Weld load W	Weld load W ₁₋₁	Path 1-1 strength	Weld load W ₂₋₂	Path 2-2 strength	Weld load W ₃₋₃	Path 3-3 strength
356,189.72	340,704	606,254.73	64,883.5	744,856.69	378,711.5	972,242.42

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to pad fillet (Leg ₄₁)	0.35	0.35	weld size is adequate
Pad to shell fillet (Leg ₄₂)	0.375	0.3938	weld size is adequate

Calculations for internal pressure 250 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(23, 11.5 + (0.5 - 0) + (0.875 - 0)) \\
 &= 23 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(0.5 - 0) + 0.75) \\
 &= 2 \text{ in}
 \end{aligned}$$

Inner Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_I &= \text{MIN}(h, 2.5*(t - C), 2.5*(t_i - C_n - C)) \\
 &= \text{MIN}(1.25, 2.5*(0.875 - 0), 2.5*(0.5 - 0 - 0)) \\
 &= 1.25 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_n &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 250 \cdot 11.5 / (17,100 \cdot 1 - 0.6 \cdot 250) \\
 &= 0.1696 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 250 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 250) \\
 &= 0.8209 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: $S_n = 17,100$, $S_v = 20,000$, $S_p = 20,000$ psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 0.855$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 0.855$$

$$f_{r3} = \text{lesser of } f_{r2} \text{ or } S_p / S_v = 0.855$$

$$f_{r4} = \text{lesser of } 1 \text{ or } S_p / S_v = 1$$

$$\begin{aligned} A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\ &= 23 \cdot 0.8209 \cdot 1 + 2 \cdot 0.5 \cdot 0.8209 \cdot 1 \cdot (1 - 0.855) \\ &= \underline{18.9997 \text{ in}^2} \end{aligned}$$

Area available from FIG. UG-37.1

$$A_1 = \text{larger of the following} = \underline{1.2365 \text{ in}^2}$$

$$\begin{aligned} &= d \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\ &= 23 \cdot (1 \cdot 0.875 - 1 \cdot 0.8209) - 2 \cdot 0.5 \cdot (1 \cdot 0.875 - 1 \cdot 0.8209) \cdot (1 - 0.855) \\ &= \underline{1.2365 \text{ in}^2} \\ &= 2 \cdot (t + t_n) \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\ &= 2 \cdot (0.875 + 0.5) \cdot (1 \cdot 0.875 - 1 \cdot 0.8209) - 2 \cdot 0.5 \cdot (1 \cdot 0.875 - 1 \cdot 0.8209) \cdot (1 - 0.855) \\ &= \underline{0.1409 \text{ in}^2} \end{aligned}$$

$$A_2 = \text{smaller of the following} = \underline{1.13 \text{ in}^2}$$

$$\begin{aligned} &= 5 \cdot (t_n - t_{rn}) \cdot f_{r2} \cdot t \\ &= 5 \cdot (0.5 - 0.1696) \cdot 0.855 \cdot 0.875 \\ &= \underline{1.2359 \text{ in}^2} \\ &= 2 \cdot (t_n - t_{rn}) \cdot (2.5 \cdot t_n + t_e) \cdot f_{r2} \\ &= 2 \cdot (0.5 - 0.1696) \cdot (2.5 \cdot 0.5 + 0.75) \cdot 0.855 \\ &= \underline{1.13 \text{ in}^2} \end{aligned}$$

$$A_3 = \text{smaller of the following} = \underline{1.0688 \text{ in}^2}$$

$$\begin{aligned} &= 5 \cdot t \cdot t_i \cdot f_{r2} \\ &= 5 \cdot 0.875 \cdot 0.5 \cdot 0.855 \\ &= \underline{1.8703 \text{ in}^2} \\ &= 5 \cdot t_i \cdot t_i \cdot f_{r2} \\ &= 5 \cdot 0.5 \cdot 0.5 \cdot 0.855 \\ &= \underline{1.0688 \text{ in}^2} \\ &= 2 \cdot h \cdot t_i \cdot f_{r2} \\ &= 2 \cdot 1.25 \cdot 0.5 \cdot 0.855 \\ &= \underline{1.0688 \text{ in}^2} \end{aligned}$$

$$\begin{aligned} A_{41} &= \text{Leg}^2 \cdot f_{r3} \\ &= 0.5^2 \cdot 0.855 \\ &= \underline{0.2138 \text{ in}^2} \end{aligned}$$

$$\begin{aligned} A_{42} &= \text{Leg}^2 \cdot f_{r4} \\ &= 0.5625^2 \cdot 1 \\ &= \underline{0.3164 \text{ in}^2} \end{aligned}$$

$$\begin{aligned} A_{43} &= \text{Leg}^2 \cdot f_{r2} \\ &= 0.3125^2 \cdot 0.855 \end{aligned}$$

$$= 0.0835 \text{ in}^2$$

$$\begin{aligned} A_5 &= (D_p - d - 2*t_n)*t_e*f_{r4} \\ &= (44.5 - 23 - 2*0.5)*0.75*1 \\ &= 15.375 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} \text{Area} &= A_1 + A_2 + A_3 + A_{41} + A_{42} + A_{43} + A_5 \\ &= 1.2365 + 1.13 + 1.0688 + 0.2138 + 0.3164 + 0.0835 + 15.375 \\ &= 19.424 \text{ in}^2 \end{aligned}$$

As Area >= A the reinforcement is adequate.

UW-16(c)(2) Weld Check

Inner fillet: $t_{\min}$ = lesser of 0.75 or t_n or $t_e = 0.5$ in

$$t_{w(\min)} = 0.7*t_{\min} = 0.35 \text{ in}$$

$$t_{w(\text{actual})} = 0.7*\text{Leg} = 0.7*0.5 = 0.35 \text{ in}$$

Outer fillet: $t_{\min}$ = lesser of 0.75 or t_e or $t = 0.75$ in

$$t_{w(\min)} = 0.5*t_{\min} = 0.375 \text{ in}$$

$$t_{w(\text{actual})} = 0.7*\text{Leg} = 0.7*0.5625 = 0.3938 \text{ in}$$

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned} t_{a \text{ UG-27}} &= P*R_n / (S_n*E - 0.6*P) + \text{Corrosion} \\ &= 250*11.5 / (17,100*0.85 - 0.6*250) + 0 \\ &= 0.1999 \text{ in} \end{aligned}$$

$$\begin{aligned} t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\ &= \max[0.1999, 0] \\ &= 0.1999 \text{ in} \end{aligned}$$

$$\begin{aligned} t_{b1} &= P*R_o / (S*E + 0.4*P) + \text{Corrosion} \\ &= 250*66 / (20,000*1 + 0.4*250) + 0 \\ &= 0.8209 \text{ in} \end{aligned}$$

$$\begin{aligned} t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\ &= \max[0.8209, 0.0625] \\ &= 0.8209 \text{ in} \end{aligned}$$

$$\begin{aligned} t_b &= \min[t_{b3}, t_{b1}] \\ &= \min[0.3281, 0.8209] \\ &= 0.3281 \text{ in} \end{aligned}$$

$$\begin{aligned} t_{\text{UG-45}} &= \max[t_a, t_b] \\ &= \max[0.1999, 0.3281] \\ &= 0.3281 \text{ in} \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.875*0.5 = 0.4375$ in

The nozzle neck thickness is adequate.

Allowable stresses in joints UG-45 and UW-15(c)

Groove weld in tension: $0.74*20,000 = 14,800$ psi

Nozzle wall in shear: $0.7*17,100 = 11,970$ psi

Inner fillet weld in shear: $0.49*17,100 = 8,379$ psi

Outer fillet weld in shear: $0.49*20,000 = 9,800$ psi

Lower fillet weld in shear: $0.49 \times 17,100 = 8,379$ psi

Strength of welded joints:

(1) Inner fillet weld in shear

$$(\pi / 2) * \text{Nozzle OD} * \text{Leg} * S_i = (\pi / 2) * 24 * 0.5 * 8,379 = 157,940.43 \text{ lb}_f$$

(2) Outer fillet weld in shear

$$(\pi / 2) * \text{Pad OD} * \text{Leg} * S_o = (\pi / 2) * 44.5 * 0.5625 * 9,800 = 385,326.15 \text{ lb}_f$$

(3) Nozzle wall in shear

$$(\pi / 2) * \text{Mean nozzle dia} * t_n * S_n = (\pi / 2) * 23.5 * 0.5 * 11,970 = 220,928.58 \text{ lb}_f$$

(4) Groove weld in tension

$$(\pi / 2) * \text{Nozzle OD} * t_w * S_g = (\pi / 2) * 24 * 0.875 * 14,800 = 488,203.5 \text{ lb}_f$$

(5) Lower fillet weld in shear

$$(\pi / 2) * \text{Nozzle OD} * \text{Leg} * S_l = (\pi / 2) * 24 * 0.3125 * 8,379 = 98,712.77 \text{ lb}_f$$

Loading on welds per UG-41(b)(1)

$$\begin{aligned} W &= (A - A_1 + 2 * t_n * f_{r1} * (E_1 * t - F * t_r)) * S_v \\ &= (18.9997 - 1.2365 + 2 * 0.5 * 0.855 * (1 * 0.875 - 1 * 0.8209)) * 20,000 \\ &= \underline{356,189.72} \text{ lb}_f \end{aligned}$$

$$\begin{aligned} W_{1-1} &= (A_2 + A_5 + A_{41} + A_{42}) * S_v \\ &= (1.13 + 15.375 + 0.2138 + 0.3164) * 20,000 \\ &= \underline{340,704} \text{ lb}_f \end{aligned}$$

$$\begin{aligned} W_{2-2} &= (A_2 + A_3 + A_{41} + A_{43} + 2 * t_n * t * f_{r1}) * S_v \\ &= (1.13 + 1.0688 + 0.2138 + 0.0835 + 2 * 0.5 * 0.875 * 0.855) * 20,000 \\ &= \underline{64,883.5} \text{ lb}_f \end{aligned}$$

$$\begin{aligned} W_{3-3} &= (A_2 + A_3 + A_5 + A_{41} + A_{42} + A_{43} + 2 * t_n * t * f_{r1}) * S_v \\ &= (1.13 + 1.0688 + 15.375 + 0.2138 + 0.3164 + 0.0835 + 2 * 0.5 * 0.875 * 0.855) * 20,000 \\ &= \underline{378,711.5} \text{ lb}_f \end{aligned}$$

Load for path 1-1 lesser of W or $W_{1-1} = 340,704 \text{ lb}_f$

Path 1-1 through (2) & (3) = $385,326.15 + 220,928.58 = \underline{606,254.73} \text{ lb}_f$

Path 1-1 is stronger than W_{1-1} so it is acceptable per UG-41(b)(1).

Load for path 2-2 lesser of W or $W_{2-2} = 64,883.5 \text{ lb}_f$

Path 2-2 through (1), (4), (5) = $157,940.43 + 488,203.5 + 98,712.77 = \underline{744,856.69} \text{ lb}_f$

Path 2-2 is stronger than W_{2-2} so it is acceptable per UG-41(b)(1).

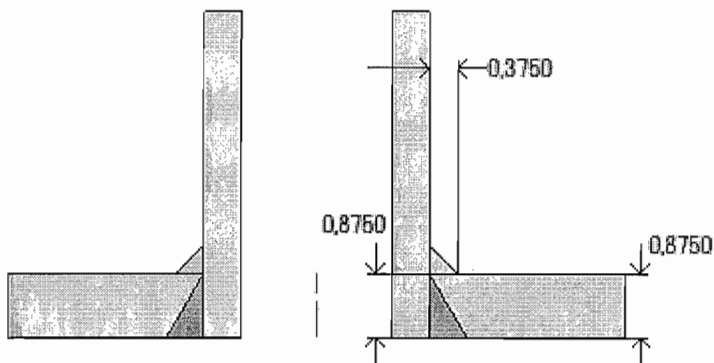
Load for path 3-3 lesser of W or $W_{3-3} = 356,189.72 \text{ lb}_f$

Path 3-3 through (2), (4), (5) = $385,326.15 + 488,203.5 + 98,712.77 = \underline{972,242.42} \text{ lb}_f$

Path 3-3 is stronger than W so it is acceptable per UG-41(b)(2).

Nozzle N3 - 2" 150# LP Drain Inlet (Nozzle N4 similar) (N3)

ASME Section VIII Division 1, 2017 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Shell
Orientation	0°
Nozzle center line offset to datum line	24"
End of nozzle to shell center	74"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	2"
Nominal wall thickness	0.53"
Corrosion allowance	0"
Projection available outside vessel, L _{pr}	7.25"
Projection available outside vessel to flange face, L _f	8"
Local vessel minimum thickness	0.875"
Liquid static head included	0 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg ₄₁	0.375"
Nozzle to vessel groove weld	0.875"

ASME B16.5-2013 Flange

Description	NPS 2 Class 150 LWN A105
Bolt Material	SA-193 B7 Bolt ≤ 2 1/2 (II-D p. 388, ln. 32)

Blind included	No
Rated MDMT	-32.3°F
Liquid static head	0 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Gasket	
Description	Klingsil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -32.3°F (Coincident ratio = 0.8772)	
Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements	
LWN rated MDMT per UCS-66(c)(4) =	-32.3°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 250 psi @ 125 °F							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.189	0.53

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 250 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(2, 1 + (0.53 - 0) + (0.875 - 0)) \\
 &= 2.405 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(0.53 - 0) + 0) \\
 &= 1.325 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_m &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 250 \cdot 1 / (20,000 \cdot 1 - 0.6 \cdot 250) \\
 &= 0.0126 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 250 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 250) \\
 &= 0.8209 \text{ in}
 \end{aligned}$$

This opening does not require reinforcement per UG-36(c)(3)(a)

UW-16(c) Weld Check

$$\begin{aligned}
 \text{Fillet weld: } t_{\min} &= \text{lesser of } 0.75 \text{ or } t_n \text{ or } t = 0.53 \text{ in} \\
 t_{c(\min)} &= \text{lesser of } 0.25 \text{ or } 0.7 \cdot t_{\min} = 0.25 \text{ in} \\
 t_{c(\text{actual})} &= 0.7 \cdot \text{Leg} = 0.7 \cdot 0.375 = 0.2625 \text{ in}
 \end{aligned}$$

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 250 \cdot 1 / (20,000 \cdot 1 - 0.6 \cdot 250) + 0 \\
 &= 0.0126 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.0126, 0] \\
 &= 0.0126 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) + \text{Corrosion} \\
 &= 250 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 250) + 0 \\
 &= 0.8209 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\
 &= \max[0.8209, 0.0625] \\
 &= 0.8209 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_b &= \min[t_{b3}, t_{b1}] \\
 &= \min[0.189, 0.8209] \\
 &= 0.189 \text{ in}
 \end{aligned}$$

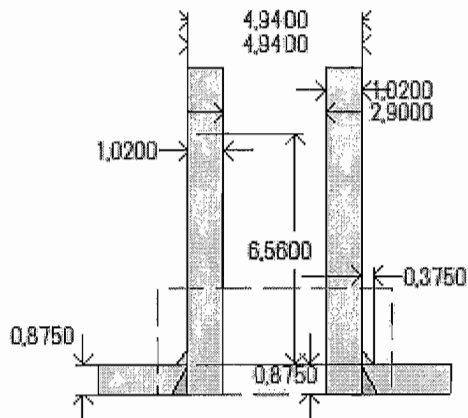
$$\begin{aligned}
 t_{\text{UG-45}} &= \max[t_a, t_b] \\
 &= \max[0.0126, 0.189] \\
 &= \underline{0.189} \text{ in}
 \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.53$ in

The nozzle neck thickness is adequate.

Nozzle N6 - 3" 150# Drain (Nozzles N9A & N9B similar) (N6)

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Note: Per UW-16(b) minimum inside corner radius $r_1 = \min [1 / 4 * t, 0.125 \text{ in}] = 0.125 \text{ in}$

Location and Orientation

Located on	Shell
Orientation	180°
Nozzle center line offset to datum line	24"
End of nozzle to shell center	74"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	2.9"
Wall thickness, t_n	1.02"
Minimum wall thickness	0.8325"
Corrosion allowance	0"
Projection available outside vessel, L_{pr}	7.06"
Heavy barrel length, L_{hb}	6.56"
Projection available outside vessel to flange face, L_f	8"
Local vessel minimum thickness	0.875"
Liquid static head included	4.73 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg_{41}	0.375"
Nozzle to vessel groove weld	0.875"

ASME B16.5-2013 Flange

Description	NPS 3 Class 150 FVC HB A105 (Nut Stop)
Bolt Material	SA-193 B7 Bolt $\leq 2 \frac{1}{2}$ (II-D p. 388, ln. 32)
Blind included	No
Rated MDMT	-30.5°F
Liquid static head	5.02 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Gasket	
Description	Klingsil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -30.5°F (Coincident ratio = 0.8948) Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle At Intersection

$t_r = 254.73 * 1.45 / (20,000 * 1 - 0.6 * 254.73) =$	0.0186"
Stress ratio = $t_r * E^* / (t_n - c) = 0.0186 * 1 / (1.02 - 0) =$	0.0183
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

UCS-66 Material Toughness Requirements Nozzle

$t_r = 254.73 * 1.45 / (20,000 * 1 - 0.6 * 254.73) =$	0.0186"
Stress ratio = $t_r * E^* / (t_n - c) = 0.0186 * 1 / (0.8325 - 0) =$	0.0224
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 254.73 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
<u>2.4254</u>	<u>4.6681</u>	<u>0.1464</u>	<u>4.3811</u>	--	--	<u>0.1406</u>	<u>0.2258</u>	0.8325

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	<u>0.25</u>	0.2625	weld size is adequate

Calculations for internal pressure 254.73 psi @ 125 °F

Parallel Limit of reinforcement per UG-40 and Fig. UG-40 sketch (e-2)

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(2.9, 1.45 + (1.02 - 0) + (0.875 - 0)) \\
 &= 3.345 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40 and Fig. UG-40 sketch (e-2)

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(1.02 - 0) + 0) \\
 &= 2.1875 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 254.7332 \cdot 1.45 / (20,000 \cdot 1 - 0.6 \cdot 254.7332) \\
 &= 0.0186 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 254.7332 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 254.7332) \\
 &= 0.8364 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: $S_n = 20,000$, $S_v = 20,000$ psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$\begin{aligned}
 A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\
 &= 2.9 \cdot 0.8364 \cdot 1 + 2 \cdot 1.02 \cdot 0.8364 \cdot 1 \cdot (1 - 1) \\
 &= \underline{2.4254} \text{ in}^2
 \end{aligned}$$

Area available from FIG. UG-37.1

$A_1 = \text{larger of the following} = 0.1464 \text{ in}^2$

$$\begin{aligned}
 &= d(E_1 t - F t_r) - 2 t_n (E_1 t - F t_r) (1 - f_{r1}) \\
 &= 2.9(1*0.875 - 1*0.8364) - 2*1.02(1*0.875 - 1*0.8364)(1 - 1) \\
 &= 0.1121 \text{ in}^2 \\
 &= 2(t + t_n)(E_1 t - F t_r) - 2 t_n (E_1 t - F t_r) (1 - f_{r1}) \\
 &= 2(0.875 + 1.02)(1*0.875 - 1*0.8364) - 2*1.02(1*0.875 - 1*0.8364)(1 - 1) \\
 &= 0.1464 \text{ in}^2
 \end{aligned}$$

$A_2 = \text{smaller of the following} = 4.3811 \text{ in}^2$

$$\begin{aligned}
 &= 5(t_n - t_{rn}) f_{r2} t \\
 &= 5(1.02 - 0.0186) * 1 * 0.875 \\
 &= 4.3811 \text{ in}^2 \\
 &= 5(t_n - t_{rn}) f_{r2} t_n \\
 &= 5(1.02 - 0.0186) * 1 * 1.02 \\
 &= 5.1071 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 A_{41} &= \text{Leg}^2 f_{r2} \\
 &= 0.375^2 * 1 \\
 &= 0.1406 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 \text{Area} &= A_1 + A_2 + A_{41} \\
 &= 0.1464 + 4.3811 + 0.1406 \\
 &= 4.6681 \text{ in}^2
 \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c) Weld Check

Fillet weld: $t_{\min} = \text{lesser of } 0.75 \text{ or } t_n \text{ or } t = 0.75 \text{ in}$

$t_{c(\min)} = \text{lesser of } 0.25 \text{ or } 0.7 * t_{\min} = 0.25 \text{ in}$

$t_{c(\text{actual})} = 0.7 * \text{Leg} = 0.7 * 0.375 = 0.2625 \text{ in}$

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P R_n / (S_n E - 0.6 P) + \text{Corrosion} \\
 &= 255.022 * 1.45 / (20,000 * 1 - 0.6 * 255.022) + 0 \\
 &= 0.0186 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.0186, 0] \\
 &= 0.0186 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= P R_o / (S E + 0.4 P) + \text{Corrosion} \\
 &= 254.7332 * 66 / (20,000 * 1 + 0.4 * 254.7332) + 0 \\
 &= 0.8364 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\
 &= \max[0.8364, 0.0625] \\
 &= 0.8364 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_b &= \min[t_{b3}, t_{b1}] \\
 &= \min[0.2258, 0.8364] \\
 &= 0.2258 \text{ in}
 \end{aligned}$$

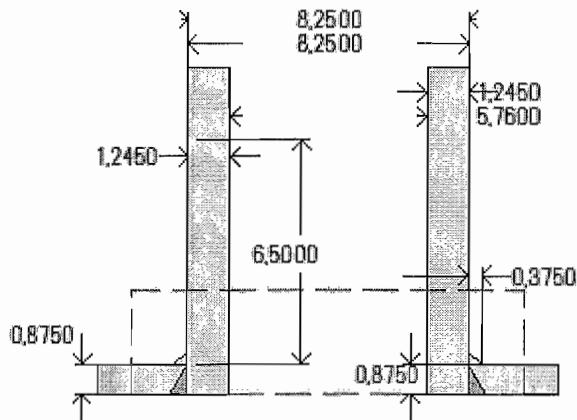
$$\begin{aligned}t_{UG-45} &= \max[t_a, t_b] \\&= \max[0.0186, 0.2258] \\&= \underline{0.2258} \text{ in}\end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.8325$ in

The nozzle neck thickness is adequate.

Nozzle N7 - 6" 150# Drain (Nozzles N8 & N10 similar) (N7)

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Note: Per UW-16(b) minimum inside corner radius $r_1 = \min [1 / 4 * t, 0.125 \text{ in}] = 0.125 \text{ in}$

Location and Orientation

Located on	Shell
Orientation	180°
Nozzle center line offset to datum line	72"
End of nozzle to shell center	74"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	5.76"
Wall thickness, t_n	1.245"
Minimum wall thickness	1.0575"
Corrosion allowance	0"
Projection available outside vessel, L_{pr}	7"
Heavy barrel length, L_{hb}	6.5"
Projection available outside vessel to flange face, L_f	8"
Local vessel minimum thickness	0.875"
Liquid static head included	4.73 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg_{41}	0.375"
Nozzle to vessel groove weld	0.875"

ASME B16.5-2013 Flange

Description	NPS 6 Class 150 FVC HB A105 (Nut Stop)
Bolt Material	SA-193 B7 Bolt $\leq 2 \frac{1}{2}$ (II-D p. 388, ln. 32)
Blind included	No
Rated MDMT	-30.5°F
Liquid static head	5.02 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Gasket	
Description	Klingsil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -30.5°F (Coincident ratio = 0.8948) Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle At Intersection

$t_r = 254.73 * 2.88 / (20,000 * 1 - 0.6 * 254.73) =$	0.037"
Stress ratio = $t_r * E^* / (t_n - c) = 0.037 * 1 / (1.245 - 0) =$	0.0297
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

UCS-66 Material Toughness Requirements Nozzle

$t_r = 254.73 * 2.88 / (20,000 * 1 - 0.6 * 254.73) =$	0.037"
Stress ratio = $t_r * E^* / (t_n - c) = 0.037 * 1 / (1.0575 - 0) =$	0.035
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 254.73 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
4.8174	5.6482	0.2226	5.285	--	--	0.1406	0.2818	1.0575

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 254.73 psi @ 125 °F

Parallel Limit of reinforcement per UG-40 and Fig. UG-40 sketch (c-2)

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(5.76, 2.88 + (1.245 - 0) + (0.875 - 0)) \\
 &= 5.76 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40 and Fig. UG-40 sketch (c-2)

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(1.245 - 0) + 0) \\
 &= 2.1875 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 254.7332 \cdot 2.88 / (20,000 \cdot 1 - 0.6 \cdot 254.7332) \\
 &= 0.037 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 254.7332 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 254.7332) \\
 &= 0.8364 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: $S_n = 20,000$, $S_v = 20,000$ psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$\begin{aligned}
 A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\
 &= 5.76 \cdot 0.8364 \cdot 1 + 2 \cdot 1.245 \cdot 0.8364 \cdot 1 \cdot (1 - 1) \\
 &= 4.8174 \text{ in}^2
 \end{aligned}$$

Area available from FIG. UG-37.1

$A_1 = \text{larger of the following} = 0.2226 \text{ in}^2$

$$\begin{aligned}
 &= d(E_1 * t - F * t_r) - 2 * t_n * (E_1 * t - F * t_r) * (1 - f_{r1}) \\
 &= 5.76 * (1 * 0.875 - 1 * 0.8364) - 2 * 1.245 * (1 * 0.875 - 1 * 0.8364) * (1 - 1) \\
 &= 0.2226 \text{ in}^2 \\
 &= 2 * (t + t_n) * (E_1 * t - F * t_r) - 2 * t_n * (E_1 * t - F * t_r) * (1 - f_{r1}) \\
 &= 2 * (0.875 + 1.245) * (1 * 0.875 - 1 * 0.8364) - 2 * 1.245 * (1 * 0.875 - 1 * 0.8364) * (1 - 1) \\
 &= 0.1638 \text{ in}^2
 \end{aligned}$$

$A_2 = \text{smaller of the following} = 5.285 \text{ in}^2$

$$\begin{aligned}
 &= 5 * (t_n - t_{rn}) * f_{r2} * t \\
 &= 5 * (1.245 - 0.037) * 1 * 0.875 \\
 &= 5.285 \text{ in}^2 \\
 &= 5 * (t_n - t_{rn}) * f_{r2} * t_n \\
 &= 5 * (1.245 - 0.037) * 1 * 1.245 \\
 &= 7.5198 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 A_{41} &= \text{Leg}^2 * f_{r2} \\
 &= 0.375^2 * 1 \\
 &= 0.1406 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 \text{Area} &= A_1 + A_2 + A_{41} \\
 &= 0.2226 + 5.285 + 0.1406 \\
 &= 5.6482 \text{ in}^2
 \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c) Weld Check

Fillet weld: $t_{\min} = \text{lesser of } 0.75 \text{ or } t_n \text{ or } t = 0.75 \text{ in}$

$t_{c(\min)} = \text{lesser of } 0.25 \text{ or } 0.7 * t_{\min} = 0.25 \text{ in}$

$t_{c(\text{actual})} = 0.7 * \text{Leg} = 0.7 * 0.375 = 0.2625 \text{ in}$

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P * R_n / (S_n * E - 0.6 * P) + \text{Corrosion} \\
 &= 255.022 * 2.88 / (20,000 * 1 - 0.6 * 255.022) + 0 \\
 &= 0.037 \text{ in} \\
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.037, 0] \\
 &= 0.037 \text{ in} \\
 t_{b1} &= P * R_o / (S * E + 0.4 * P) + \text{Corrosion} \\
 &= 254.7332 * 66 / (20,000 * 1 + 0.4 * 254.7332) + 0 \\
 &= 0.8364 \text{ in} \\
 t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\
 &= \max[0.8364, 0.0625] \\
 &= 0.8364 \text{ in} \\
 t_b &= \min[t_{b3}, t_{b1}] \\
 &= \min[0.2818, 0.8364] \\
 &= 0.2818 \text{ in}
 \end{aligned}$$

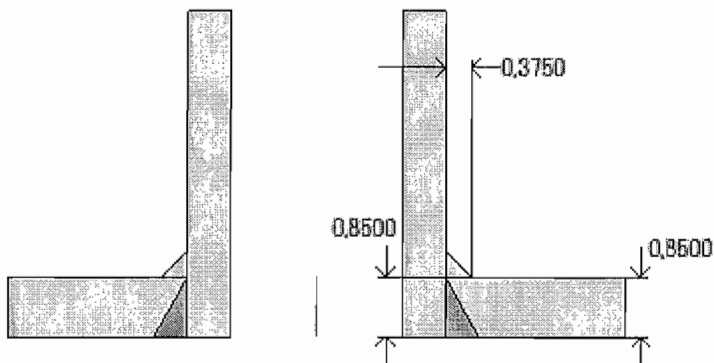
$$\begin{aligned}t_{UG-45} &= \max[t_a, t_b] \\&= \max[0.037, 0.2818] \\&= \underline{0.2818} \text{ in}\end{aligned}$$

Available nozzle wall thickness new, $t_n = 1.0575$ in

The nozzle neck thickness is adequate.

Nozzle N11 - 2" 6000# Head End Level Gauge (N11)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Left Head
Orientation	0°
End of nozzle to datum line	1,020.0374"
Calculated as hillside	No
Distance to head center, R	0"
Passes through a Category A joint	No

Nozzle

Description	NPS 2 Class 6000 - threaded
Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	2.375"
Nominal wall thickness	0.625"
Corrosion allowance	0"
Projection available outside vessel, Lpr	2.625"
Local vessel minimum thickness	0.85"
Liquid static head included	2.35 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg ₄₁	0.375"
Nozzle to vessel groove weld	0.85"

UCS-66 Material Toughness Requirements Nozzle

$t_r = 252.35 * 1.1875 / (20,000 * 1 - 0.6 * 252.35) =$	0.0151"
Stress ratio $= t_r * E^* / (t_h - c) = 0.0151 * 1 / (0.625 - 0) =$	0.0242
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) $=$	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-44 Summary (in)	
For P = 252.35 psi @ 125 °F							The nozzle passes UG-44	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.0625	0.625

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 252.35 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(2.375, 1.1875 + (0.625 - 0) + (0.85 - 0)) \\
 &= 2.6625 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5(t - C), 2.5(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5(0.85 - 0), 2.5(0.625 - 0) + 0) \\
 &= 1.5625 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 252.3508 \cdot 1.1875 / (20,000 \cdot 1 - 0.6 \cdot 252.3508) \\
 &= 0.0151 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)(c)

$$\begin{aligned}
 t_r &= P \cdot K_1 \cdot D_o / (2 \cdot S \cdot E + 0.8 \cdot P) \\
 &= 252.3508 \cdot 0.9 \cdot 132 / (2 \cdot 20,000 \cdot 1 + 0.8 \cdot 252.3508) \\
 &= 0.7457 \text{ in}
 \end{aligned}$$

Required thickness t_r per Interpretation VIII-1-07-50

$$\begin{aligned}
 t_r &= P \cdot D_o \cdot K / (2 \cdot S \cdot E + 2 \cdot P \cdot (K - 0.1)) \\
 &= 252.35 \cdot 132 \cdot 1 / (2 \cdot 20,000 \cdot 1 + 2 \cdot 252.35 \cdot (1 - 0.1)) \\
 &= 0.8234 \text{ in}
 \end{aligned}$$

This opening does not require reinforcement per UG-36(c)(3)(a)

UW-16(c) Weld Check

Fillet weld: t_{min} = lesser of 0.75 or t_n or t = 0.625 in

t_{c(min)} = lesser of 0.25 or 0.7 * t_{min} = 0.25 in

t_{c(actual)} = 0.7 * Leg = 0.7 * 0.375 = 0.2625 in

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-44 Thickness Check - ASME B16.11 Coupling

Interpretation VIII-1-83-66 has been applied.

$$\begin{aligned} t_{a \text{ App 1-1}} &= P \cdot R_o / (S_n \cdot E + 0.4 \cdot P) + \text{Corrosion} \\ &= 252.3508 \cdot 1.8125 / (20,000 \cdot 1 + 0.4 \cdot 252.3508) + 0 \\ &= 0.0228 \text{ in} \end{aligned}$$

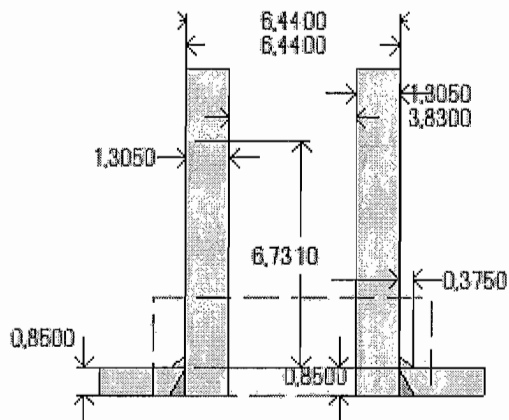
$$\begin{aligned} t_{a \text{ UG-44}} &= \max[t_{a \text{ App 1-1}} , t_{b \text{ UG16}}] \\ &= \max[0.0228 , 0.0625] \\ &= \underline{0.0625} \text{ in} \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.625$ in

The nozzle neck thickness is adequate.

Nozzle N12 - 4" 150# LAHH (N12)

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Note: Per UW-16(b) minimum inside corner radius $r_1 = \min [1 / 4 * t, 0.125 \text{ in}] = 0.125 \text{ in}$

Location and Orientation

Located on	Left Head
Orientation	0°
End of nozzle to datum line	1,022"
Calculated as hillside	Yes
Distance to head center, R	33"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	3.83"
Wall thickness, t_n	1.305"
Minimum wall thickness	1.1175"
Corrosion allowance	0"
Opening chord length	3.9924"
Projection available outside vessel, L_{pr}	7.231"
Heavy barrel length, L_{hb}	6.731"
Projection available outside vessel to flange face, L_f	8.171"
Local vessel minimum thickness	0.85"
Liquid static head included	1.16 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg_{41}	0.375"
--------------------------	--------

Nozzle to vessel groove weld	0.85"
------------------------------	-------

ASME B16.5-2013 Flange	
Description	NPS 4 Class 150 FVC HB A105 (Nut Stop)
Bolt Material	SA-193 B7 Bolt $\leq 2 \frac{1}{2}$ (II-D p. 388, ln. 32)
Blind included	No
Rated MDMT	-31.9°F
Liquid static head	1.16 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Gasket	
Description	Klingsil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -31.9°F (Coincident ratio = 0.8813) Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle At Intersection	
$t_r = 251.16 * 1.915 / (20,000 * 1 - 0.6 * 251.16) =$	0.0242"
Stress ratio = $t_r * E^* / (t_n - c) = 0.0242 * 1 / (1.305 - 0) =$	0.0186
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

UCS-66 Material Toughness Requirements Nozzle	
$t_r = 251.16 * 1.915 / (20,000 * 1 - 0.6 * 251.16) =$	0.0242"
Stress ratio = $t_r * E^* / (t_n - c) = 0.0242 * 1 / (1.1175 - 0) =$	0.0217
Stress ratio ≤ 0.35 , MDMT per UCS-66(b)(3) =	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 251.16 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
2.9632	6.0485	0.4645	5.4434	--	--	0.1406	0.245	1.1175

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 251.16 psi @ 125 °F

Parallel Limit of reinforcement per UG-40 and Fig. UG-40 sketch (e-2)

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(3.9924, 1.9962 + (1.305 - 0) + (0.85 - 0)) \\
 &= 4.1512 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40 and Fig. UG-40 sketch (e-2)

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.85 - 0), 2.5*(1.305 - 0) + 0) \\
 &= 2.125 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 251.1596 \cdot 1.915 / (20,000 \cdot 1 - 0.6 \cdot 251.1596) \\
 &= 0.0242 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)(c)

$$\begin{aligned}
 t_r &= P \cdot K_1 \cdot D_o / (2 \cdot S \cdot E + 0.8 \cdot P) \\
 &= 251.1596 \cdot 0.9 \cdot 132 / (2 \cdot 20,000 \cdot 1 + 0.8 \cdot 251.1596) \\
 &= 0.7422 \text{ in}
 \end{aligned}$$

Required thickness t_r per Interpretation VIII-1-07-50

$$\begin{aligned}
 t_r &= P \cdot D_o \cdot K / (2 \cdot S \cdot E + 2 \cdot P \cdot (K - 0.1)) \\
 &= 251.16 \cdot 132 \cdot 1 / (2 \cdot 20,000 \cdot 1 + 2 \cdot 251.16 \cdot (1 - 0.1)) \\
 &= 0.8196 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: S_n = 20,000, S_v = 20,000 psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$\begin{aligned}
 A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\
 &= 3.9924 \cdot 0.7422 \cdot 1 + 2 \cdot 1.305 \cdot 0.7422 \cdot 1 \cdot (1 - 1) \\
 &= \underline{2.9632 \text{ in}^2}
 \end{aligned}$$

Area available from FIG. UG-37.1

$$A_1 = \text{larger of the following} = \underline{0.4645 \text{ in}^2}$$

$$\begin{aligned}
 &= d \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\
 &= 3.9924 \cdot (1 \cdot 0.85 - 1 \cdot 0.7422) - 2 \cdot 1.305 \cdot (1 \cdot 0.85 - 1 \cdot 0.7422) \cdot (1 - 1) \\
 &= 0.4303 \text{ in}^2 \\
 &= 2 \cdot (t + t_n) \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\
 &= 2 \cdot (0.85 + 1.305) \cdot (1 \cdot 0.85 - 1 \cdot 0.7422) - 2 \cdot 1.305 \cdot (1 \cdot 0.85 - 1 \cdot 0.7422) \cdot (1 - 1) \\
 &= 0.4645 \text{ in}^2
 \end{aligned}$$

$$A_2 = \text{smaller of the following} = \underline{5.4434 \text{ in}^2}$$

$$\begin{aligned}
 &= 5 \cdot (t_n - t_m) \cdot f_{r2} \cdot t \\
 &= 5 \cdot (1.305 - 0.0242) \cdot 1 \cdot 0.85 \\
 &= 5.4434 \text{ in}^2 \\
 &= 5 \cdot (t_n - t_m) \cdot f_{r2} \cdot t_n \\
 &= 5 \cdot (1.305 - 0.0242) \cdot 1 \cdot 1.305 \\
 &= 8.3572 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 A_{41} &= \text{Leg}^2 \cdot f_{r2} \\
 &= 0.375^2 \cdot 1 \\
 &= \underline{0.1406 \text{ in}^2}
 \end{aligned}$$

$$\begin{aligned}
 \text{Area} &= A_1 + A_2 + A_{41} \\
 &= 0.4645 + 5.4434 + 0.1406 \\
 &= \underline{6.0485 \text{ in}^2}
 \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c) Weld Check

Fillet weld: $t_{\min}$ = lesser of 0.75 or t_n or $t = 0.75$ in

$t_{c(\min)}$ = lesser of 0.25 or $0.7 \cdot t_{\min} = \underline{0.25}$ in

$t_{c(\text{actual})} = 0.7 \cdot \text{Leg} = 0.7 \cdot 0.375 = 0.2625$ in

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

Interpretation VIII-1-83-66 has been applied.

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 251.1596 \cdot 1.915 / (20,000 \cdot 1 - 0.6 \cdot 251.1596) + 0 \\
 &= 0.0242 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.0242, 0] \\
 &= 0.0242 \text{ in}
 \end{aligned}$$

$$t_{b1} = 0.8196 \text{ in}$$

$$\begin{aligned}
 t_{b1} &= \max[t_{b1} , t_{b \text{ UG16}}] \\
 &= \max[0.8196 , 0.0625] \\
 &= 0.8196 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_b &= \min[t_{b3} , t_{b1}] \\
 &= \min[0.245 , 0.8196] \\
 &= 0.245 \text{ in}
 \end{aligned}$$

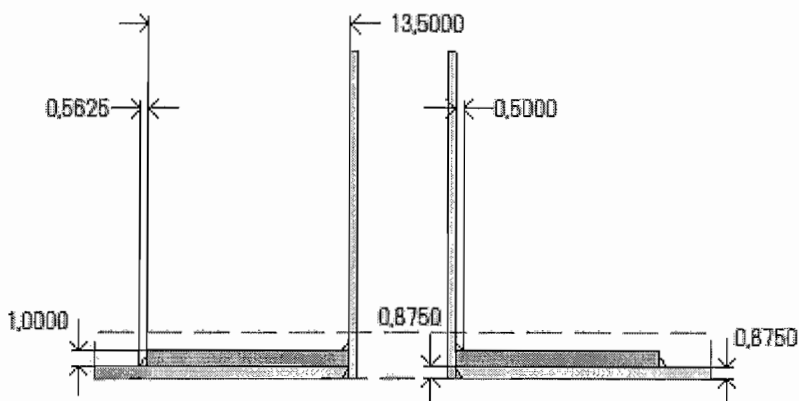
$$\begin{aligned}
 t_{\text{UG-45}} &= \max[t_a , t_b] \\
 &= \max[0.0242 , 0.245] \\
 &= \underline{0.245} \text{ in}
 \end{aligned}$$

Available nozzle wall thickness new, $t_n = 1.1175 \text{ in}$

The nozzle neck thickness is adequate.

Nozzle N13 - 36" 150# Boot (N13)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Shell
Orientation	180°
Nozzle center line offset to datum line	720"
End of nozzle to shell center	138"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-516 70 (II-D p. 18, ln. 33)
Inside diameter, new	35"
Nominal wall thickness	0.5"
Corrosion allowance	0"
Projection available outside vessel, L _{pr}	72"
Local vessel minimum thickness	0.875"
Liquid static head included	4.73 psi
Longitudinal joint efficiency	0.7

Reinforcing Pad

Material specification	SA-516 70 (II-D p. 18, ln. 33)
Diameter, D _p	63"
Thickness, t _c	1"
Is split	No

Welds

Inner fillet, Leg ₄₁	0.5"
---------------------------------	------

Outer fillet, Leg ₄₂	0.5625"
Nozzle to vessel groove weld	0.875"
Pad groove weld	0"

UCS-66 Material Toughness Requirements Nozzle	
Governing thickness, $t_g =$	0.5"
Exemption temperature from Fig UCS-66 Curve B =	-7°F
$t_r = 254.73 \cdot 17.5 / (20,000 \cdot 0.7 - 0.6 \cdot 254.73) =$	0.3219"
Stress ratio $= t_r \cdot E^* / (t_n - c) = 0.3219 \cdot 0.8 / (0.5 - 0) =$	0.5151
Reduction in MDMT, T_R from Fig UCS-66.1 =	55°F
MDMT $= \max[\text{MDMT} - T_R, -55] = \max[-7 - 55, -55] =$	-55°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

UCS-66 Material Toughness Requirements Pad	
Governing thickness, $t_g =$	0.875"
MDMT =	-20°F
Material is exempt from impact testing per UG-20(f) at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 254.73 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
<u>29.2726</u>	<u>30.1237</u>	<u>1.3524</u>	<u>1.2049</u>	--	<u>27</u>	<u>0.5664</u>	<u>0.3281</u>	0.5

UG-41 Weld Failure Path Analysis Summary (lb _f)						
All failure paths are stronger than the applicable weld loads						
Weld load W	Weld load W ₁₋₁	Path 1-1 strength	Weld load W ₂₋₂	Path 2-2 strength	Weld load W ₃₋₃	Path 3-3 strength
<u>559,176.8</u>	<u>575,426</u>	<u>935,860.81</u>	<u>46,598</u>	<u>1,009,393.72</u>	<u>592,926</u>	<u>1,277,823.17</u>

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to pad fillet (Leg ₄₁)	<u>0.35</u>	0.35	weld size is adequate
Pad to shell fillet (Leg ₄₂)	<u>0.375</u>	0.3938	weld size is adequate

Calculations for internal pressure 254.73 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(35, 17.5 + (0.5 - 0) + (0.875 - 0)) \\
 &= 35 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(0.5 - 0) + 1) \\
 &= 2.1875 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_m &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 254.7332 \cdot 17.5 / (20,000 \cdot 1 - 0.6 \cdot 254.7332) \\
 &= 0.2246 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 254.7332 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 254.7332) \\
 &= 0.8364 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: S_n = 20,000, S_v = 20,000, S_p = 20,000 psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$f_{r3} = \text{lesser of } f_{r2} \text{ or } S_p / S_v = 1$$

$$f_{r4} = \text{lesser of } 1 \text{ or } S_p / S_v = 1$$

$$\begin{aligned} A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\ &= 35 \cdot 0.8364 \cdot 1 + 2 \cdot 0.5 \cdot 0.8364 \cdot 1 \cdot (1 - 1) \\ &= \underline{29.2726} \text{ in}^2 \end{aligned}$$

Area available from FIG. UG-37.1

$$A_1 = \text{larger of the following} = \underline{1.3524} \text{ in}^2$$

$$\begin{aligned} &= d \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\ &= 35 \cdot (1 \cdot 0.875 - 1 \cdot 0.8364) - 2 \cdot 0.5 \cdot (1 \cdot 0.875 - 1 \cdot 0.8364) \cdot (1 - 1) \\ &= 1.3524 \text{ in}^2 \\ &= 2 \cdot (t + t_n) \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\ &= 2 \cdot (0.875 + 0.5) \cdot (1 \cdot 0.875 - 1 \cdot 0.8364) - 2 \cdot 0.5 \cdot (1 \cdot 0.875 - 1 \cdot 0.8364) \cdot (1 - 1) \\ &= 0.1063 \text{ in}^2 \end{aligned}$$

$$A_2 = \text{smaller of the following} = \underline{1.2049} \text{ in}^2$$

$$\begin{aligned} &= 5 \cdot (t_n - t_m) \cdot f_{r2} \cdot t \\ &= 5 \cdot (0.5 - 0.2246) \cdot 1 \cdot 0.875 \\ &= 1.2049 \text{ in}^2 \\ &= 2 \cdot (t_n - t_m) \cdot (2.5 \cdot t_n + t_e) \cdot f_{r2} \\ &= 2 \cdot (0.5 - 0.2246) \cdot (2.5 \cdot 0.5 + 1) \cdot 1 \\ &= 1.2393 \text{ in}^2 \end{aligned}$$

$$\begin{aligned} A_{41} &= \text{Leg}^2 \cdot f_{r3} \\ &= 0.5^2 \cdot 1 \\ &= \underline{0.25} \text{ in}^2 \end{aligned}$$

$$\begin{aligned} A_{42} &= \text{Leg}^2 \cdot f_{r4} \\ &= 0.5625^2 \cdot 1 \\ &= \underline{0.3164} \text{ in}^2 \end{aligned}$$

$$\begin{aligned} A_5 &= (D_p - d - 2 \cdot t_n) \cdot t_e \cdot f_{r4} \\ &= (63 - 35 - 2 \cdot 0.5) \cdot 1 \cdot 1 \\ &= \underline{27} \text{ in}^2 \end{aligned}$$

$$\begin{aligned} \text{Area} &= A_1 + A_2 + A_{41} + A_{42} + A_5 \\ &= 1.3524 + 1.2049 + 0.25 + 0.3164 + 27 \\ &= \underline{30.1237} \text{ in}^2 \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c)(2) Weld Check

$$\text{Inner fillet: } t_{\min} = \text{lesser of } 0.75 \text{ or } t_n \text{ or } t_e = 0.5 \text{ in}$$

$$t_{w(\min)} = 0.7 \cdot t_{\min} = \underline{0.35} \text{ in}$$

$$t_{w(\text{actual})} = 0.7 \cdot \text{Leg} = 0.7 \cdot 0.5 = 0.35 \text{ in}$$

$$\text{Outer fillet: } t_{\min} = \text{lesser of } 0.75 \text{ or } t_e \text{ or } t = 0.75 \text{ in}$$

$$t_{w(\min)} = 0.5 \cdot t_{\min} = \underline{0.375} \text{ in}$$

$$t_{w(\text{actual})} = 0.7 \cdot \text{Leg} = 0.7 \cdot 0.5625 = 0.3938 \text{ in}$$

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 257.3322 \cdot 17.5 / (20,000 \cdot 0.7 - 0.6 \cdot 257.3322) + 0 \\
 &= 0.3253 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.3253, 0] \\
 &= 0.3253 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) + \text{Corrosion} \\
 &= 254.7332 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 254.7332) + 0 \\
 &= 0.8364 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\
 &= \max[0.8364, 0.0625] \\
 &= 0.8364 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_b &= \min[t_{b3}, t_{b1}] \\
 &= \min[0.3281, 0.8364] \\
 &= 0.3281 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{\text{UG-45}} &= \max[t_a, t_b] \\
 &= \max[0.3253, 0.3281] \\
 &= \underline{0.3281} \text{ in}
 \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.5 \text{ in}$

The nozzle neck thickness is adequate.

Allowable stresses in joints UG-45 and UW-15(c)

Groove weld in tension: $0.74 \cdot 20,000 = 14,800 \text{ psi}$

Nozzle wall in shear: $0.7 \cdot 20,000 = 14,000 \text{ psi}$

Inner fillet weld in shear: $0.49 \cdot 20,000 = 9,800 \text{ psi}$

Outer fillet weld in shear: $0.49 \cdot 20,000 = 9,800 \text{ psi}$

Strength of welded joints:

(1) Inner fillet weld in shear

$$(\pi / 2) \cdot \text{Nozzle OD} \cdot \text{Leg} \cdot S_i = (\pi / 2) \cdot 36 \cdot 0.5 \cdot 9,800 = 277,088.47 \text{ lb}_f$$

(2) Outer fillet weld in shear

$$(\pi / 2) \cdot \text{Pad OD} \cdot \text{Leg} \cdot S_o = (\pi / 2) \cdot 63 \cdot 0.5625 \cdot 9,800 = 545,517.93 \text{ lb}_f$$

(3) Nozzle wall in shear

$$(\pi / 2) \cdot \text{Mean nozzle dia} \cdot t_n \cdot S_n = (\pi / 2) \cdot 35.5 \cdot 0.5 \cdot 14,000 = 390,342.89 \text{ lb}_f$$

(4) Groove weld in tension

$$(\pi / 2) \cdot \text{Nozzle OD} \cdot t_w \cdot S_g = (\pi / 2) \cdot 36 \cdot 0.875 \cdot 14,800 = 732,305.24 \text{ lb}_f$$

Loading on welds per UG-41(b)(1)

$$\begin{aligned}
 W &= (A - A_1 + 2 \cdot t_n \cdot f_{r1} \cdot (E_1 \cdot t - F \cdot t_r)) \cdot S_v \\
 &= (29.2726 - 1.3524 + 2 \cdot 0.5 \cdot 1 \cdot (1 \cdot 0.875 - 1 \cdot 0.8364)) \cdot 20,000 \\
 &= \underline{559,176.8} \text{ lb}_f
 \end{aligned}$$

$$\begin{aligned}
 W_{1-1} &= (A_2 + A_5 + A_{41} + A_{42}) \cdot S_v \\
 &= (1.2049 + 27 + 0.25 + 0.3164) \cdot 20,000
 \end{aligned}$$

$$= \underline{575,426} \text{ lb}_f$$

$$\begin{aligned} W_{2-2} &= (A_2 + A_3 + A_{41} + A_{43} + 2*t_n*t*f_{r1})*S_v \\ &= (1.2049 + 0 + 0.25 + 0 + 2*0.5*0.875*1)*20,000 \\ &= \underline{46,598} \text{ lb}_f \end{aligned}$$

$$\begin{aligned} W_{3-3} &= (A_2 + A_3 + A_5 + A_{41} + A_{42} + A_{43} + 2*t_n*t*f_{r1})*S_v \\ &= (1.2049 + 0 + 27 + 0.25 + 0.3164 + 0 + 2*0.5*0.875*1)*20,000 \\ &= \underline{592,926} \text{ lb}_f \end{aligned}$$

Load for path 1-1 lesser of W or $W_{1-1} = 559,176.8 \text{ lb}_f$

Path 1-1 through (2) & (3) = $545,517.93 + 390,342.89 = \underline{935,860.81} \text{ lb}_f$

Path 1-1 is stronger than W so it is acceptable per UG-41(b)(2).

Load for path 2-2 lesser of W or $W_{2-2} = 46,598 \text{ lb}_f$

Path 2-2 through (1), (4) = $277,088.47 + 732,305.24 = \underline{1,009,393.72} \text{ lb}_f$

Path 2-2 is stronger than W_{2-2} so it is acceptable per UG-41(b)(1).

Load for path 3-3 lesser of W or $W_{3-3} = 559,176.8 \text{ lb}_f$

Path 3-3 through (2), (4) = $545,517.93 + 732,305.24 = \underline{1,277,823.17} \text{ lb}_f$

Path 3-3 is stronger than W so it is acceptable per UG-41(b)(2).

% Extreme fiber elongation - UCS-79(d)

$$\begin{aligned} EFE &= (50*t / R_f)*(1 - R_f / R_o) \\ &= (50*0.5 / 17.75)*(1 - 17.75 / \infty) \\ &= 1.4085\% \end{aligned}$$

The extreme fiber elongation does not exceed 5%.

Boot Head

ASME Section VIII Division 1, 2017 Edition				
Component		Ellipsoidal Head		
Material		SA-516 70 (II-D p. 18, ln. 33)		
Attached To		Nozzle NI3 - 36" 150# Boot (NI3)		
Impact Tested	Normalized	Fine Grain Practice	PWHT	Optimize MDMT/ Find MAWP
No	No	Yes	No	No
		Design Pressure (psi)	Design Temperature (°F)	Design MDMT (°F)
Internal		250	125	-20
Static Liquid Head				
Condition		P _s (psi)	H _s (in)	SG
Operating		7.72	213.9375	1
Test horizontal		8.19	226.8125	1
Dimensions				
Outer Diameter		36"		
Head Ratio		2		
Minimum Thickness		0.375"		
Corrosion	Inner	0"		
	Outer	0"		
Length L _{sf}		2"		
Nominal Thickness t _{sf}		0.5"		
Weight and Capacity				
		Weight (lb) ¹	Capacity (US gal) ¹	
New		186.03	33.15	
Corroded		186.03	33.15	
Radiography				
Category A joints		Seamless No RT		
Head to shell seam		None UW-11(c) Type 1		

¹ includes straight flange

Results Summary	
Governing condition	internal pressure
Minimum thickness per UG-16	0.0625" + 0" = 0.0625"
Design thickness due to internal pressure (t)	0.2693"
Straight Flange governs MDMT	-55°F

Factor K

$K = (1/6) * [2 + (D / (2 * h))^2]$		
Corroded	$K = (1/6) * [2 + (35.25 / (2 * 8.8125))^2]$	1
New	$K = (1/6) * [2 + (35.25 / (2 * 8.8125))^2]$	1

Design thickness for internal pressure, (Corroded at 125 °F) Appendix 1-4(c)

$$\begin{aligned}
 t &= P * D_o * K / (2 * S * E + 2 * P * (K - 0.1)) + \text{Corrosion} \\
 &= 257.72 * 36 * 1 / (2 * 20,000 * 0.85 + 2 * 257.72 * (1 - 0.1)) + 0 \\
 &= \underline{0.2692"}
 \end{aligned}$$

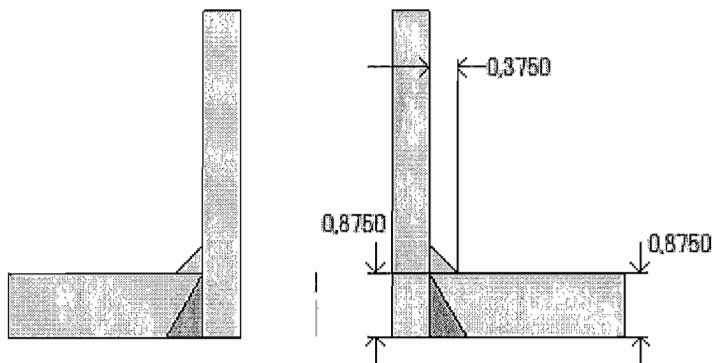
% Extreme fiber elongation - UCS-79(d)

$$\begin{aligned}
 \text{EFE} &= (75 * t / R_f) * (1 - R_f / R_o) \\
 &= (75 * 0.5 / 6.2425) * (1 - 6.2425 / \infty) \\
 &= 6.0072\%
 \end{aligned}$$

The extreme fiber elongation exceeds 5 percent. Heat treatment per UCS-56 may be required. See UCS-79(d)(4) or (5).

Nozzle N14 - 2" 150# HP Drain Recycle (N14)

ASME Section VIII Division 1, 2017 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Shell
Orientation	0°
Nozzle center line offset to datum line	177"
End of nozzle to shell center	74"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	2"
Nominal wall thickness	0.53"
Corrosion allowance	0"
Projection available outside vessel, L _{pr}	7.25"
Projection available outside vessel to flange face, L _f	8"
Local vessel minimum thickness	0.875"
Liquid static head included	0 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg ₄₁	0.375"
Nozzle to vessel groove weld	0.875"

ASME B16.5-2013 Flange

Description	NPS 2 Class 150 LWN A105
Bolt Material	SA-193 B7 Bolt ≤ 2 1/2 (II-D p. 388, ln. 32)

Blind included	No
Rated MDMT	-32.3°F
Liquid static head	0 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Gasket	
Description	Klingersil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -32.3°F (Coincident ratio = 0.8772)	
Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements	
LWN rated MDMT per UCS-66(c)(4) =	-32.3°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 250 psi @ 125 °F							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.189	0.53

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 250 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(2, 1 + (0.53 - 0) + (0.875 - 0)) \\
 &= 2.405 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(0.53 - 0) + 0) \\
 &= 1.325 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P * R_n / (S_n * E - 0.6 * P) \\
 &= 250 * 1 / (20,000 * 1 - 0.6 * 250) \\
 &= 0.0126 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P * R_o / (S * E + 0.4 * P) \\
 &= 250 * 66 / (20,000 * 1 + 0.4 * 250) \\
 &= 0.8209 \text{ in}
 \end{aligned}$$

This opening does not require reinforcement per UG-36(c)(3)(a)

UW-16(c) Weld Check

Fillet weld: t_{min} = lesser of 0.75 or t_n or t = 0.53 in

t_{c(min)} = lesser of 0.25 or 0.7*t_{min} = 0.25 in

t_{c(actual)} = 0.7*Leg = 0.7*0.375 = 0.2625 in

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 250 \cdot 1 / (20,000 \cdot 1 - 0.6 \cdot 250) + 0 \\
 &= 0.0126 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.0126, 0] \\
 &= 0.0126 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) + \text{Corrosion} \\
 &= 250 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 250) + 0 \\
 &= 0.8209 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\
 &= \max[0.8209, 0.0625] \\
 &= 0.8209 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_b &= \min[t_{b3}, t_{b1}] \\
 &= \min[0.189, 0.8209] \\
 &= 0.189 \text{ in}
 \end{aligned}$$

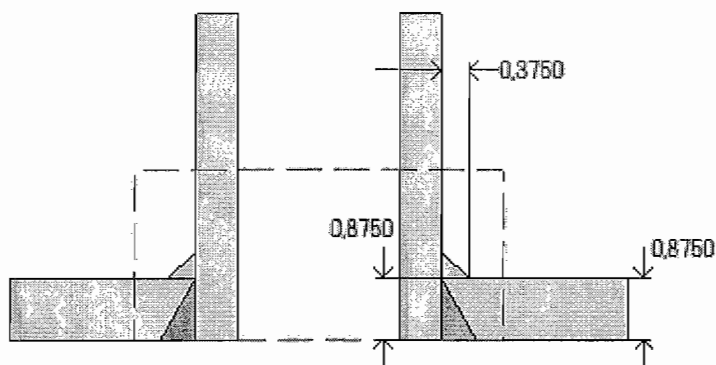
$$\begin{aligned}
 t_{\text{UG-45}} &= \max[t_a, t_b] \\
 &= \max[0.0126, 0.189] \\
 &= \underline{0.189} \text{ in}
 \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.53 \text{ in}$

The nozzle neck thickness is adequate.

Nozzle N15A - 3" 150# Level (Boot Interface) (N15A)

ASME Section VIII Division 1, 2017 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Shell
Orientation	270°
Nozzle center line offset to datum line	720"
End of nozzle to shell center	65"
Offset from center, Lo	-36"
Passes through a Category A joint	No

Nozzle

Description	NPS 3 XXS
Access opening	No
Material specification	SA-106 B Smls pipe (II-D p. 14, ln. 10)
Inside diameter, new	2.3"
Pipe nominal wall thickness	0.6"
Pipe minimum wall thickness ¹	0.525"
Corrosion allowance	0"
Opening chord length	2.7526"
Projection available outside vessel, L _{pr}	5.8325"
Projection available outside vessel to flange face, L _f	8.5825"
Local vessel minimum thickness	0.875"
Liquid static head included	3.65 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg ₄₁	0.375"
---------------------------------	--------

Nozzle to vessel groove weld	0.875"
------------------------------	--------

¹Pipe minimum thickness = nominal thickness times pipe tolerance factor of 0.875.

ASME B16.5-2013 Flange	
Description	NPS 3 Class 150 WN A105
Bolt Material	SA-193 B7 Bolt <= 2 1/2 (II-D p. 388, ln. 32)
Blind included	No
Rated MDMT	-31°F
Liquid static head	3.65 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Circumferential joint radiography	Full UW-11(a) Type 1
Gasket	
Description	Klingsil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -31°F (Coincident ratio = 0.89) Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements Nozzle	
$t_r = 253.65 * 1.15 / (17,100 * 1 - 0.6 * 253.65) =$	0.0172"
$\text{Stress ratio} = t_r * E^* / (t_n - c) = 0.0172 * 1 / (0.525 - 0) =$	0.0328
$\text{Stress ratio} \leq 0.35, \text{MDMT per UCS-66(b)(3)} =$	-155°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 253.65 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
1.2187	2.8881	1.273	1.4949	--	--	0.1202	0.189	0.525

UG-41 Weld Failure Path Analysis Summary

The nozzle is exempt from weld strength calculations per UW-15(b)(1)

UW-16 Weld Sizing Summary

Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 253.65 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(2.7526, 1.3763 + (0.6 - 0) + (0.875 - 0)) \\
 &= 2.8513 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(0.6 - 0) + 0) \\
 &= 1.5 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 253.6503 \cdot 1.15 / (17,100 \cdot 1 - 0.6 \cdot 253.6503) \\
 &= 0.0172 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 253.6503 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 253.6503) \\
 &= 0.8328 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: S_n = 17,100, S_v = 20,000 psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 0.855$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 0.855$$

$$\begin{aligned}
 A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\
 &= 2.7526 \cdot 0.8328 \cdot 0.5 + 2 \cdot 0.6 \cdot 0.8328 \cdot 0.5 \cdot (1 - 0.855) \\
 &= 1.2187 \text{ in}^2
 \end{aligned}$$

Area available from FIG. UG-37.1

$A_1 = \text{larger of the following} = 1.273 \text{ in}^2$

$$\begin{aligned}
 &= d(E_1 * t - F * t_r) - 2 * t_n(E_1 * t - F * t_r)(1 - f_{r1}) \\
 &= 2.7526 * (1 * 0.875 - 0.5 * 0.8328) - 2 * 0.6 * (1 * 0.875 - 0.5 * 0.8328) * (1 - 0.855) \\
 &= 1.1825 \text{ in}^2 \\
 &= 2 * (t + t_n)(E_1 * t - F * t_r) - 2 * t_n(E_1 * t - F * t_r)(1 - f_{r1}) \\
 &= 2 * (0.875 + 0.6) * (1 * 0.875 - 0.5 * 0.8328) - 2 * 0.6 * (1 * 0.875 - 0.5 * 0.8328) * (1 - 0.855) \\
 &= 1.273 \text{ in}^2
 \end{aligned}$$

$A_2 = \text{smaller of the following} = 1.4949 \text{ in}^2$

$$\begin{aligned}
 &= 5 * (t_n - t_{rn}) * f_{r2} * t \\
 &= 5 * (0.6 - 0.0172) * 0.855 * 0.875 \\
 &= 2.18 \text{ in}^2 \\
 &= 5 * (t_n - t_{rn}) * f_{r2} * t_n \\
 &= 5 * (0.6 - 0.0172) * 0.855 * 0.6 \\
 &= 1.4949 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 A_{41} &= \text{Leg}^2 * f_{r2} \\
 &= 0.375^2 * 0.855 \\
 &= 0.1202 \text{ in}^2
 \end{aligned}$$

$$\begin{aligned}
 \text{Area} &= A_1 + A_2 + A_{41} \\
 &= 1.273 + 1.4949 + 0.1202 \\
 &= 2.8881 \text{ in}^2
 \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c) Weld Check

Fillet weld: $t_{\min} = \text{lesser of } 0.75 \text{ or } t_n \text{ or } t = 0.6 \text{ in}$

$t_{c(\min)} = \text{lesser of } 0.25 \text{ or } 0.7 * t_{\min} = 0.25 \text{ in}$

$t_{c(\text{actual})} = 0.7 * \text{Leg} = 0.7 * 0.375 = 0.2625 \text{ in}$

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P * R_n / (S_n * E - 0.6 * P) + \text{Corrosion} \\
 &= 253.6503 * 1.15 / (17,100 * 1 - 0.6 * 253.6503) + 0 \\
 &= 0.0172 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.0172, 0] \\
 &= 0.0172 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= P * R_o / (S * E + 0.4 * P) + \text{Corrosion} \\
 &= 253.6503 * 66 / (20,000 * 1 + 0.4 * 253.6503) + 0 \\
 &= 0.8328 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\
 &= \max[0.8328, 0.0625] \\
 &= 0.8328 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_b &= \min[t_{b3}, t_{b1}] \\
 &= \min[0.189, 0.8328] \\
 &= 0.189 \text{ in}
 \end{aligned}$$

$$\begin{aligned}t_{UG-45} &= \max[t_a, t_b] \\&= \max[0.0172, 0.189] \\&= \underline{0.189} \text{ in}\end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.875 \cdot 0.6 = 0.525$ in

The nozzle neck thickness is adequate.

Reinforcement check in the plane parallel to the longitudinal axis

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 253.65 psi @ 125 °F							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.189	0.525

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(2.3, 1.15 + (0.6 - 0) + (0.875 - 0)) \\
 &= 2.625 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.875 - 0), 2.5*(0.6 - 0) + 0) \\
 &= 1.5 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 253.6503 \cdot 1.15 / (17,100 \cdot 1 - 0.6 \cdot 253.6503) \\
 &= 0.0172 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R_o / (S \cdot E + 0.4 \cdot P) \\
 &= 253.6503 \cdot 66 / (20,000 \cdot 1 + 0.4 \cdot 253.6503) \\
 &= 0.8328 \text{ in}
 \end{aligned}$$

This opening does not require reinforcement per UG-36(c)(3)(a)

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned}
 t_{a \text{ UG-27}} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 253.6503 \cdot 1.15 / (17,100 \cdot 1 - 0.6 \cdot 253.6503) + 0 \\
 &= 0.0172 \text{ in}
 \end{aligned}$$

$$\begin{aligned}
 t_a &= \text{max}[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \text{max}[0.0172, 0] \\
 &= 0.0172 \text{ in}
 \end{aligned}$$

$$t_{bl} = P \cdot R_o / (S \cdot E + 0.4 \cdot P) + \text{Corrosion}$$

$$= 253.6503 * 66 / (20,000 * 1 + 0.4 * 253.6503) + 0$$

$$= 0.8328 \text{ in}$$

$$t_{b1} = \max[t_{b1} , t_{b \text{ UG16}}]$$

$$= \max[0.8328 , 0.0625]$$

$$= 0.8328 \text{ in}$$

$$t_b = \min[t_{b3} , t_{b1}]$$

$$= \min[0.189 , 0.8328]$$

$$= 0.189 \text{ in}$$

$$t_{\text{UG-45}} = \max[t_a , t_b]$$

$$= \max[0.0172 , 0.189]$$

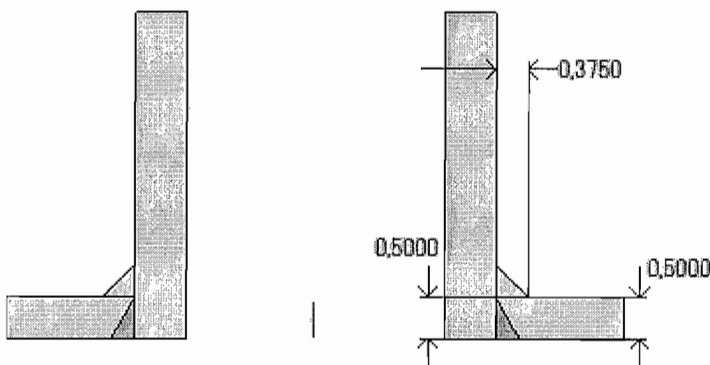
$$= \underline{0.189} \text{ in}$$

Available nozzle wall thickness new, $t_n = 0.875 * 0.6 = 0.525 \text{ in}$

The nozzle neck thickness is adequate.

Nozzle N15C - 3" 150# Water Level Gauge [In Boot] (Nozzle N15B, N17A, & N17B similar) (N15C)

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Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Nozzle N13 - 36" 150# Boot (N13)
Orientation	270°
Nozzle center line offset to face of parent nozzle	6"
End of nozzle to shell center	26"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	3"
Nominal wall thickness	0.625"
Corrosion allowance	0"
Projection available outside vessel, L_{pr}	7.06"
Projection available outside vessel to flange face, L_f	8"
Local vessel minimum thickness	0.5"
Liquid static head included	7.12 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg₄₁	0.375"
Nozzle to vessel groove weld	0.5"

ASME B16.5-2013 Flange

Description	NPS 3 Class 150 LWN A105
Bolt Material	SA-193 B7 Bolt ≤ 2 1/2 (II-D p. 388, ln. 32)

Blind included	No
Rated MDMT	-29.8°F
Liquid static head	7.12 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Gasket	
Description	Klingersil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -29.8°F (Coincident ratio = 0.9022)	
Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements	
LWN rated MDMT per UCS-66(c)(4) =	-29.8°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 257.12 psi @ 125 °F							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.2074	0.625

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 257.12 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(3, 1.5 + (0.625 - 0) + (0.5 - 0)) \\
 &= 3 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.5 - 0), 2.5*(0.625 - 0) + 0) \\
 &= 1.25 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 257.1156 \cdot 1.5 / (20,000 \cdot 1 - 0.6 \cdot 257.1156) \\
 &= 0.0194 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P \cdot R / (S \cdot E - 0.6 \cdot P) \\
 &= 257.1156 \cdot 17.5 / (20,000 \cdot 1 - 0.6 \cdot 257.1156) \\
 &= 0.2267 \text{ in}
 \end{aligned}$$

Required thickness t_r per Interpretation VIII-1-07-50

$$\begin{aligned}
 t_r &= P \cdot R / (S \cdot E - 0.6 \cdot P) \\
 &= 257.1156 \cdot 17.5 / (20,000 \cdot 0.7 - 0.6 \cdot 257.1156) \\
 &= 0.325 \text{ in}
 \end{aligned}$$

This opening does not require reinforcement per UG-36(c)(3)(a)

UW-16(c) Weld Check

Fillet weld: t_{min} = lesser of 0.75 or t_n or $t = 0.5$ in

$t_{c(min)}$ = lesser of 0.25 or $0.7 \cdot t_{min} = 0.25$ in

$t_{c(actual)}$ = $0.7 \cdot \text{Leg} = 0.7 \cdot 0.375 = 0.2625$ in

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-c).

UG-45 Nozzle Neck Thickness Check

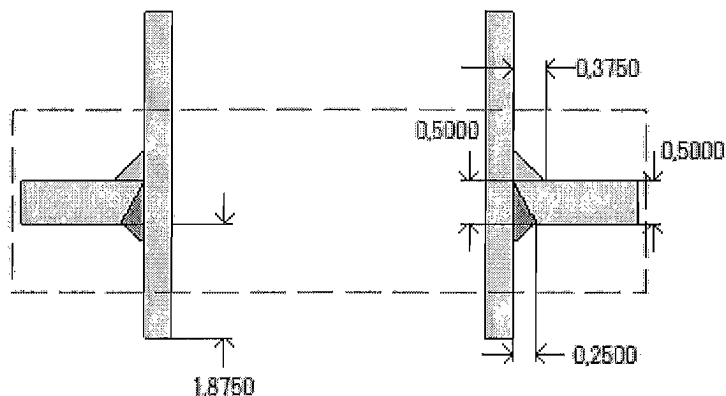
$$\begin{aligned}
 t_{a \text{ UG-27}} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 257.1156 \cdot 1.5 / (20,000 \cdot 1 - 0.6 \cdot 257.1156) + 0 \\
 &= 0.0194 \text{ in} \\
 t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\
 &= \max[0.0194, 0] \\
 &= 0.0194 \text{ in} \\
 t_{b1} &= P \cdot R / (S \cdot E - 0.6 \cdot P) + \text{Corrosion} \\
 &= 257.1156 \cdot 17.5 / (20,000 \cdot 1 - 0.6 \cdot 257.1156) + 0 \\
 &= 0.2267 \text{ in} \\
 t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\
 &= \max[0.2267, 0.0625] \\
 &= 0.2267 \text{ in} \\
 t_b &= \min[t_{b3}, t_{b1}] \\
 &= \min[0.2074, 0.2267] \\
 &= 0.2074 \text{ in} \\
 t_{\text{UG-45}} &= \max[t_a, t_b] \\
 &= \max[0.0194, 0.2074] \\
 &= \underline{0.2074} \text{ in}
 \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.625$ in

The nozzle neck thickness is adequate.

Nozzle N16 - 4" 150# Water Outlet [In Boot] (N16)

ASME Section VIII Division 1, 2017 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Nozzle N13 - 36" 150# Boot (N13)
Orientation	0°
Nozzle center line offset to face of parent nozzle	6"
End of nozzle to shell center	26"
Passes through a Category A joint	No

Nozzle

Description	NPS 4 Sch 80S (XS)
Access opening	No
Material specification	SA-312 TP304 Wld & smls pipe (II-D p. 86, ln. 42)
Inside diameter, new	3.826"
Pipe nominal wall thickness	0.337"
Pipe minimum wall thickness ¹	0.2949"
Corrosion allowance	0"
Projection available outside vessel, L _{pr}	5"
Internal projection, h _{new}	1.875"
Projection available outside vessel to flange face, L _f	8"
Local vessel minimum thickness	0.5"
Liquid static head included	7.12 psi
Longitudinal joint efficiency	0.85

Welds

Inner fillet, Leg ₄₁	0.375"
Lower fillet, Leg ₄₃	0.25"

Nozzle to vessel groove weld

0.5"

¹Pipe minimum thickness = nominal thickness times pipe tolerance factor of 0.875.

ASME B16.5-2013 Flange	
Description	NPS 4 Class 150 WN A105
Bolt Material	SA-193 B7 Bolt <= 2 1/2 (II-D p. 388, ln. 32)
Blind included	No
Rated MDMT	-29.8°F
Liquid static head	7.12 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Circumferential joint radiography	Full UW-11(a) Type 1
Gasket	
Description	Klingersil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -29.8°F (Coincident ratio = 0.9022)	
Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UHA-51 Material Toughness Requirements Nozzle	
$t_r = 257.12 * 1.913 / (20,000 * 0.85 - 0.6 * 257.12) =$	0.0292"
Stress ratio = $t_r * E^* / (t_n - c) = 0.0292 * 0.85 / (0.2949 - 0) =$	0.0842
Impact test exempt per UHA-51(g) (coincident ratio = 0.0842)	
Rated MDMT =	-320°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 257.12 psi @ 125 °F The opening is adequately reinforced							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
0.8674	2.3426	1.0456	0.5261	0.5678	--	0.2031	0.2074	0.2949

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(1)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.2359	0.2625	weld size is adequate

Calculations for internal pressure 257.12 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(3.826, 1.913 + (0.337 - 0) + (0.5 - 0)) \\
 &= 3.826 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.5 - 0), 2.5*(0.337 - 0) + 0) \\
 &= 0.8425 \text{ in}
 \end{aligned}$$

Inner Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_I &= \text{MIN}(h, 2.5*(t - C), 2.5*(t_i - C_n - C)) \\
 &= \text{MIN}(1.875, 2.5*(0.5 - 0), 2.5*(0.337 - 0 - 0)) \\
 &= 0.8425 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_{rn} &= P * R_n / (S_n * E - 0.6 * P) \\
 &= 257.1156 * 1.913 / (20,000 * 1 - 0.6 * 257.1156) \\
 &= 0.0248 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)

$$\begin{aligned}
 t_r &= P * R / (S * E - 0.6 * P) \\
 &= 257.1156 * 17.5 / (20,000 * 1 - 0.6 * 257.1156) \\
 &= 0.2267 \text{ in}
 \end{aligned}$$

Required thickness t_r per Interpretation VIII-1-07-50

$$\begin{aligned}
 t_r &= P * R / (S * E - 0.6 * P) \\
 &= 257.1156 * 17.5 / (20,000 * 0.7 - 0.6 * 257.1156) \\
 &= 0.325 \text{ in}
 \end{aligned}$$

Area required per UG-37(c)

Allowable stresses: $S_n = 20,000$, $S_v = 20,000$ psi

$$f_{r1} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$f_{r2} = \text{lesser of } 1 \text{ or } S_n / S_v = 1$$

$$\begin{aligned} A &= d \cdot t_r \cdot F + 2 \cdot t_n \cdot t_r \cdot F \cdot (1 - f_{r1}) \\ &= 3.826 \cdot 0.2267 \cdot 1 + 2 \cdot 0.337 \cdot 0.2267 \cdot 1 \cdot (1 - 1) \\ &= \underline{0.8674} \text{ in}^2 \end{aligned}$$

Area available from FIG. UG-37.1

$$A_1 = \text{larger of the following} = \underline{1.0456} \text{ in}^2$$

$$\begin{aligned} &= d \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\ &= 3.826 \cdot (1 \cdot 0.5 - 1 \cdot 0.2267) - 2 \cdot 0.337 \cdot (1 \cdot 0.5 - 1 \cdot 0.2267) \cdot (1 - 1) \\ &= 1.0456 \text{ in}^2 \\ &= 2 \cdot (t + t_n) \cdot (E_1 \cdot t - F \cdot t_r) - 2 \cdot t_n \cdot (E_1 \cdot t - F \cdot t_r) \cdot (1 - f_{r1}) \\ &= 2 \cdot (0.5 + 0.337) \cdot (1 \cdot 0.5 - 1 \cdot 0.2267) - 2 \cdot 0.337 \cdot (1 \cdot 0.5 - 1 \cdot 0.2267) \cdot (1 - 1) \\ &= 0.4575 \text{ in}^2 \end{aligned}$$

$$A_2 = \text{smaller of the following} = \underline{0.5261} \text{ in}^2$$

$$\begin{aligned} &= 5 \cdot (t_n - t_{rn}) \cdot f_{r2} \cdot t \\ &= 5 \cdot (0.337 - 0.0248) \cdot 1 \cdot 0.5 \\ &= 0.7805 \text{ in}^2 \\ &= 5 \cdot (t_n - t_{rn}) \cdot f_{r2} \cdot t_n \\ &= 5 \cdot (0.337 - 0.0248) \cdot 1 \cdot 0.337 \\ &= 0.5261 \text{ in}^2 \end{aligned}$$

$$A_3 = \text{smaller of the following} = \underline{0.5678} \text{ in}^2$$

$$\begin{aligned} &= 5 \cdot t_i \cdot f_{r2} \\ &= 5 \cdot 0.5 \cdot 0.337 \cdot 1 \\ &= \underline{0.8425} \text{ in}^2 \\ &= 5 \cdot t_i \cdot f_{r2} \\ &= 5 \cdot 0.337 \cdot 0.337 \cdot 1 \\ &= \underline{0.5678} \text{ in}^2 \\ &= 2 \cdot h \cdot t_i \cdot f_{r2} \\ &= 2 \cdot 1.875 \cdot 0.337 \cdot 1 \\ &= \underline{1.2638} \text{ in}^2 \end{aligned}$$

$$\begin{aligned} A_{41} &= \text{Leg}^2 \cdot f_{r2} \\ &= 0.375^2 \cdot 1 \\ &= \underline{0.1406} \text{ in}^2 \end{aligned}$$

$$\begin{aligned} A_{43} &= \text{Leg}^2 \cdot f_{r2} \\ &= 0.25^2 \cdot 1 \\ &= \underline{0.0625} \text{ in}^2 \end{aligned}$$

$$\begin{aligned} \text{Area} &= A_1 + A_2 + A_3 + A_{41} + A_{43} \\ &= 1.0456 + 0.5261 + 0.5678 + 0.1406 + 0.0625 \\ &= \underline{2.3426} \text{ in}^2 \end{aligned}$$

As Area $\geq$ A the reinforcement is adequate.

UW-16(c) Weld Check

Fillet weld: $t_{\min} = \text{lesser of } 0.75 \text{ or } t_n \text{ or } t = 0.337 \text{ in}$

$t_{c(\min)} = \text{lesser of } 0.25 \text{ or } 0.7 * t_{\min} = \underline{0.2359} \text{ in}$

$t_{c(\text{actual})} = 0.7 * \text{Leg} = 0.7 * 0.375 = 0.2625 \text{ in}$

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

$$\begin{aligned} t_a \text{ UG-27} &= P * R_n / (S_n * E - 0.6 * P) + \text{Corrosion} \\ &= 257.1156 * 1.913 / (20,000 * 0.85 - 0.6 * 257.1156) + 0 \\ &= 0.0292 \text{ in} \end{aligned}$$

$$\begin{aligned} t_a &= \max[t_a \text{ UG-27}, t_a \text{ UG-22}] \\ &= \max[0.0292, 0] \\ &= 0.0292 \text{ in} \end{aligned}$$

$$\begin{aligned} t_{b1} &= P * R / (S * E - 0.6 * P) + \text{Corrosion} \\ &= 257.1156 * 17.5 / (20,000 * 1 - 0.6 * 257.1156) + 0 \\ &= 0.2267 \text{ in} \end{aligned}$$

$$\begin{aligned} t_{b1} &= \max[t_{b1}, t_b \text{ UG16}] \\ &= \max[0.2267, 0.0625] \\ &= 0.2267 \text{ in} \end{aligned}$$

$$\begin{aligned} t_b &= \min[t_{b3}, t_{b1}] \\ &= \min[0.2074, 0.2267] \\ &= 0.2074 \text{ in} \end{aligned}$$

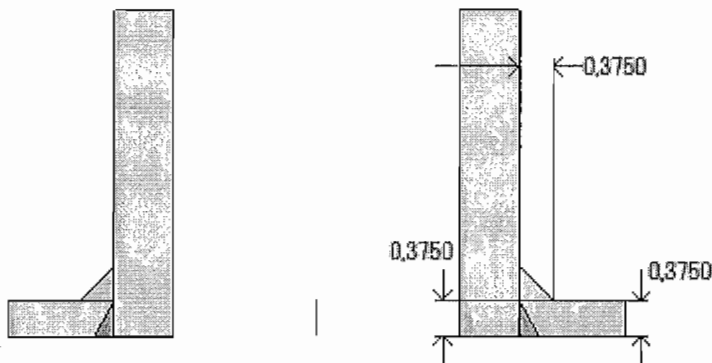
$$\begin{aligned} t_{\text{UG-45}} &= \max[t_a, t_b] \\ &= \max[0.0292, 0.2074] \\ &= \underline{0.2074} \text{ in} \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.875 * 0.337 = 0.2949 \text{ in}$

The nozzle neck thickness is adequate.

Nozzle N18 - 3" 150# Drain [In Boot] (N18)

ASME Section VIII Division 1, 2017 Edition



Note: round inside edges per UG-76(c)

Location and Orientation

Located on	Boot Head
Orientation	0°
End of nozzle to datum line	0"
Calculated as hillside	No
Distance to head center, R	0"
Passes through a Category A joint	No

Nozzle

Access opening	No
Material specification	SA-105 (II-D p. 18, ln. 19)
Inside diameter, new	3"
Nominal wall thickness	0.625"
Corrosion allowance	0"
Projection available outside vessel, L _{pr}	6.9367"
Projection available outside vessel to flange face, L _f	7.8767"
Local vessel minimum thickness	0.375"
Liquid static head included	7.74 psi
Longitudinal joint efficiency	1

Welds

Inner fillet, Leg ₄₁	0.375"
Nozzle to vessel groove weld	0.375"

ASME B16.5-2013 Flange

Description	NPS 3 Class 150 LWN A105
-------------	--------------------------

Bolt Material	SA-193 B7 Bolt $\leq 2 \frac{1}{2}$ (II-D p. 388, ln. 32)
Blind included	No
Rated MDMT	-29.5°F
Liquid static head	8.02 psi
MAWP rating	278.75 psi @ 125°F
MAP rating	285 psi @ 40°F
Hydrotest rating	450 psi @ 40°F
PWHT performed	No
Impact Tested	No
Gasket	
Description	Klingersil C-4401 Synthetic Fiber
Notes	
Flange rated MDMT per UCS-66(b)(1)(b) = -29.5°F (Coincident ratio = 0.9053)	
Bolts rated MDMT per Fig UCS-66 note (c) = -55°F	

UCS-66 Material Toughness Requirements	
LWN rated MDMT per UCS-66(c)(4) =	-29.5°F
Material is exempt from impact testing at the Design MDMT of -20°F.	

Reinforcement Calculations for Internal Pressure

UG-37 Area Calculation Summary (in ²)							UG-45 Summary (in)	
For P = 257.74 psi @ 125 °F							The nozzle passes UG-45	
A required	A available	A ₁	A ₂	A ₃	A ₅	A welds	t _{req}	t _{min}
This nozzle is exempt from area calculations per UG-36(c)(3)(a)							0.2074	0.625

UG-41 Weld Failure Path Analysis Summary
The nozzle is exempt from weld strength calculations per UW-15(b)(2)

UW-16 Weld Sizing Summary			
Weld description	Required weld throat size (in)	Actual weld throat size (in)	Status
Nozzle to shell fillet (Leg ₄₁)	0.25	0.2625	weld size is adequate

Calculations for internal pressure 257.74 psi @ 125 °F

Parallel Limit of reinforcement per UG-40

$$\begin{aligned}
 L_R &= \text{MAX}(d, R_n + (t_n - C_n) + (t - C)) \\
 &= \text{MAX}(3, 1.5 + (0.625 - 0) + (0.375 - 0)) \\
 &= 3 \text{ in}
 \end{aligned}$$

Outer Normal Limit of reinforcement per UG-40

$$\begin{aligned}
 L_H &= \text{MIN}(2.5*(t - C), 2.5*(t_n - C_n) + t_e) \\
 &= \text{MIN}(2.5*(0.375 - 0), 2.5*(0.625 - 0) + 0) \\
 &= 0.9375 \text{ in}
 \end{aligned}$$

Nozzle required thickness per UG-27(c)(1)

$$\begin{aligned}
 t_m &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) \\
 &= 257.7361 \cdot 1.5 / (20,000 \cdot 1 - 0.6 \cdot 257.7361) \\
 &= 0.0195 \text{ in}
 \end{aligned}$$

Required thickness t_r from UG-37(a)(c)

$$\begin{aligned}
 t_r &= P \cdot K_1 \cdot D_o / (2 \cdot S \cdot E + 0.8 \cdot P) \\
 &= 257.7361 \cdot 0.936 / (2 \cdot 20,000 \cdot 1 + 0.8 \cdot 257.7361) \\
 &= 0.2077 \text{ in}
 \end{aligned}$$

Required thickness t_r per Interpretation VIII-1-07-50

$$\begin{aligned}
 t_r &= P \cdot D_o \cdot K / (2 \cdot S \cdot E + 2 \cdot P \cdot (K - 0.1)) \\
 &= 257.74 \cdot 36 \cdot 1 / (2 \cdot 20,000 \cdot 0.85 + 2 \cdot 257.74 \cdot (1 - 0.1)) \\
 &= 0.2692 \text{ in}
 \end{aligned}$$

This opening does not require reinforcement per UG-36(c)(3)(a)

UW-16(c) Weld Check

Fillet weld: t_{min} = lesser of 0.75 or t_n or t = 0.375 in

t_{c(min)} = lesser of 0.25 or 0.7*t_{min} = 0.25 in

t_{c(actual)} = 0.7*Leg = 0.7*0.375 = 0.2625 in

The fillet weld size is satisfactory.

Weld strength calculations are not required for this detail which conforms to Fig. UW-16.1, sketch (c-e).

UG-45 Nozzle Neck Thickness Check

Interpretation VIII-1-83-66 has been applied.

$$\begin{aligned} t_{a \text{ UG-27}} &= P \cdot R_n / (S_n \cdot E - 0.6 \cdot P) + \text{Corrosion} \\ &= 258.0181 \cdot 1.5 / (20,000 \cdot 1 - 0.6 \cdot 258.0181) + 0 \\ &= 0.0195 \text{ in} \end{aligned}$$

$$\begin{aligned} t_a &= \max[t_{a \text{ UG-27}}, t_{a \text{ UG-22}}] \\ &= \max[0.0195, 0] \\ &= 0.0195 \text{ in} \end{aligned}$$

$$t_{b1} = 0.2293 \text{ in}$$

$$\begin{aligned} t_{b1} &= \max[t_{b1}, t_{b \text{ UG16}}] \\ &= \max[0.2293, 0.0625] \\ &= 0.2293 \text{ in} \end{aligned}$$

$$\begin{aligned} t_b &= \min[t_{b3}, t_{b1}] \\ &= \min[0.2074, 0.2293] \\ &= 0.2074 \text{ in} \end{aligned}$$

$$\begin{aligned} t_{\text{UG-45}} &= \max[t_a, t_b] \\ &= \max[0.0195, 0.2074] \\ &= \underline{0.2074 \text{ in}} \end{aligned}$$

Available nozzle wall thickness new, $t_n = 0.625 \text{ in}$

The nozzle neck thickness is adequate.



Eaton Metal Products Company LLC

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(303) 296-4800 FAX: (303) 296-5736

Material Test Reports

Final Bill of Material																			
ASME CODE VESSEL				BY				BY	DATE	JOB NO.	REQUIRED DATE:				12/21/18				
MILL TEST REPORTS REQUIRED AS INDICATED				DATE				RT	10/23/2018	5361-S01	STOCK CHECK:				11/29/18				
				REV				CHK'D	DATE	CUSTOMER	TO PURCHASING:				11/26/18				
								DB	11/26/2018	Anadarko									
Rev	Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Specification	See Note	MTR	Weight	Ship To:	PO No. / Vendor	Manufacturer	Heat & Slab Number	Plate ID		
		5361-1-1	2	HEAD	0.85" MIN x 132" OD ASME 2:1 SF=2"				SA-516-70		X	11263	SLC	44986 CMF	Hyundai	FA38079			
		5361-1-2	4	PLATE	0.875" SHELL, ROLLED	0.875	124.25	411.938	SA-516-70		X	50805	SLC	44980 Evraz	Evraz	N19015, N19840, N19841	35U, 36U, 37U, 38U		
		5361-1-3	4	PLATE	0.875" SHELL, ROLLED	0.875	124.25	411.938	SA-516-70		X	50808	SLC	44980 Evraz	Evraz	N19008, N19833, N19841, N20370	31U, 32U, 33U, 34U		
		5361-1-4	1	PLATE	1/4" PLATE SK	0.250	3.188	9	A-36		X	2	SLC	Stock	Arcelormittal	D0872	38R		
		5361-1-5	1	PLATE	1/4" PLATE	0.250	6	9	A-36			4	SLC	Stock					
		5361-1-6	1	NAMEPL	ASME NAMEPLATE (EMP STD)				STN STL			-	SLC	Purchase by QC					
		5361-1B-1	1	PLATE	1-1/2" BASEPLATE W/ HOLES	1.500	22	129	A-36			1194	SLC	Stock					
		5361-1B-2	1	PLATE	1-1/2" BASEPLATE W/ SLOTS	1.500	22	129	A-36			1187	SLC	Stock					
		5361-1B-3	2	PLATE	3/4" WEB PLATE SKETCH	0.750	53.813	124.75	A-36			1168	SLC	45336 Reliance					
		5361-1B-4	4	PLATE	3/4" END PLATE	0.750	18	53.813	A-36			824	SLC	45336 Reliance					
		5361-1B-5	8	PLATE	3/4" RIB PLATE	0.750	8.625	25.375	A-36			368	SLC	45336 Reliance					
		5361-1B-6	8	PLATE	3/4" RIB PLATE	0.750	8.625	13.688	A-36			199	SLC	45336 Reliance					
		5361-1B-7	4	PLATE	3/4" RIB PLATE	0.750	8.625	10.125	A-36			74	SLC	45336 Reliance					
		5361-1B-8	2	PLATE	3/8" WEAR PLATE, ROLL	0.375	30	175.688	SA-516-70		X	1121	SLC	45335 Ryerson	SSAB	A810J2	40U		
		5361-1B-9	2	PLATE	1/4" PLATE W/HOLE	0.250	2	3	A-36			-	SLC	Stock					
		5361-1C-1	1	FLANGE	20" - 150# RFWN XH BORE				SA-105		X	199	SLC	45009 IPP	Norma	1231			
		5361-1C-2	1	FLANGE	20" - 150# RF BLIND				SA-105		X	271	SLC	45009 IPP	ST&H	805820E			
		5361-1C-3	1	GASKET	1/8" - 20" - 150# RING TYPE KLINGERSIL C-4401				KLINGERSIL			1	SLC	45281 KLINGER					
		5361-1C-4	2	PLATE	1-1/4" SKETCH PL W/ HOLE	1.250	3	5.5	A-36		X	8	SLC	45335 Ryerson	Nucor	8505747	27U		
		5361-1C-5	1	PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	5	SLC	45335 Ryerson	Nucor	8505747	27U		
		5361-1C-6	1	PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	5	SLC	45335 Ryerson	Nucor	8505747	27U		
		5361-1C-7	1	ROD	1" DIA ROD W/ HOLES			15.5	A-36			3	SLC	45335 Ryerson					
		5361-1C-8	1	ROD	3/4" DIA ROD, BEND			12	A-36		X	1	SLC	Stock	Nucor	PL16105676			
		5361-1C-9	20	STUD	1-1/8" DIA FULL THREAD			6.25	SA-193-B7			35	SLC	45302 UINTAH					
		5361-1C-10	40	NUT	1-1/8" HEAVY HEX				SA-194-2H			23	SLC	45302 UINTAH					
		5361-1C-11	2	WASHER	1" STANDARD ROUND				STEEL			-	SLC	45302 UINTAH					
		5361-1C-12	2	COTTER	1/4" DIA COTTER PIN			1.5	STEEL			-	SLC	45302 UINTAH					
		5361-1C-13	1	PIPE	20" NOM XH	0.500		8	SA-106-B		X	69	SLC	45009 IPP	USS	MA6721			
		5361-1C-14	1	PLATE	3/4" CIRC PL 20.25" ID x 33.5" OD	0.750	Shop to Form		SA-516-70		X	119	SLC	45335 Ryerson	SSAB	A81210	39U		
		5361-1D-1	1	FLANGE	36" - 150# SERIES "B" RFWN XH BORE (35" I.D.)				SA-105		X	270	SLC	45009 IPP	Coastal	ACDXJ			
		5361-1D-2	2	FLANGE	24" - 150# RFWN XH BORE				SA-105		X	542	SLC	45009 IPP	ST&H	N13378			
		5361-1D-3	3	FLANGE	6" - 150# RF HB LWN NS			9	SA-105		X	239	SLC	45008 Ameriforge	FVC	DVB			
		5361-1D-4	1	FLANGE	4" - 150# RF HB LWN NS			12.25	SA-105		X	80	SLC	45008 Ameriforge	FVC	EKR			
		5361-1D-5	3	FLANGE	3" - 150# RF HB LWN NS			9	SA-105		X	114	SLC	45008 Ameriforge	FVC	BWL, DXN			
		5361-1D-6	1	FLANGE	3" - 150# RFWN XXH BORE				SA-105		X	13	SLC	45009 IPP	ST&H	012898F			
		5361-1D-7	3	FLANGE	2" - 150# RF LWN			9	SA-105		X	44	SLC	45008 Ameriforge	FVC	DGT			
		5361-1D-8	1	COUPLING	2" - 6000# FULL SCRCD			3.375	SA-105		X	8	SLC	45009 IPP	Bonney Forge	1133			

Final Bill of Material																						
ASME CODE VESSEL				BY					BY	DATE	JOB NO.	REQUIRED DATE:				12/21/18						
MILL TEST REPORTS REQUIRED AS INDICATED				DATE					RT	10/23/2018	5361-S01	STOCK CHECK:				11/29/18						
				REV					CHK'D	DATE	CUSTOMER	TO PURCHASING:				11/26/18						
									D8	11/26/2018	Anadarko											
Rev	Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Specification	See Note	MTR	Weight	Ship To:	PO No. / Vendor	Manufacturer	Heat & Slab Number	Plate ID					
		5361-1D-9	2	PIPE	24" NOM XH	0.500		9.5	SA-106-B		X	199	SLC	45009 IPP	USS	MA2116						
		5361-1D-10	1	PIPE	3" NOM XXH	0.600		10	SA-106-B		X	16	SLC	45009 IPP	TMK	478063						
		5361-1D-11	1	PIPE	3" NOM XH, SKETCH	0.300		2	SA-106-B		X	2	SLC	45009 IPP	Arcelormittal	1609658						
		5361-1D-12	1	PLATE	1/2" PLATE, ROLLED w/4" TANS	0.500	10.938	119.5	SA-516-70		X	173	SLC	45335 Ryerson	Nucor	8505498	30U					
		5361-1D-13	1	PLATE	CIRC 36.25 ID x 63 OD ROLL	1.000			SA-516-70		X	616	SLC	45335 Ryerson	Nucor	8505555	28U					
		5361-1D-14	2	PLATE	CIRC 24.25 ID x 44.5 OD ROLL	0.750			SA-516-70		X	474	SLC	45335 Ryerson	SSAB	A81210	39U					
		5361-1D-15	1	PLATE	PLATE CIRC 10.50" DIA	0.500			A-36			12	SLC	45335 Ryerson								
		5361-1D-16	1	PLATE	1/2" PLATE (VORTEX BRK)	0.500	6	8	SA-516-70		X	7	SLC	45335 Ryerson	Nucor	8505498	30U					
		5361-1D-17	2	PLATE	1/2" SKETCH PL (VORTEX BRK)	0.500	3.75	6	SA-516-70		X	6	SLC	45335 Ryerson	Nucor	8505498	30U					
		5361-1D-18	1	FLANGE	6" - 150# RF BLIND				SA-105		X	25	SLC	45289 MWPS	RNG	5912						
		5361-1D-19	1	FLANGE	3" - 150# RF BLIND				SA-105		X	11	SLC	45289 MWPS	Boltex	T217						
		5361-1D-20	1	GASKET	1/8" - 6" - 150#, RING TYPE, C-4401				KLINGERSIL			1	SLC	45281 KLINGER								
		5361-1D-21	1	GASKET	1/8" - 3" - 150#, RING TYPE, C-4401				KLINGERSIL			-	SLC	45281 KLINGER								
		5361-1D-22	8	STUD	3/4" DIA. FULL THREAD			4.25	SA-193-B7			4	SLC	45302 UINTAH								
		5361-1D-23	16	NUT	3/4" HEAVY HEX				SA-194-2H			3	SLC	45302 UINTAH								
		5361-1D-24	4	STUD	5/8" DIA. FULL THREAD			3.75	SA-193-B7			1	SLC	45302 UINTAH								
		5361-1D-25	8	NUT	5/8" HEAVY HEX				SA-194-2H			-	SLC	45302 UINTAH								
		5361-1E-1	1	HOUSING	VANE PAK HOUSING (BY AMACS)				SA-516-70		X	393	SLC	Furnished by Customer	Nucor	8507558						
		5361-1E-2	1	VANE PAK	VANE PAK W/ DISTRIBUTOR (BY AMACS)				304L SS			500	SLC	Furnished by Customer								
		5361-1E-3	1	PLATE	1/2" WEIR PLATE, SKETCH	0.500	32	112.125	SA-516-70		X	360	SLC	45335 Ryerson	Nucor	8505498	30U					
		5361-1F-1	4	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	50.125	100.25	SA-240-304		X	175	SLC	45335 Ryerson	NAS	A19W	29U					
		5361-1F-2	2	BEAM	W6 x 20 W/HOLES & SLOTS			123.5	304 SS			412	SLC	45349 Ryerson								
		5361-1F-3	4	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	6	7	SA-240-304		X	23	SLC	45335 Ryerson	NAS	A19W	29U					
		5361-1F-4	4	PLATE	1/2" PLATE, SKETCH	0.500	5.25	7	SA-240-304		X	17	SLC	45335 Ryerson	NAS	A19W	29U					
		5361-1F-5	156	NUT	3/8" HEAVY HEX				304 SS			5	SLC	45302 UINTAH								
		5361-1F-6	2	BAFFLE	DISTRIBUTION BAFFLE (BY AMACS)				304L SS			900	SLC	Furnished by Customer								
		5361-1G-1	1	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	30	36	SA-240-304			87	SLC	45335 Ryerson								
		5361-1G-2	1	PIPE	24" NOM XH, SKETCH	0.500		18.688	SA-312-TP304			144	SLC	45289 MWPS								
		5361-1G-3	1	PIPE	24" NOM XH, SKETCH	0.500		23.75	SA-312-TP304			145	SLC	45289 MWPS								
		5361-1G-4	1	PIPE	24" NOM XH, SKETCH	0.500		10.563	SA-312-TP304		X	59	SLC	45289 MWPS	Outokumpu	441917						
		5361-1G-5	2	PLATE	1/2" PLATE W/HOLES	0.500	4	12	SA-240-304			13	SLC	45335 Ryerson								
		5361-1G-6	4	PLATE	1/2" PLATE, SKETCH	0.500	2.25	3.5	SA-240-304			4	SLC	45335 Ryerson								
		5361-1G-7	2	PLATE	1/2" PLATE W/HOLES	0.500	2.5	70	SA-240-304		X	49	SLC	45335 Ryerson	NAS	A19W	29U					
		5361-1G-8	2	PLATE	1/2" PLATE W/HOLE	0.500	5.5	7.813	SA-240-304		X	12	SLC	45335 Ryerson	NAS	A19W	29U					
		5361-1G-9	4	PLATE	1/2" PLATE, SKETCH	0.500	4	9.688	SA-240-304		X	20	SLC	45335 Ryerson	NAS	A19W	29U					
		5361-1G-10	1	PLATE	1/2" PLATE, SKETCH W/HOLES	0.500	6	12	SA-240-304		X	10	SLC	45335 Ryerson	NAS	A19W	29U					
		5361-1G-11	1	DIFFUSER	INLET DIFFUSER ASSY (BY AMACS)				304L SS			942	SLC	Furnished by Customer								

Final Bill of Material																							
ASME CODE VESSEL				BY				BY	DATE	JOB NO.				REQUIRED DATE:			12/21/18						
MILL TEST REPORTS REQUIRED AS INDICATED				DATE				RT	10/23/2018	5361-S01				STOCK CHECK:			11/29/18						
				REV				CHK'D	DATE	CUSTOMER				TO PURCHASING:			11/26/18						
								DB	11/26/2018	Anadarko													
Rev	Ship Pcs	Mark No.	Assy Pcs	Name	Description	Thk Inches	Width Inches	Length Inches	Material Specification	See Note	MTR	Weight	Ship To:	PO No. / Vendor	Manufacturer	Heat & Slab Number	Plate ID						
		5361-1H-1	1	FLANGE	36" - 150# SERIES "B" RFWN XH BORE (35" I.D.)				SA-105		X	270	SLC	45009 IPP	Coastal	ACDXJ							
		5361-1H-2	1	PLATE	1/2" PLATE, ROLLED w/4" TANS	0.500	55.25	119.5	SA-516-70		X	874	SLC	45335 Ryerson	Nucor	8505498	30U						
		5361-1H-3	1	HEAD	0.375" MIN x 36" OD ASME 2:1 SF=2"				SA-516-70		X	228	SLC	44997 CMF	Nucor	8505299							
		5361-1H-4	1	FLANGE	4" - 150# RFWN XH BORE				SA-105		X	16	SLC	45009 IPP	RNG	H6336							
		5361-1H-5	5	FLANGE	3" - 150# RF LWN			9	SA-105		X	127	SLC	45008 Ameriforge	FVC	C1000AF							
		5361-1H-6	1	PIPE	4" NOM XH, SKETCH	0.337		9.25	SA-312-TP304		X	10	SLC	45009 IPP	Seah	N08288							
		5361-1H-7	1	PIPE	4" NOM XH, SKETCH	0.337		24	SA-312-TP304		X	26	SLC	45009 IPP	Seah	N08288							
1		5361-1H-B		GASKET	1/8" - 36" - 150# SERIES "B" RING TYPE C-4401				KLINGERSIL			1	SLC	45281 KLINGER									
44		5361-1H-C		STUD	7/8" DIA FULL THREAD			6.75	SA-193-B7			51	SLC	45302 UINTAH									
88		5361-1H-D		NUT	7/8" HEAVY HEX				SA-194-2H			26	SLC	45302 UINTAH									
		5361-1J-1	2	FLANGE	20" - 150# RFWN XH BORE				SA-105		X	399	SLC	45009 IPP	Norma	1231							
		5361-1J-2	2	FLANGE	20" - 150# RF BLIND				SA-105		X	541	SLC	45009 IPP	ST&H	805820E							
		5361-1J-3	2	GASKET	1/8" - 20" - 150# RING TYPE KLINGERSIL C-4401				KLINGERSIL			2	SLC	45281 KLINGER									
		5361-1J-4	4	PLATE	1-1/4" SKETCH PL W/ HOLE	1.250	3	5.5	A-36		X	16	SLC	45335 Ryerson	Nucor	8505747	27U						
		5361-1J-5	2	PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	9	SLC	45335 Ryerson	Nucor	8505747	27U						
		5361-1J-6	2	PLATE	1-1/4" SKETCH PL W/ SLOT	1.250	4.188	4.813	A-36		X	9	SLC	45335 Ryerson	Nucor	8505747	27U						
		5361-1J-7	2	ROD	1" DIA ROD W/ HOLES			15.5	A-36			7	SLC	45335 Ryerson									
		5361-1J-8	2	ROD	3/4" DIA ROD, BEND			12	A-36		X	3	SLC	Stock	Nucor	PL16105676							
		5361-1J-9	40	STUD	1-1/8" DIA FULL THREAD			6.25	SA-193-B7			70	SLC	45302 UINTAH									
		5361-1J-10	80	NUT	1-1/8" HEAVY HEX				SA-194-2H			46	SLC	45302 UINTAH									
		5361-1J-11	4	WASHER	1" STANDARD ROUND				STEEL			-	SLC	45302 UINTAH									
		5361-1J-12	4	COTTER	1/4" DIA COTTER PIN			1.5	STEEL			-	SLC	45302 UINTAH									
		5361-1J-13	2	PIPE	20" NOM XH	0.500		20.563	SA-106-B		X	357	SLC	45009 IPP	USS	MA6721							
		5361-1J-14	2	PLATE	CIRC 20.25 ID x 39" OD ROLL	1.000			SA-516-70		X	586	SLC	45335 Ryerson	Nucor	8505555	28U						

SA516-70

5361

MK# 1-1

1"

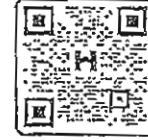
P30709

Reviewed to 2017 ASME Section II

H J J P

검사증명서 MILL TEST CERTIFICATE

HYUNDAI STEEL

 당진제철소 : 충남 당진시 송악읍 죽부산로 1460
 460 Southasan-ro Songsi-eup, Dangjin-Si, Chungnam, Korea

 주문번호
Order No. : E170400143

 품명
Commodity : Hot Rolled Steel Plate

 고객사
Customer : AMERICAN ALLOY

 증명서 번호
Certificate No. : 20170501-PS-022-013

 제품규격
Specification : ASME SA516-70(2013)/ASTM A516-70(2015)

 주문자
Contractor : METAL ONE AMERICA, INC.

 발행일자
Date of Issue : 2017-08-01

제품(수) Dimension	수량 Quantity	중량 Weight (Kg)	제강번호 Heat No.	제품번호 Product No.	Position	인장시험 Tensile Test						화합성분 Chemical Composition(%)														단위 Unit 2"x100 3"x1,000 4"x10,000 5"x100,000		
						YP	TS	EL	YP-EL	RA	YR	YP Mid	C	Mn	P	S	Cr	Ni	B	Cu	Mo	Nb	Ti	V	Se	CSQ		
1"x170"x340"	1	7,436	P30709	FA83807901	T	345.2	524.5	49				2	L	1,713	357	1,136	135	36	14	1	3	26	9	18	2	2	45	409
1"x170"x340"	1	7,436	P30709	FA83807902	T	345.2	524.5	49				2	L	1,713	357	1,136	135	36	14	1	3	26	9	16	2	2	45	409
*** Sub Total(010) *** 2 14,872(Kg)																												
*** Condition of supply: As-Rolled ***																												
*** Test Coupon Heat Treatment ***																												
** Method A *** Applicable test items - Tensile Test																												
** Method A *** 1. Normalizing (Times 1) - Heating Temp: 900°C, Heating Rate: 170°C/Hr Max at above 400°C, Holding Time: 30 Min, Cooling Rate: Air Cooling																												
*** Lot Total *** 106 385,603(Kg) PO/Contract No.: 111005																												
*** Grade Total *** 106 385,603(Kg) Ceq(CS), G = C+Mn/6 + Ni + Cu/15 + (Cr+Mo+V)/5																												
*** Last Item ***																												
APPROVED ASME SEC. II 2015 Ed. _____ Ad. CMF																												
* Position - T: Top, M: Middle, B: Bottom * Tensile test - Direction: Transverse, YP Mid: 2 (0.2% off-set), 5 (0.5% underload), U (Upper yield point), L (Lower yield point) * Division - C: Check analysis, L: Ladle analysis * The plate is fully killed and fine grained steel. Basic oxygen process and Vacuum degassing process were applied. This Mill Test Certificate is issued in accordance with EN 10204 Type 3.1																												
상기 제품 검사와 결과 지정된 규격에 합격한 것을 증명합니다. WE HEREBY CERTIFY THAT THE MATERIAL HAS BEEN MADE AND TESTED IN ACCORDANCE WITH THE ABOVE SPECIFICATION AND THE REQUIREMENTS Signature S. B. Park Chief Of Quality Assurance Team																												

- * 본 검사증명서는 원본의 전자문서(전자시험 정보 포함)로부터 출력된 사용입니다. 전자문서의 내용은 원본과 동일하게 효력을 인정할 수 있습니다. (<http://smhyundai-steel.com/cs/cm/asp/jsp>)
- * This Mill Test Certificate is a copy that has been printed from original electronic document with digital signature.
- * You are able to check an original electronic document at HyundaiSteel's customer portal (<http://smhyundai-steel.com/cs/cm/asp/jsp>) * QRcode scanner App: 'QRReal'
- * [사용상 주의사항] 본 검사증명서에 기재된 규격 외 사용시 제품손상 및 안전상 문제가 발생할 수 있습니다.
- * [Caution for Use] Damage on products and safety problems may arise if used other than to the spec stated in this Mill Test Certificate.



P064675 7/14/17 H



EVRAZ INC. NA

Evraz Oregon Steel 14400 N. Rivergate Blvd., Portland, Oregon 97203

REPORT OF CHEMICAL/PHYSICAL TESTS

CERTIFICATE NO.	DATE	PAGE
1643589	Dec 21, 2018	1
MILL ORDER NO.	DATE	
329921		
CUSTOMER ORDER NO.		
0044980		
JOB/REQ. NO.		
5361-S01 01031		
SHIPPING NO.	DATE	
1643589	12/21/2018	
CARRIER		
Trinity Transport		
CAR/TRUCK NO.		
4F002		

ISO 9001

REGISTERED

U.S. PLATE PRODUCER

SOLD TO

EATON METAL PRODUCTS CO
PO BOX 16405
STOCKYARD STATION
DENVER, CO 80216
US

EATON METAL PRODUCTS CO.
844 CHESTNUT STREET
SALT LAKE CITY, UT 84104

THIS MATERIAL HAS BEEN MANUFACTURED, TESTED AND FOUND TO MEET THE SPECIFICATIONS AND PURCHASE ORDER REQUIREMENTS
CARBON STEEL PRESSURE VESSEL QUALITY PLATE ASTM A516-17 GRADE 70 ASME SA516
GRADE 70 2017. AS ROLLED KILLED FINE GRAIN NO WELD REPAIR. PRESSURE VESSEL
QUALITY.

PHYSICAL PROPERTIES

ITEM NO	DESCRIPTION	HEAT NO.	SLAB	YIELD PSI X 100	TENSILE PSI X 100	% ELONG 8" 2"	% RA	HARDNESS BHN	BEND TEST	IMPACTS
1	0.8750 X 126.000ME X 413.500 PT# SA-516-70									
	1 PC 12929 LBS	^ N19015	A32	570	785	29				35U
	2 PCS 25858 LBS	^ N19840	A22	560	780	23				36U & 37U
	1 PC 12929 LBS	^ N19841	A23	575	810	23				38U
	4 PCS 51716 LBS TOTALS									
										PO# 44980 5361 mk#1-2



CHEMICAL ANALYSIS

HEAT NO.	C	Mn	P	S	Si	Cu	Ni	V	Co	Al	Cr	Mo	Ti	B	N	Ca		CE	Mn/Cu/Al Grain Size
N19015	.19	1.34	.013	.008	.28	.01	.05	.025	.000	.045	.02	.00	.000	.0000					
N19840	.19	1.35	.012	.006	.31	.02	.05	.024	.000	.034	.02	.00	.000	.0000					
N19841	.20	1.33	.013	.006	.30	.01	.05	.024	.000	.041	.02	.00	.000	.0000					
HEATS INDICATED WITH (+) WERE MELTED & MANUFACTURED IN THE USA. HEATS INDICATED WITH (^) WERE ROLLED IN THE USA.																			
..... END OF REPORT																			

I certify the above to be correct as contained in the records of EVRAZ INC. NA By

Aaron Capps

Quality Coordinator



EVRAZ INC. NA

Evraz Oregon Steel 14400 N. Rivergate Blvd., Portland, Oregon 97203

REPORT OF CHEMICAL/PHYSICAL TESTS

CERTIFICATE NO.	DATE	PAGE
1643429	Dec 19, 2018	1
MILL ORDER NO.	DATE	
329921		
CUSTOMER ORDER NO.		
0044980		
JOB/REQ. NO.		
5361-S01 01031		
SHIPPING NO.	DATE	
1643429	12/19/2018	
CARRIER		
Trinity Transport		
CAR/TRUCK NO.		
14		

ISO 9001

REGISTERED

U.S. PLATE PRODUCER

SOLD TO

EATON METAL PRODUCTS CO
PO BOX 16405
STOCKYARD STATION
DENVER, CO 80216
US

EATON METAL PRODUCTS CO.
844 CHESTNUT STREET
SALT LAKE CITY, UT 84104

THIS MATERIAL HAS BEEN MANUFACTURED, TESTED AND FOUND TO MEET THE SPECIFICATIONS AND PURCHASE ORDER REQUIREMENTS
CARBON STEEL PRESSURE VESSEL QUALITY PLATE ASTM A516-17 GRADE 70 ASME SA516
GRADE 70 2017. AS ROLLED KILLED FINE GRAIN NO WELD REPAIR. PRESSURE VESSEL
QUALITY.

PHYSICAL PROPERTIES

ITEM NO.	DESCRIPTION	HEAT NO.	SLAB	YIELD PSI X 100	TENSILE PSI X 100	% ELONG 8" 2"	% RA	HARDNESS BHN	BEND TEST	IMPACTS
1	0.8750 X 126.000ME X 413.500 PT# SA-516-70									
	1 PC 12929 LBS	^ N19008	A33	575	790	23				31U
	1 PC 12929 LBS	^ N19833	A23	575	810	23				32U
	1 PC 12929 LBS	^ N19841	A27	575	810	25				34U
	1 PC 12929 LBS	^ N20370	A22	565	800	22				33U
	4 PCS 51716 LBS TOTALS									5361 PO# 44980 mk# 1-3

CHEMICAL ANALYSIS

HEAT NO.	C	Mn	P	S	Si	Cu	Ni	V	Co	Al	Cr	Mo	Ti	B	N	Ca			CE	McQuaid Ehn Grain Size
N19008	.20	1.31	.015	.006	.28	.01	.05	.024	.000	.037	.02	.00	.000	.0000						
N19833	.20	1.39	.012	.004	.32	.02	.05	.024	.000	.039	.02	.00	.000	.0000						
N19841	.20	1.33	.013	.006	.30	.01	.05	.024	.000	.041	.02	.00	.000	.0000						
N20370	.19	1.33	.015	.005	.33	.01	.05	.024	.000	.040	.03	.00	.002	.0000						

HEATS INDICATED WITH (+) WERE MELTED & MANUFACTURED IN THE USA. HEATS INDICATED WITH (^) WERE ROLLED IN THE USA.

..... END OF REPORT

I certify the above to be correct as contained in the records of EVRAZ INC. NA

By

Aaron Capps

Quality Coordinator

08/29/2017 From: AMERICAN ALLOY STEEL, INC.

To: EATON METAL PRODUCTS

P.O.#: 0043258

S.O.#: 580058

AA PL#: 5187341

Item: 1 (1 PC) 1/4" X 96" X 240"

TAG: MARK# 1B-1

ArceLorMitt

TEST CERTIFICATE

SHIP TO: ARCELORMITTAL PLATE LLC
AMERICAN ALLOY STEEL
C/O SKOL TRACK 21
6350 N ERIE AVE
OWASSO OK 00000

PAGE NO: 01 OF 05
FILE NO: 0284-01-43
MILL ORDER NO: 80489-002
MELT NO: D0872
SLAB NO: 39A
DATE: 07/18/17

SOLD TO: AMERICAN ALLOY STEEL, INC
P. O. BOX 40469
HOUSTON TX 77240-0469

SEND TO:

01-C

STEEL PLATE DIMENSIONS / DESCRIPTION

TOTAL QTY	GAUGE	WIDTH	LENGTH	DESCRIPTION	PIECE WEIGHT
9	.25"	96"	240"	RECTANGLE	1634#

CUSTOMER INFORMATION

CUSTOMER PO: 111583-OK

PART NO. 2

Certified a true copy of the original, retained in our file.
AMERICAN ALLOY STEEL, INC.

SPECIFICATION(S)

THIS MATERIAL HAS BEEN MANUFACTURED AND TESTED IN ACCORDANCE WITH PURCHASE ORDER REQUIREMENTS AND SPECIFICATION(S).

ASTM A516 YR 10 GR 70
ASTM A516 YR 10 GR 65
ASTM A516 YR 10 GR 60
ASME SA516 ED 15 GRADE 70
ASME SA516 ED 15 GRADE 65
ASME SA516 ED 15 GRADE 60
PRODUCT OF COIL

THE MANAGEMENT SYSTEMS FOR MANUFACTURE OF THIS PRODUCT ARE CERTIFIED TO ISO 9001:2008 (CERTIFICATE NO. 30130) AND ISO 14001:2004 (CERTIFICATE NO. 49009).

CHEMICAL COMPOSITION (WT%) FOR ALL ELEMENTS EXCEPT H (PPM)

MELT: D0872	C .20	MN .93	P .015	S .004	CU .28	SI .19	NI .16	CR .19	MO .04
MELT: D0872	V .002	TI .003	B .0002	AL .019	CB .001				

Reviewed to 2017 ASME section II



5361-1
MK# 1-4
ID# 38R

AMERICAN ALLOY
PLATE # 5187341

WE HEREBY CERTIFY THE ABOVE INFORMATION IS CORRECT:

ARCELORMITTAL PLATE LLC
QUALITY ASSURANCE LABORATORY
139 MODENA ROAD
COATESVILLE, PA 19320

[Signature]

SUPERVISOR - TEST REPORTING
LOC TRAN

08/29/2017 From: AMERICAN ALLOY STEEL, INC.

To: EATON METAL PRODUCTS

P.O.#: 0043258

S.O.#: 580050

AA PL#: 5187341

Item: 1 (1 PC) 1/4" X 96" X 240"

TAG: MARK# 1B-1

TEST CERTIFICATE

PAGE NO: 03 OF 05
FILE NO: 0284-01-43
MILL ORDER NO: 80489-002
MELT NO: D0872
SLAB NO: 39A
DATE: 07/18/17

HEAT TREAT CONDITION

SET TWO

MATL OR TEST	HEAT TREAT DESCRIPTION	NOM TEMP	HOLD MINS	COOL MTHD
TEST ONLY	NORMALIZE	1650F	30	AIR COOL

TENSILE PROPERTIES

SET TWO

SLAB NO.	LOC	DIR	YIELD STRENGTH PSI X 1000	TENSILE STRENGTH PSI X 1000	ELONGATION AFTER FRACTURE GAGE LGTH	%
39A	BOT.	TRANS.	55	75	8.00"	22.0
39A	MID.	TRANS.	56	77	8.00"	23.0
39A	TOP	TRANS.	57	77	8.00"	23.0

WE HEREBY CERTIFY THE ABOVE
INFORMATION IS CORRECT:

ARCELORMITTAL PLATE LLC
QUALITY ASSURANCE LABORATORY
138 MODENA ROAD
COATESVILLE, PA 19320



Loc Tran

SUPERVISOR - TEST REPORTING
LOC TRAN

08/29/2017 From: AMERICAN ALLOY STEEL, INC.

To: EATON METAL PRODUCTS

P.O.#: 0043258

S.O.#: 580058

AA PL#: 5187341

Item: 1 (1 PC) 1/4" X 96" X 240"

TAG: MARK# 1B-1

TEST CERTIFICATE

PAGE NO: 04 OF 05

FILE NO: 0284-01-43

MILL ORDER NO: 80489-002

MELT NO: D0872

SLAB NO: 39A

DATE: 07/18/17

GENERAL INFORMATION

ALL STEEL HAS BEEN MELTED AND MANUFACTURED IN THE U.S.A.
TEST CERTS. ARE PREPARED IN ACCORD. WITH PROCEDURES
OUTLINED IN EN10204:2004 TYPE 3.1
MERCURY OR MERCURY COMPOUNDS ARE NOT USED IN THE
MANUFACTURE OF ARCELORMITTAL PLATE LLC PRODUCTS.
ALL STEEL HAS BEEN MANUFACTURED IN THE U.S.A.
ACID SOLUBLE ALUMINUM
FOR MORE INFORMATION AND PROCESSING GUIDELINES, REFER TO
WWW.USA.ARCELORMITTAL.COM/PLATE

MERCURY OR MERCURY COMPOUNDS ARE NOT USED IN THE MANUFACTURE OF
ARCELORMITTAL PLATE LLC PRODUCTS.

B/L #17519 TTPX 80714



WE HEREBY CERTIFY THE ABOVE
INFORMATION IS CORRECT:

ARCELORMITTAL PLATE LLC
QUALITY ASSURANCE LABORATORY
139 MODENA ROAD
COATESVILLE, PA 19320

SUPERVISOR - TEST REPORTING
LOC TRAN

08/29/2017 From: AMERICAN ALLOY STEEL, INC.

To: EATON METAL PRODUCTS

P.O.#: 0043258

S.O.#: 580058

AA PL#: 5187341

Item: 1 (1 PC) 1/4" X 96" X 240"

TAG: MARK# 1B-1

TEST CERTIFICATE

PAGE NO: 05 OF 05
FILE NO: 0284-01-43
MILL ORDER NO: 80489-002
MELT NO: D0872
SLAB NO: 39A
DATE: 07/18/17

MEXICAN GOVERNMENT PRODUCT IDENTIFICATION REQUIREMENTS:

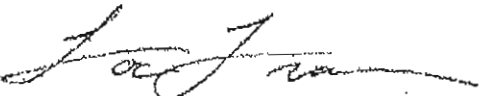
01. PRODUCT DESCRIPTION: HOT ROLLED CARBON STEEL PLATE CUT TO LENGTH
02. TYPE OF STEEL: NON-ALLOY
03. TYPE OF COATING USED: N/A
04. TYPE OF FINISHING OR COMPLEMENTARY MANUFACTURING: N/A
05. PROPRIETARY STANDARD: ASTM A516 YR 10 GR 70
ASTM A516 YR 10 GR 65
ASTM A516 YR 10 GR 60
ASME SA516 ED 15 GRADE 70
ASME SA516 ED 15 GRADE 65
ASME SA516 ED 15 GRADE 60
06. PRODUCT PRESENTATION: PLATE
07. ACCESSORIES INTEGRATED TO THE GOOD: N/A
08. PRODUCT DIMENSIONS: GAUGE WIDTH LENGTH
.25 96 240 INCHES
6.35MM 2438.4MM 6096MM MILLIMETERS
09. TECHNICAL SPECIFICATION: N/A
10. PHYSICAL SPECIFICATIONS: NORMALIZE AIR COOL
11. COUNTRY OF ORIGIN: USA
12. CHEMICAL COMPOSITION: (WEIGHT %) DETAILED IN MILL TEST REPORT
13. PRODUCING MILL: ARCELORMITTAL PLATE LLC
SUPERVISOR TEST REPORTING, QUALITY, 930
139 MODENA ROAD
COATESVILLE, PA 19320

CONTACT PERSON: LOC TRAN
PHONE: (610) 238-7579
EMAIL: MAILTO:LOC.TRAN@ARCELORMITTAL.COM
14. CERTIFICATE NUMBER: D0872
15. PLATE IDENTIFIER: 39A



WE HEREBY CERTIFY THE ABOVE
INFORMATION IS CORRECT:

ARCELORMITTAL PLATE LLC
QUALITY ASSURANCE LABORATORY
139 MODENA ROAD
COATESVILLE, PA 19320


SUPERVISOR - TEST REPORTING
LOC TRAN

SSAB

Test Certificate

Form TCI: Revision 3: Date 7 Feb 2018

1770 Bill Sharp Boulevard, Muscatine, IA 52761-9412, US

Customer: JOSEPH T. RYERSON & SON, INC. ACCOUNTS PAYABLE DEPT. PO BOX 91601 LUBBOCK TX 79490-1601			Customer P.O. No.: 4500000445			Mill Order No.: 41-550133-01			Shipping Manifest #: MFC359274									
Product Description: ASTM A516-70(17)/ASME SA516-70(17)						Ship Date: 15 Oct 18			Cert No: 861737010									
Size: 0.375 X 96.00 X 240.0 (IN)						Cert Date: 15 Oct 18			(Page 1 of 1)									
Tested Pieces			Tensiles					Charpy Impact Tests										
Heat Id	Piece Id	Tested Thickness	Tst Loc	YS (KSI)	UTS (KSI)	%RA	Elong % 2in	Elong % 8in	Tst Dir	Hardness	Abs. Energy (FT-LB) 1 2 3 Avg	% Shear 1 2 3 Avg	Tst Temp	Tst Dir	Tst Size (mm)	BDWUT Temp	% Shr	
AB1012	C54	0.373 (DISCUT)	15	55	77		29		T									
Chemical Analysis																		
Heat Id	C	Mn	P	S	Si	Total Al	Sol Al	Cu	Ni	Cr	Mg	Ca	V	Ti	B	Nb	ORGN	
AB1012	.17	.93	.009	.002	.17	.026	.023	.28	.09	.11	.03	.000	.024	.006	.0002	.38	USA	
KILLED STEEL MERCURY IS NOT A METALLURGICAL COMPONENT OF THE STEEL AND NO MERCURY WAS INTENTIONALLY ADDED DURING THE MANUFACTURE OF THIS PRODUCT. KILLED STEEL, PRODUCED TO A FINE GRAIN PRACTICE CEV (IIV) = C + MN/6 + (CR+MO+V)/5 + (NI+CU)/15 NACE MR0175/ISO15156-2:2015 ANNEX A2.1.2 COMPLIANT WTR EN 10204:2004 INSPECTION CERTIFICATE 3.1 COMPLIANT 100% MELTED AND MANUFACTURED IN THE USA. NO WELD REPAIR HAS BEEN PERFORMED ON THIS MATERIAL. PRODUCTS SHIPPED: AB1012 C54 PCS: 0, LBS: 19500																		
Cust Part #: 160004835						WE HEREBY CERTIFY THAT THIS MATERIAL WAS TESTED IN ACCORDANCE WITH, AND MEETS THE REQUIREMENTS OF, THE APPROPRIATE SPECIFICATION						Brian Wales SSAB METAL PRODUCTS COMPANY						

P045335
ID 400
5361

mk# 1B-8



5361-1 Reviewed to 2017 ASME Section II
mk# 1C-1, 1J-1

NORMA (INDIA) LIMITED				Works Test Certificate			
48, Site IV industrial Area, Sahibabad, Ghaziabad-201010 (U.P) INDIA. Tel: 91-120-2896091, 2895404 Fax: 91-120-2895930 E-mail: normaindia@gmail.com							
NORMA/LAB NO-6539/14-15		INVOICE NO. E-400		DATE:-13-10-14			
P. Order. No:	503/005034	Customer:-		Forging specification		ASME SA105 -09	
Component	20"-150# WNRF XH FLG.			ASTM A105 -12			
Drawing No.		Quantity:-		Steel Supplier		Adhumik Metaliks Ltd.	
Machining STD	ANSI B16.5- 2009 ASME B16.5- 2009			09Nos.		Mill Heat No.	
TEST RESULTS				NORMA HEAT NO-1231			
CHEMICAL COMPOSITION				MECHANICAL PROPERTIES.			
Elements %	Specified Composition	Actual		PROPERTIES	SPECIFIED	OBTAINED	Specified carbon as per Purchase Order 0.25max.
		NORMA LAB	MILL T.C.				
Carbon	0.35max.	0.20	0.20	Yield Strength (mpa)	250.00 min.	321.65	Serrated face as per MSS-SP-6 With in limits of 125-250AARH
Manganese	0.60-1.05	1.11	1.10				
Silicon	0.10-0.35	0.18	0.20	Tensile Strength (mpa)	485.00 min.	521.86	CARBON EQUIVALENT (CE) $CE = C + \frac{Mn}{6} + \frac{Cr}{5} + \frac{Mo}{5} + \frac{V}{15} + \frac{Ni}{15} + \frac{Cu}{15}$
Sulphur	0.040max.	0.012	0.015				
Phosphorous	0.035max.	0.016	0.015	%Elongation in 50mm / 4D	22.00 min	31.76	MARKING AS PER MSS-SP-25-2008 20"-150 XH SA/A105 1231 B16.5 NORMA INDIA.
Chromium	0.30max.	0.012	0.014				
Nickel	0.40max.	0.009	0.007	Hardness HB.	187. max.	149-163	
Copper	0.40max.	0.012	0.009				
Molybdenum	0.12max.	0.004	0.001	% Reduction of Area	30.00 min.	61.01	
Vanadium	0.080max.	0.004	0.002				
Carbon Equivalent (CE)	0.47max.	0.390	0.387	Remarks:- We here by certify that the material described here in has been tested in accordance with the applicable specifications referred above and meets the requirements as per EN10204/3.1B & NACE Standard-MR0175-2003. "As per ASTM A105 Table 1 Note:-For each reduction of 0.01% below the specified carbon maximum(0.35%)an increase of 0.06% manganese above the specified maximum (1.05%)will be permitted up to maximum 1.35% & NACE Standard MRO175/ISO15156 Standard Country of Origin-India.		Checked by: Metallurgist	
						Certified by: Quality Control Manager	



CERTIFICATE OF INSPECTION & TEST (EN 10204 3.1)



ST&H CORPORATION

74, Jwadongsunhwan-ro, Haeundae-gu, Busan, Korea

Tel : +82.51.744-4680(5 line) Fax : +82.51.744-4670

E-mail : qm@stnhcorp.com



Certificate No. MJH0003A-19/25

Date : AUG. 21. 2018

Customer

Certified to ISO9001/ ISO14001:2015, PED2014/68/EC by LRQA

Contract No. 202261-00-1ST

Spec. For Material ASTM A105N-14, ASME SA105N-17, NACE MR0175/ISO 15156-2:2015, NACE MR0103/ISO 17495-1:2016

Heat Treatment 930°C NORMALIZED & A.C

Dimensional inspection ASME B16.5 - 2017

ITEM / SIZE	Q'ty	Heat No./ Batch No.	Size of Test Specimen		Tension Test				Hardness Test (HB)	Charpy Impact Test (10X10mm Specimen Size)						
					Max	Y.S	T.S	E.L		R.A	Indiv.	Ave.	Notch	Temp.		
			MPa	MPa		%	%									
			D mm	GL mm		Min	250	485	22.0	30.0					187	21J
12.5	50.0							Test Result (J)			Ave.(J)					
BA150BR16	150LBS BL RF 16"	60	805820D	12.5	50.0		323	518	33	75	152	156	143	120	118	127
BA150BR20	150LBS BL RF 20"	60	805820E	12.5	50.0		323	518	33	75	152	156	143	120	118	127
	BLANK		BLANK													

5361-1
mk# 1C-2, 1J-2

Heat No./ Batch No.	Max Min	Chemical Composition (%)										NDE		
		C	Si	Mn	P	S	NI	Cr	Mo	Cu	V	CE	UT	MT
		0.350	0.350	1.050	0.035	0.040	0.400	0.300	0.120	0.400	0.080			
		0.100	0.600											
805820D	H	0.184	0.258	1.040	0.012	0.005	0.007	0.016	0.002	0.023	0.001	0.363		
	P	0.175	0.250	1.030	0.014	0.004	0.007	0.019	0.003	0.023	0.001	0.353		
805820E	H	0.184	0.258	1.040	0.012	0.005	0.007	0.016	0.002	0.023	0.001	0.363		
	P	0.175	0.250	1.030	0.014	0.004	0.007	0.019	0.003	0.023	0.001	0.353		

REMARK

* H : Heat Analysis P : Product Analysis

* Impact Test performed according to ASTM A370 & MESC 76/210/2017 Paragraph 8.5 / Table 4 & 5.

* C:Mn = 1±5

* Mn is Permitted up to Max 1.65% (ASTM A105-14 TABLE 1, NOTE 1.)



We hereby certify that the material herein has been made and tested in accordance with the above specification and also with the requirements called for by the above order.

Witnessed by / H. J. LEE

Manager of QA Dept / JAY KIM

ST-801-14-02

ST&H CORPORATION

NUCOR
PLATE MILL

P.O.Box 279
Winton, NC 27986
(252) 366-3700

Mill Test Report

Page 1

1605 River Rd
Coffield, NC 27922
(252) 366-3700

NUCOR
By: Cha Nann...

Issuing Date : 09/12/2018 B/L No. : 512940 Load No. : 623425 Our Order No. : 159438/1 Cust. Order No. : 4500893649
Vehicle No: NOIKL 725090 Sold To: RYERSON PROCUREMENT CORP Ship To: RYERSON INC, DENVER
Specification: 1.2600" x 96.000" x 240.000" PO BOX 91601 6600 HIGHWAY 05
ASTM A36-14/ASTM A709 Grade 35-18/AASHTO M270 Grade 35/ASME LUDBOCK, TX 79490 COMMERCE CITY, CO 80022
SA36 2015/2017 AASHTO M270-2017 35
Marking : 160005004

Heat No	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al(tot)	V	Nb	Ti	N	Ca	B	Sn	Coq	Pcm
0505747	0.20	0.04	0.010	0.004	0.19	0.19	0.09	0.10	0.01	0.025	0.003	0.002	0.002		0.0042	0.0003	0.011	0.39	0.26

Plate Serial No	Pieces	Tons	Tensile Test			
			Yld.	Tensile	Elong. % in 2"	Elong. % in 8"
8505747-01	3	12.25	40,900	69,700	27.2	
			41,000	70,100	20.7	



Manufactured to fully killed fine grain practice by Electric Arc Furnace. Welding or weld repair was not performed on this material. Mercury has not been used in the direct manufacturing of this material. Produced as continuous cast electric plate as noted, unless otherwise noted in Specification. For Mexico shipments: nhs-SalesMX@Nucor.com
Yield by 0.5EUL method unless otherwise specified. Coq = $C + (Mn/5) + ((Cr + Mo + V)/5) + ((Cu + Ni)/16)$
Pcm = $C + (Si/30) + (Mn/20) + (Cu/20) + (Ni/60) + (Cr/20) + (Mo/15) + (V/10) + S$
Noted and Manufactured in the USA, ISO 9001:2008 certified (#010940) by SRI Quality System Registrar (00885-09) PED 97/23/EC 7/2 Annex 1, Para 4.3 Compliant
DIN 60349 3.1, EN 10204 3.1(2004), DIN EN 10204 3.1(2005) compliant. For ABS grades only, Quality Assurance certificate 14-1AN/PQA-723

We hereby certify that the contents of this report are accurate and correct. All test results and operations performed by the material manufacturer are in compliance with the applicable specifications, including customer specifications.

T. A. Deparis
T. A. Deparis, Metallurgist

9/13/2018 8:48:15 AM

5361-1
PL ID # 270
mk # 1C-4, 5, 6
1S-4, 5, 6

NUCOR
NUCOR CORPORATION
NUCOR STEEL UTAH

Mill Certification
10/11/2016

MTR #: U1-357740
 PO Box 100
 7285 West 21200 North
 PLYMOUTH, UT 84330
 (435) 458-2300
 Fax: (435) 458-2309

Sold To: INTSEL STEEL WEST LLC
 PO BOX 21119
 HOUSTON, TX 77226-1119

Ship To: INTSEL STEEL WEST
 1887 SOUTH 700 WEST
 SALT LAKE CITY, UT 84104
 (801) 433-2210
 Fax: (801) 972-6145

Customer P.O.	SLC-12130	Sales Order	268246.4
Product Group	Merchant Bar Quality	Part Number	3000075024004W0
Grade	A36/A529GR50/CSA44W/50W	Lot #	PL1610567651
Size	3/4" (.7500) Round	Heat #	PL16105676
Product	3/4" (.7500) Round 20'A36/A529-50/44W/50W	B.L. Number	U1-548929
Description	A36/A529-50/44W/50W	Load Number	U1-357740
Customer Spec		Customer Part #	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Roll Date: 8/13/2016 Melt Date: 8/10/2016 Qty Shipped LBS: 11,895 Qty Shipped Pcs: 396

ASTM A36/A36M-12, A709/709M-13 GR36, ASME SA36-10 Ed '11 Ad.
 ASME SA36-2010 EDITION-2011 ADDENDA
 ASTM A709/A709M-13 GR 36 [250]

C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Cb
0.19%	0.72%	0.010%	0.045%	0.24%	0.23%	0.09%	0.13%	0.018%	0.0016%	0.000%

Yield 1: 51,498psi

Yield 2: 50,764psi

Weight Variation 000.0%

Tensile 1: 73,816psi

Tensile 2: 73,645psi

Elongation: 28% in 8"(% in 203.3mm)

Elongation 26% in 8"(% in 203.3mm)

Specification Comments: MEETS THE REQUIREMENTS OF: ASTM A36/A36M-12, A529/A529-05 GR50, CSA G40.21-04 GR44W(300W)&GR50W(350W) AASHTO M270/M270M-12 GR36(270), ASME SA36/SA36M-07

Comments: NUCOR - PLYMOUTH IS AN I.S.O. 9001 AND AN A.B.S. CERTIFIED MILL
 CMTR COMPLIES WITH DIN EN 10204 - 3.1

1. ALL MANUFACTURING PROCESSES OF THE STEEL MATERIALS IN THIS PRODUCT, INCLUDING MELTING, CASTING, AND HOT ROLLING HAVE OCCURRED WITHIN THE UNITED STATES. ALL PRODUCTS PRODUCED ARE WELD FREE. MERCURY, IN ANY FORM, HAS NOT BEEN USED IN THE PRODUCTION OR TESTING OF THIS MATERIAL.
 2. PROPOSITION 65 WARNING: THIS PRODUCT CONTAINS A CHEMICAL KNOWN TO THE STATE OF CALIFORNIA TO CAUSE CANCER AND/OR BIRTH DEFECTS OR OTHER REPRODUCTIVE HARM. FOR MORE INFORMATION, PLEASE CALL 1-435-458-2300.

Reviewed to 2017 ASME Section II

5361-1
 MK# 1C-8, 1J-8



Ryan Pennington

Ryan Pennington
 Division Metallurgist

5361-1
MK#1C-13

Reviewed to 2017 ASME Section II



UNITED STATES STEEL CORPORATION

TUBULAR PRODUCTS
CERTIFIED TEST REPORT

(IN ACCORDANCE WITH ISO 10474/EN10204/DIN50049 "type 3.1")

DATE: 11/30/14
TIME: 04:05:47
SERIAL NO: L0054107

MILL ORDER/ITEM NO DR00652 08		SHIPPER'S NO. R03446		P.O. NUMBER 10P15701-CA		VEHICLE ID GONX310310												
SOLD TO ADDRESS				MAIL TO ADDRESS				VENDOR UNITED STATES STEEL CORP. LORAIN TUBULAR OPERATIONS 2199 EAST 28TH ST. LORAIN, OH 44055										
SPECIFICATION AND GRADE PIPE CARBON SMLS STD PIPE API 5L--45TH EDITION DATED 12/1/12 PSL-2 GRADE B AND GRADE X42 R N OR Q ASTM A53--12 GRADE B ASTM A106--13 GRADE B/C SPECIAL OD TOLERANCE ASME SA53--2013 EDITION GRADE B ASME SA106--2013 EDITION GRADE B/C BLK REG MILL COAT PE BEV 30 DEG MERTING ALL THE APPLICABLE REQUIREMENTS OF NACE STANDARD MR-01-75 *:ISO 15156-2 2009 ED AND MR-0103-2012 ED																		
MATERIAL COND: AS ROLLED				O.D.: 20.000 (508.000)		WALL: 0.500 (12.700)												
PRODUCT IDENTIFICATION	TENSILE TEST TYPE/ ORIENTATION	TEST COND.	GAUGE WIDTH IN	YIELD	EXT %	TENSILE	Y/T	ELONG %	HARDNESS	MIN HYDRO	DWELL(SEC)							
				PSI	.50	PSI		(IN 2")	SCALE:	PSI								
MA6721 F157AA X83582 E795AA	STRIP/L/B STRIP/L/B	AR AR	1.500 1.500	MIN: 42100 MAX: 71800	.50 .50	MIN: 70000 MAX: 95000	MAX: 0.93 0.65 0.62	MIN: 29.0 39.7 45.5	MIN: 1900 1900	5 5								
				** END OF DATA THIS SHEET **														
LEGEND: L - LONGITUDINAL U - UPSET T - TRANSVERSE NM - NORMALIZED QT - QUENCH & TEMPERED SR - STRESS RELIEVED AR - AS ROLLED G - BODY W - WELD TR - THERMOMECHANICAL ROLLED																		
PRODUCT IDENTIFICATION	TYPE	C	MN	P	S	SI	CU	NI	CR	MO	AL	N	V	B	TI	CB	CO	C.E.*
		MAX																
MA6721	HEAT	19	104	010	003	23	16	08	09	02	025	03	0003	002	003			.41
MA6721 F157AA	PROD	20	104	007	002	24	15	07	08	03	026	03	0002	001	001			.42
MA6721 F157AA	PROD	20	104	006	003	24	16	07	08	02	027	03	0002	001	001			.42
X83582	HEAT	20	104	008	007	23	02	01	09	01	038	03	0002	002	001			.40
X83582 E795AA	PROD	19	105	004	005	25	02	01	08	01	041	03	0001	002	003			.40
X83582 E795AA	PROD	21	105	003	009	25	01	01	08	01	042	03	0005	002	006			.41
** END OF DATA THIS SHEET **																		
*C.E. IS BASED ON THE FOLLOWING EQUATION(S): $CE = C + MN/6 + (CR + MO + V)/5 + (NI + CU)/15$																		



DECIMAL POSITIONS FOR ELEMENTS ARE INDICATED BY THE LEFT MARGIN, VERTICAL DOTTED LINE OR DECIMAL POINT. ELEMENTS REPORTED IN MASS FRACTION (%)



UNITED STATES STEEL CORPORATION

TUBULAR PRODUCTS

CERTIFIED TEST REPORT

(IN ACCORDANCE WITH ISO 10474/EN10204/DIN50849 "type 3.1")

DATE: 11/30/14

TIME: 04:05:47

SERIAL NO: L0054107

MILL ORDER/ITEM NO DR00652 08		SHIPPERS NO. R03446		P.O. NUMBER 10P15701-CA		0019012											
MATERIAL COND: AS ROLLED				O.D.: 20.000 (508.000)				WALL: 0.500 (12.700)									
PRODUCT IDENTIFICATION	FLAT	BEND	DRAIN SIZE	MIN COLLAPSE	DIR	TEST LOC.	TEMP	SIZE	TEST COND.	CHARPY V-NOTCH IMPACT TESTING FT-LBS				% SHEAR			
					DEG F				1	2	3	AVG	1	2	3	AVG	
MA6721 F157AA X83582 E795AA	OK OK				T	B	+ 32	3/4	AR	58	77	60	65	40	60	50	50
					T	B	+ 32	3/4	AD	100	94	104	99	100	100	100	100
** END OF DATA THIS SHEET **																	
LEGEND L - LONGITUDINAL T - TRANSVERSE B - BODY W - WELD HAZ - HEAT AFFECTED ZONE																	
TESTING / INSPECTION INFORMATION																	
TEST / INSPECTION				YES	RESULTS / COMMENTS												
FULL LENGTH VISUAL				X													
FULL LENGTH EMI				X	OD	X	OD/ID		L	X	LT		10.0% NOTCH				
FULL LENGTH MPI																	
FULL LENGTH UT				X	ID	X	OD/ID		L	X	LT		10.0% NOTCH				
END AREA INSPECTION (PLAIN END)				X	MPI	X	UT										
SPECIAL END AREA (SEA) INSP					MPI		UT										
FULL LENGTH DRIFT					DRIFT MANDREL SIZE:												
ADDITIONAL NOTES/COMMENTS																	
MELTED AND MANUFACTURED IN THE USA, NO REPAIRS BY WELDING, NO MERCURY COMPOUNDS ARE ADDED TO THE STEEL AND ALL MERCURY BEARING EQUIPMENT IS PROTECTED BY A DOUBLE BOUNDARY OF CONTAINMENT.. MANUFACTURED IN AN ISO 9001 CERTIFIED FACILITY - CERTIFICATE #32022. PRODUCT WAS HOT ROLLED AND HOT FINISHED																	

THIS IS TO CERTIFY THAT THE PRODUCT DESCRIBED HEREIN WAS MANUFACTURED,
 SAMPLED, TESTED AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION
 AND FULFILLS THE REQUIREMENTS IN SUCH RESPECTS.

PREPARED BY THE OFFICE OF: **BRAD KOURY - MANAGER, Q.A.**

DATE 11/30/14





UNITED STATES STEEL CORPORATION

TUBULAR PRODUCTS
ADDITIONAL COMMENTS SHEET

DATE: 11/30/14

TIME: 04:05:51

PAGE: 1 OF 1

MILL ORDER/ITEM NO. DR00652 08	SHIPPERS NO.	P.O. NUMBER 10P15701-CA	HEAT	SERIAL NUMBER: L0054107
SOLD TO ADDRESS		MAIL TO ADDRESS		VENDOR UNITED STATES STEEL CORP LORAIN TUBULAR OPERATIONS 2199 EAST 28TH ST. LORAIN, OH 44055

HEAT MA6721 - MELTED AT:NUCOR STEEL MEMPHIS, MEMPHIS, TN 38109
HEAT X83582 - MELTED AT:FAIRFIELD WORKS, FAIRFIELD, AL 35064
END OF DATA



Test Certificate

Form TCI; Revision 3; Date 7 Feb 2018

1770 Dill Sharp Boulevard, Muscatine, IA 52761-9412, US

Customer: JQSEPH.T. RYKISON & SON, INC. ACCOUNTS PAYABLE DEPT. PO BOX 91601 LATHROP TX 79490-1601		Customer P.O. No.: 4500999993		MHI Order No.: 41-549855-01		Shipping Manifest: MT359173											
Product Description: ASTM A516-70(17)/ASME SA516-70(17)				Ship Date: 12 Oct 18 Cert Date: 12 Oct 18		Cert No: 061736667 (Page 1 of 1)											
Size: 0.750 X 9.5.00 X 240.0 (IN)																	
Tested Pieces			Tensiles			Charpy Impact Tests											
Heat Id	Piece Id	Tested Thickness	Tst Loc	YS (KSI)	UTS (KSI)	%RA	Elong % 2in 8in										
AB1210	C09	0.748 (DISCRT)	L	55	76		35 T										
				Hardness													
				Abs. Energy (FTLB) 1 2 3 Avg													
				% Shear 1 2 3 Avg													
				Tst Tmp													
				Tst Dir													
				Tst Sts (mm)													
				MHWAT Temp %Str													
Chemical Analysis																	
Heat Id	C	Mn	P	S	Si	Tot Al	Sol Al	Cu	NI	Cr	Mo	Cb	V	Ti	B	HW	ORGN
AB1210	.17	.99	.010	.002	.17	.028	.026	.28	.11	.08	.02	.001	.030	.002	.0003	.38	USA
KILLED STEEL MERCURY IS NOT A METALLURGICAL COMPONENT OF THE STEEL AND NO MERCURY WAS INTENTIONALLY ADDED DURING THE MANUFACTURE OF THIS PRODUCT. KILLED STEEL, PRODUCED TO A FINE GRAIN PRACTICE CEV (IIN) = C + MN/6 + (CR+NO+V)/5 + (NI+CU)/15 KTR EN 10204:2004 INSPECTION CERTIFICATION 3.1 COMPLIANT 100% MELTED AND MANUFACTURED IN THE USA. NO WELD REPAIR HAS BEEN PERFORMED ON THIS MATERIAL. PRODUCTS SHIPPED: AB1210 C09 PCNR: 2, LDS: 9802																	
mk# 1C-14 ID-14 P046335 ID 39U 5361																	
WE HEREBY CERTIFY THAT THIS MATERIAL WAS TESTED IN ACCORDANCE WITH, AND MEETS THE REQUIREMENTS OF, THE APPROPRIATE SPECIFICATION Brian Walgs SENIOR METALLURGY PRODUCT																	



COASTAL FLANGE

P.O. BOX 40443
HOUSTON, TX 77240-0443

MATERIAL CERTIFICATION

745671001 MTR #: 857

Page : 1 of 1

SOLD TO:

SHIP TO:

DATE	SALES ORDER #	CUST P.O.#	TAG NUMBER	SPECIFICATION
04/08/2016	160414	S630278		SA105
ITEM #	QTY	ITEM DESCRIPTION		HEAT CODE
7		36" 150# RF WN XH "B" ASME B16.47		ACDXJ

CHEMICAL ANALYSIS									
C	Mn	P	S	SI	Cr	NI	Mo	V	Cu
.20	.94	.006	.004	.29	.025	.021	.005	.001	.012

PHYSICAL PROPERTIES						HEAT TREATMENT
Tensile PSI	Yield PSI	Elongation	REDUCTION OF AREA %	BHN	BHN	
75565	47427	33	60	149	147	



SUPPLEMENTAL INFORMATION

I hereby certify that the reported figures are correct, as contained in the records of the corporation and that the material was manufactured in the United States of America under a ISO:9001:2008 certified Quality Management System. NACE MRO175 EN 10204 3.1

5361-1
mk# 10-1, 14-1

Reviewed to ASME 2017 Section II

Production Assistant

5361-1
mk# 10-2

CERTIFICATE OF INSPECTION & TEST (EN 10204 3.1)



ST&H CORPORATION

74, Jwadongsunhwan-ro, Haeundae-gu, Busan, Korea
Tel : +82.51.744-4680(5 line) Fax : +82.51.744-4670
E-mail : qm@stnhcorp.com



CE
KPS 20000 / 01

Certificate No. MJH0029A-05/08

Date : JUL 25. 2018

Customer

Certified to ISO9001/ ISO14001:2015, PED2014/68/EC by LRQA

Contract No. 203880-00-1ST

Spec. For Material ASTM A105N-14, ASME SA105N-17, NACE MR0175/ISO 15156-2:2015, NACE MR0103/ISO 17495-1:2016

Heat Treatment 930°C NORMALIZED & A.C

Dimensional inspection ASME B16.5 - 2017

ITEM / SIZE	Q'ty	Heat No./ Batch No.	Size of Test Specimen		Tension Test				Hardness Test (HB)		Charpy Impact Test (10X10mm Specimen Size)			
			D mm	GL mm	Max Min	Y.S MPa	T.S MPa	E.L %	R.A %	187	Indiv. 21J	Ave. 27J	Notch V	Temp. -29°C
			12.5	50.0		250	485	22.0	30.0		Test Result (J)			Ave.(J)
BA300WRSTD20	300LBS WN RF STD 20"	5 N08178	12.5	50.0		324	506	38	70.5	143 146	48	80	73	67
BA600WRXH16	600LBS WN RF XH 16"	30 N08178	12.5	50.0		324	506	38	70.5	143 146	48	80	73	67
BA150BF24	150LBS BL RF 24"	10 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121
BA150BR22	150LBS BL RF 22"	5 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121
BA150BR24	150LBS BL RF 24"	100 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121
BA150WRXH24	150LBS WN RF XH 24"	5 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121
BA300BR20	300LBS BL RF 20"	10 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121
BA300WR4024	300LBS WN RF S40 24"	10 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121
BA600BR18	600LBS BL RF 18"	5 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121
BA900BR18	900LBS BL RF 18"	5 N13378	12.5	50.0		364	506	32	65.5	143 146	123	129	112	121

Heat No./ Batch No.	Max Min	Chemical Composition (%)										NDE		
		C	Si	Mn	P	S	NI	Cr	Mo	Cu	V	CE	UT	MT
		0.350	0.350	1.050	0.035	0.040	0.400	0.300	0.120	0.400	0.080			
			0.100	0.600										
N08178	H	0.199	0.220	1.040	0.014	0.005	0.005	0.014	0.002	0.013	0.001	0.376		
	P	0.195	0.216	1.050	0.012	0.003	0.008	0.021	0.001	0.012	0.001	0.375		
N13378	H	0.169	0.273	0.964	0.015	0.004	0.009	0.018	0.002	0.013	0.002	0.335		
	P	0.173	0.271	0.952	0.011	0.002	0.009	0.022	0.002	0.012	0.001	0.338		

BLANK

REMARK

* H : Heat Analysis P : Product Analysis

* Impact Test performed according to ASTM A370 & MESG 76/210/2017 Paragraph 8.5 / Table 4 & 5.

* C:Min = 1≤5

[Signature]

Witnessed by / H. J. LEE



Manager of Q.A Dept. / JAY KIM

ST&H CORPORATION

We hereby certify that the material herein has been made and tested in accordance with the above specification and also with the requirements called for by the above order.

ST-801-14-02

Material Test Report

Heat Code: **DVB**

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

Sales: (713) 393-4200

ISO 9001:2015 Certified

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 1
4800 York Street		Item Code: HBN060150090A001A1	Qty Shipped: 2	
Denver, CO 80216		Item Desc: HBN RF 6"150X9" SA105		
		Mill Heat: A181215		
Spec: ASTM A105/A105M-(18) /ASME SA 105/SA 105M-(17) Section II Part A				

Element	(%wt)	Ladle	Product	EPCRA	CAS#	Element	(%wt)	Ladle	Product	EPCRA	CAS#
C Carbon	0.19	✓				Cr Chromium	0.14	✓		✓	7440-47-3
Mn Manganese	1.13	✓		✓	7439-96-5	Mo Molybdenum	0.03	✓			
Mn:C	5.9	✓				V Vanadium	0.032	✓			
P Phosphorous	0.006	✓				Cb Columbium	0.001				
S Sulphur	0.003	✓				C.E.	0.43				
Si Silicon	0.27	✓				CuNiCrMoV	0.422				
Cu Copper	0.15	✓		✓	7440-50-8	CrMo	0.17				
Ni Nickel	0.07	✓		✓	7440-02-0						

5361-1
mk# 1D-3

Mechanical Testing					Other	
Test Lab	AFG	VD			YES	
Test Bar Size	SACRIFICIAL PIECE	Fully Killed			YES	
HBW	163 - 163					
Elg (%)	28					
RA (%)	52					
Tensile Specimen Size (in)	.494					
Tensile (ksi)	77.8					
Yield (ksi)	51.4					
Gauge Length (in)	2					



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1348576

Certification Date: 10/27/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b

Material Test Report

Heat Code: DVB

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 1
4800 York Street		Item Code: HBN060150090A001A1	Qty Shipped: 2	
Denver, CO 80216		Item Desc: HBN RF 6"150X9" SA105		
		Mill Heat: A181215		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A				

MARK #1D-3

Product compliant with NACE MR0175/ISO 15156-2:2015, Annex A (A.2.1.2, A2.1.3).

- * No Weld repair performed.
- * Ladle Chemical Analysis results are reported from the raw material suppliers MTR.
- * Tensile taken from a round specimen. Measurement of elongation after fracture.
- * Yield strength was determined using the .2% offset method, unless otherwise specified.
- * All material supplied under this order is certified to be free of mercury contamination and no mercury bearing equipment was used in manufacturing, fabrication or testing.
- * When reported on MTR: Tensile Testing Per ASTM E8; Brinell Hardness Per ASTM E10; Charpy Testing Per ASTM E23
- * AF Global manufactures materials according to a certified Quality Management System conforming to ISO 9001:2015

Unless otherwise noted on PO, Dimensions of all standard pipe flanges and flange fittings (NPS 1/2 to NPS 24) per ASME B16.5-2013, large diameter steel flanges (NPS 26 to 60) per ASME B16.47-2011, Orifice flanges per ASME B16.36-2015.

- * FVC FLANGE DIMENSIONS & BOLTING COMPLY - ASME B16.5
- SELF-REINFORCING NOZZLES COMPLY WITH SPECIFICATION OF SECTION VIII DIV. 1 OR DIV. 2 PER CUSTOMER DESIGN/FVC DESIGN.



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1348576

Certification Date: 10/27/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b

Rina Sane - Metallurgical Lab Manager

Material Test Report

Heat Code: **EKR**

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 2
4800 York Street		Item Code: HBN040150140A001SP	Qty Shipped: 1	
Denver, CO 80216		Item Desc: HBN SA105 150# 4" x 12.25" RF		
		Mill Heat: C149949		
Spec: ASTM A105/A105M-(18) / ASME SA 105/SA 105M-(17) Section II Part A				

Element	(%wt)	Ladle	Product	EPCRA	CAS#	Element	(%wt)	Ladle	Product	EPCRA	CAS#
C	Carbon	0.18				Cr	Chromium	0.09			7440-47-3
Mn	Manganese	1.11		16	7439-96-5	Mo	Molybdenum	0.04			
P	Phosphorous	0.009				V	Vanadium	0.034			
S	Sulphur	0.003				Cb	Columbium	0.001			
Si	Silicon	0.26				C.E.		0.42			
Cu	Copper	0.18		16	7440-50-8	CuNiCrMoV		0.554			
Ni	Nickel	0.21		16	7440-02-0	CrMo		0.13			

5361-1
mk# 1D-4

Mechanical Testing		Other	
Test Lab	AFG	VD	YES
HBW	163 - 163	Fully Killed	YES
Elg (%)	56	Made to Fine Grain Practice	YES
RA (%)	72		
Tensile Specimen Size (in)	.491		
Tensile (ksi)	80		
Yield (ksi)	54.9		
Gauge Length (in)	2		



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III) of the Superfund Amendments and Reauthorization Act of 1986 and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1350715

Certification Date: 11/10/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b

Material Test Report

Heat Code: EKR

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc 00011756 4800 York Street Denver, CO 80216	PO: 0045008	Sales Order: 169271	Line: 2
	Item Code: HBN040150140A001SP		Qty Shipped: 1
	Item Desc: HBN SA105 150# 4" x 12.25" RF		
	Mill Heat: C149949		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A			

MARK #1D-4

Product compliant with NACE MR0175/ISO 15156-2:2015, Annex A (A.2.1.2, A2.1.3).

- * No Weld repair performed.
- * Ladle Chemical Analysis results are reported from the raw material suppliers MTR.
- * Tensile taken from a round specimen. Measurement of elongation after fracture.
- * Yield strength was determined using the .2% offset method, unless otherwise specified.
- * All material supplied under this order is certified to be free of mercury contamination and no mercury bearing equipment was used in manufacturing, fabrication or testing.
- * When reported on MTR: Tensile Testing Per ASTM E8; Brinell Hardness Per ASTM E10; Charpy Testing Per ASTM E23
- * AF Global manufactures materials according to a certified Quality Management System conforming to ISO 9001:2015

Unless otherwise noted on PO, Dimensions of all standard pipe flanges and flange fittings (NPS 1/2 to NPS 24) per ASME B16.5-2013, large diameter steel flanges (NPS 26 to 60) per ASME B16.47-2011, Orifice flanges per ASME B16.36-2015.

* FVC FLANGE DIMENSIONS & BOLTING COMPLY - ASME B16.5
SELF-REINFORCING NOZZLES COMPLY WITH SPECIFICATION OF SECTION VIII DIV. 1 OR DIV. 2 PER CUSTOMER DESIGN/FVC DESIGN.



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1350715

Certification Date: 11/10/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b


Rina Sane - Metallurgical Lab Manager

Page 2 of 2

Material Test Report

FVC
an **AFGlobal** Company

Heat Code: **DXN**

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

Sales: (713) 393-4200

ISO 9001:2015 Certified

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 3
4800 York Street		Item Code: HBN030150090A001A1	Qty Shipped: 1	
Denver, CO 80216		Item Desc: HBN RF 3"150X9" SA105		
		Mill Heat: A181216		
Spec: ASTM A105/A105M-(18) / ASME SA 105/SA 105M-(17) Section II Part A				

Element	(%wt)	Ladle	Product	EPCRA	CAS#	Element	(%wt)	Ladle	Product	EPCRA	CAS#
C	Carbon	0.17				Cr	Chromium	0.11			7440-47-3
Mn	Manganese	1.12			7439-96-5	Mo	Molybdenum	0.03			
Mn:C		6.5				V	Vanadium	0.034			
P	Phosphorous	0.006				Cb	Columbium	0.000			
S	Sulphur	0.002				C.E.		0.41			
Si	Silicon	0.26				CuNiCrMoV		0.354			
Cu	Copper	0.18			7440-50-8	CrMo		0.14			
Ni	Nickel	0.07			7440-02-0						

5361-1
mk# 10-5

Mechanical Testing					Other	
Test Lab	AFG	VD			YES	
Test Bar Size	3.5X3.5X12	Fully Killed			YES	
HBW	163 - 163					
Elg (%)	30					
RA (%)	71					
Tensile Specimen Size (in)	0.490					
Tensile (ksi)	78.3					
Yield (ksi)	52.8					
Gauge Length (in)	2					



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1980) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1350283

Certification Date: 11/8/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b

Material Test Report

Heat Code: DXN

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 3
4800 York Street		Item Code: HBN030150090A001A1	Qty Shipped: 1	
Denver, CO 80216		Item Desc: HBN RF 3"150X9" SA105		
		Mill Heat: A181216		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A				

MARK #1D-5

Product compliant with NACE MR0175/ISO 15156-2:2015, Annex A (A.2.1.2, A2.1.3).

- * No Weld repair performed.
- * Ladle Chemical Analysis results are reported from the raw material suppliers MTR.
- * Tensile taken from a round specimen. Measurement of elongation after fracture.
- * Yield strength was determined using the .2% offset method, unless otherwise specified.
- * All material supplied under this order is certified to be free of mercury contamination and no mercury bearing equipment was used in manufacturing, fabrication or testing.
- * When reported on MTR: Tensile Testing Per ASTM E8; Brinell Hardness Per ASTM E10; Charpy Testing Per ASTM E23
- * AF Global manufactures materials according to a certified Quality Management System conforming to ISO 9001:2015

Unless otherwise noted on PO, Dimensions of all standard pipe flanges and flange fittings (NPS 1/2 to NPS 24) per ASME B16.5-2013, large diameter steel flanges (NPS 26 to 60) per ASME B16.47-2011, Orifice flanges per ASME B16.36-2015.

* FVC FLANGE DIMENSIONS & BOLTING COMPLY - ASME B16.5
SELF-REINFORCING NOZZLES COMPLY WITH SPECIFICATION OF SECTION VIII DIV. 1 OR DIV. 2 PER CUSTOMER DESIGN/FVC DESIGN.



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1350283

Certification Date: 11/8/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b


Rina Sane - Metallurgical Lab Manager

Page 2 of 2

Material Test Report

FVC
an **AFGlobal** Company

Heat Code: **BWL**

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

Sales: (713) 393-4200

ISO 9001:2015 Certified

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 3
4800 York Street		Item Code: HBN030150090A001A1	Qty Shipped: 2	
Denver, CO 80216		Item Desc: HBN RF 3"150X9" SA105		
		Mill Heat: A171871		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A				

Element	(%wt)	Ladle	Product	EPCRA	CAS#	Element	(%wt)	Ladle	Product	EPCRA	CAS#
C	Carbon	0.19				Cr	Chromium	0.08			7440-47-3
Mn	Manganese	1.10			7439-96-5	Mo	Molybdenum	0.03			
P	Phosphorous	0.009				V	Vanadium	0.014			
S	Sulphur	0.004				Cb	Columbium	0.000			
Si	Silicon	0.26				C.E.		0.41			
Cu	Copper	0.13			7440-50-8	CuNiCrMoV		0.314			
Ni	Nickel	0.06			7440-02-0	CrMo		0.11			
5361-1 mk# 1D-5											

Mechanical Testing			Other	
Test Lab	AFG		VD	YES
Test Bar Size	3.5X3.5X12		Fully Killed	YES
HBW	149 - 156			
Elg (%)	34			
RA (%)	64			
Tensile Specimen Size (in)	.493			
Tensile (ksi)	78.8			
Yield (ksi)	51.9			
Gauge Length (ln)	2			



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1350027

Certification Date: 11/7/2018

Issued By: Nancy Loos

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b

Material Test Report

Heat Code: BWL

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc 00011756	PO: 0045008	Sales Order: 169271	Line: 3
4800 York Street	Item Code: HBN030150090A001A1	Qty Shipped: 2	
Denver, CO 80216	Item Desc: HBN RF 3"150X9" SA105		
	Mill Heat: A171871		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A			

MARK #1D-5

Product compliant with NACE MR0175/ISO 15156-2:2015, Annex A (A.2.1.2, A2.1.3).

- * No Weld repair performed.
- * Ladle Chemical Analysis results are reported from the raw material suppliers MTR.
- * Tensile taken from a round specimen. Measurement of elongation after fracture.
- * Yield strength was determined using the .2% offset method, unless otherwise specified.
- * All material supplied under this order is certified to be free of mercury contamination and no mercury bearing equipment was used in manufacturing, fabrication or testing.
- * When reported on MTR: Tensile Testing Per ASTM E8; Brinell Hardness Per ASTM E10; Charpy Testing Per ASTM E23
- * AF Global manufactures materials according to a certified Quality Management System conforming to ISO 9001:2015

Unless otherwise noted on PO, Dimensions of all standard pipe flanges and flange fittings (NPS 1/2 to NPS 24) per ASME B16.5-2013, large diameter steel flanges (NPS 26 to 60) per ASME B16.47-2011, Orifice flanges per ASME B16.36-2015.

* FVC FLANGE DIMENSIONS & BOLTING COMPLY - ASME B16.5
SELF-REINFORCING NOZZLES COMPLY WITH SPECIFICATION OF SECTION VIII DIV. 1 OR DIV. 2 PER CUSTOMER DESIGN/FVC DESIGN.



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1350027

Certification Date: 11/7/2018

Issued By: Nancy Loos

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b


Rina Sane - Metallurgical Lab Manager

Page 2 of 2

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mk# 1D-6

CERTIFICATE OF INSPECTION & TEST (EN 10204 3.1)



ST&H CORPORATION

74, Jwadongsunhwan-ro, Haeundae-gu, Busan, Korea

Tel : +82.51.744-4680(5 line) Fax : +82.51.744-4670

E-mail : qm@stnhcorp.com



CE

ISO 9001:2008 / 01

Certificate No. MJH9943-01/08

Date : AUG. 01. 2018

Customer

Contract No. 199005-00

Spec. For Material ASTM A105N-14, ASME SA105N-17, NACE MR0175/ISO 15156-2:2015, NACE MR0103/ISO 17495-1:2016

Heat Treatment 930°C NORMALIZED & A.C

Certified to ISO9001:2008, ISO14001:2004, PED2014/68/EC by LRQA

Dimensional inspection ASME B16.5 - 2017

ITEM / SIZE	Q'ty	Heat No./ Batch No.	Size of Test Specimen		Tension Test				Hardness		Charpy Impact Test (10X10mm Specimen Size)			
			D mm	GL mm	Y.S MPa	T.S MPa	EL %	R.A %	Test (HB)	187	Indiv. 21J	Ave. 27J	Notch V	Temp. -29°C
			12.5	50.0	Max Min	250 485	22.0 30.0				Test Result (J)			Ave.(J)
BA900WRXH3	900LBS WN RF XH 3"	350 012898E	12.5	50.0		345	540	35	75	160 163	120	103	155	126
BA150BR1	150LBS BL RF 1"	500 012898F	12.5	50.0		345	540	35	75	160 163	120	103	155	126
BA150WRXXH3	150LBS WN RF XXH 3"	25 012898F	12.5	50.0		345	540	35	75	160 163	120	103	155	126
BA900WRXH3	900LBS WN RF XH 3"	350 012898F	12.5	50.0		345	540	35	75	160 163	120	103	155	126
BLANK		BLANK				BLANK				BLANK				

Heat No./ Batch No.	Max Min.	Chemical Composition (%)															NDE			
		C	SI	Mn	P	S	NI	Cr	Mo	Cu	V						CE	UT	MT	PT
		0.350	0.350 0.100	1.050 0.600	0.035	0.040	0.400	0.300	0.120	0.400	0.080									
012898E	H	0.170	0.261	1.000	0.015	0.003	0.062	0.083	0.012	0.104	0.002						0.367			
	P	0.174	0.280	1.020	0.020	0.002	0.108	0.131	0.002	0.123	0.001						0.386			
012898F	H	0.170	0.261	1.000	0.015	0.003	0.062	0.083	0.012	0.104	0.002						0.367			
	P	0.174	0.280	1.020	0.020	0.002	0.108	0.131	0.002	0.123	0.001						0.386			
BLANK																				

REMARK

- * H : Heat Analysis P : Product Analysis
- * Impact Test performed according to ASTM A370 & MESC 76/210/2017 Paragraph 8.5 / Table 4 & 5.
- * C:Mn = 1≤5
- * Mn is Permitted up to Max 1.65% (ASTM A105-14 TABLE 1, NOTE 1.)

We hereby certify that the material herein has been made and tested in accordance with the above specification and also with the requirements called for by the above order.

ST-801-14-02

Witnessed by / H. J. LEE

Manager of Q.A Dept / JAY KIM

ST&H CORPORATION



Material Test Report

Heat Code: **DGT**

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 4
4800 York Street		Item Code: LWN020150090A001A1	Qty Shipped: 3	
Denver, CO 80216		Item Desc: LWN RF 2"150X9" SA105		
		Mill Heat: C140139		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A				

Element	(%wt)	Ladle	Product	EPCRA	CAS#	Element	(%wt)	Ladle	Product	EPCRA	CAS#
C	Carbon	0.18				Cr	Chromium	0.05			7440-47-3
Mn	Manganese	1.09		✓	7439-96-5	Mo	Molybdenum	0.02			
P	Phosphorous	0.005				V	Vanadium	0.035			
S	Sulphur	0.002				Cb	Columbium	0.001			
Si	Silicon	0.26				C.E.		0.41			
Cu	Copper	0.18		✓	7440-50-8	CuNiCrMoV		0.485			
Ni	Nickel	0.20		✓	7440-02-0	CrMo		0.07			

S361
mk# 10-7

Mechanical Testing					Other	
Test Lab	AFG				VD	YES
Test Bar Size	SACRIFICIAL PIECE				Fully Killed	YES
HBW	179 - 179					
Elg (%)	28					
RA (%)	65					
Tensile Specimen Size (in)	.490					
Tensile (ksi)	86.6					
Yield (ksi)	56.8					
Gauge Length (in)	2					



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EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical. In addition to the percent by weight of the chemical present in this product, it is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1348577

Certification Date: 10/27/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b

Material Test Report

Heat Code: DGT

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc 00011756	PO: 0045008	Sales Order: 169271	Line: 4
4800 York Street	Item Code: LWN020150090A001A1	Qty Shipped: 3	
Denver, CO 80216	Item Desc: LWN RF 2"150X9" SA105		
	Mill Heat: C140139		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A			

MARK #1D-7

Product compliant with NACE MR0175/ISO 15156-2:2015, Annex A (A.2.1.2, A2.1.3).

- * No Weld repair performed.
- * Ladle Chemical Analysis results are reported from the raw material suppliers MTR.
- * Tensile taken from a round specimen. Measurement of elongation after fracture.
- * Yield strength was determined using the .2% offset method, unless otherwise specified.
- * All material supplied under this order is certified to be free of mercury contamination and no mercury bearing equipment was used in manufacturing, fabrication or testing.
- * When reported on MTR: Tensile Testing Per ASTM E8; Brinell Hardness Per ASTM E10; Charpy Testing Per ASTM E23
- * AF Global manufactures materials according to a certified Quality Management System conforming to ISO 9001:2015

Unless otherwise noted on PO, Dimensions of all standard pipe flanges and flange fittings (NPS 1/2 to NPS 24) per ASME B16.5-2013, large diameter steel flanges (NPS 26 to 60) per ASME B16.47-2011, Orifice flanges per ASME B16.36-2015.

* FVC FLANGE DIMENSIONS & BOLTING COMPLY - ASME B16.5
SELF-REINFORCING NOZZLES COMPLY WITH SPECIFICATION OF SECTION VIII DIV. 1 OR DIV. 2 PER CUSTOMER DESIGN/FVC DESIGN.



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Certification No.: 1348577

Certification Date: 10/27/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 /ISO 10474 3.1.b


Rina Sane - Metallurgical Lab Manager

Page 2 of 2

5361-1
MK# 1D-8



MILL TEST REPORTS

Bonney Forge
14496 Croghan Pike
Mt. Union, PA 17066

CERTIFIED MILL TEST REPORT

Industrial Piping Products 9/26/2018

LOT NO.

1133

CHEMICAL ANALYSIS, PHYSICAL PROPERTIES, REMARKS

2" 6M A105 Coupling Threaded

C	0.160	MN	1.020	P	0.010	S	0.020	SI	0.250
NI	0.060	CR	0.130	MO	0.020	CU	0.180	CO	0.006
V	0.023	AL	0.025	CB	0.000				
CE(LONG FORMULA) = 0.381									
T/S(PSI) 80000 Y/S(PSI) 51800 EL(%) 25.000 RA(%) 43.000									
BRINELL HARDNESS 164, 163									



1. CERTIFYING ASTM A105-14 / **ASME SA105-17 EDITION.**
2. THE MATERIAL SUPPLIED MEETS THE REQUIREMENTS OF NACE MR0175/ISO 15156-2.
3. THE MATERIAL SUPPLIED WAS INSPECTED AND MANUFACTURED IN ACCORDANCE WITH EN DIN 10204:2004 EDITION TYPE 3.1 INSPECTION DOCUMENT.
4. THE ELONGATION TEST RESULTS ARE OBTAINED USING STANDARD ROUND SPECIMEN, 2 INCH OR 50 MM GAGE LENGTH.

THIS DOCUMENT HAS BEEN ELECTRONICALLY SUBMITTED.

Cancel Logout

5361-1
MK# 1D-9

Reviewed to 2017 ASME Code Edition



UNITED STATES STEEL

TUBULAR PRODUCTS
CERTIFIED TEST REPORT
(IN ACCORDANCE WITH ISO 10474/EN10204/DIN50049 "type 3.1")

DATE: 03/23/11
TIME: 05:19:12
SERIAL NO: L0035412

BILL ORDER ITEM NO DR00098 01		SHIPPER'S NO. R83708		P.O. NUMBER 109454-00		VEHICLE ID LT8120																																																																																																
SOLD TO ADDRESS				MAIL TO ADDRESS																																																																																																		
				VENUE USS TUBULAR PRODUCTS 2199 EAST 28TH ST. LORAIN, OH 44055																																																																																																		
SPECIFICATION AND GRADE																																																																																																						
PRESSURE PIPE CARBON <u>SELS HP</u> ASTM A333-10 GRADE 1 ASTM A333-10 GRADE 6 ASME SA333-2010 EDITION GRADE 1 ASME SA333-2010 EDITION GRADE 6 ASTM A106-08 GRADE B ASME SA106-2010 EDITION GRADE B OD/ID WMPI SEA FOR TRANSLONG FLAWS PER APISL B.3.3.1 AND E.6.1.2 BLK REG MILL COAT PE BEV 30 DEG MEETING ALL THE APPLICABLE REQUIREMENTS OF NACE STANDARD MR-01-75 *:2003/COR.1:2005 AND MR0103-2007																																																																																																						
MATERIAL COND: FULL BODY NORMALIZED				OD: 24.000 (609.600)		WALL: 0.500 (12.700)																																																																																																
PRODUCT IDENTIFICATION	TENSILE TEST TYPE/ ORIENTATION	TEST COND.	GUAGE WIDTH IN	YIELD PSI MIN: 35000 MAX:	EXT% .50	TENSILE PSI MIN: 60000 MAX:	Y/T MAX:																																																																																															
MA2116 S500NA MA2116 S500NA	STRIP/L/B STRIP/L/B	NM NM	1.500 1.500	55500 54500	.50 .50	78000 77500	0.71 0.70																																																																																															
** END OF DATA THIS SHEET **																																																																																																						
LEGEND: L - LONGITUDINAL U - UPSET T - TRANSVERSE NM - NORMALIZED QT - QUENCH & TEMPERED SR - STRESS RELIEVED AR - AIR ROLLED TR - THERMO MECHANICAL ROLLED B - BODY W - WELD <table border="1"> <thead> <tr> <th>PRODUCT IDENTIFICATION</th> <th>TYPE</th> <th>C</th> <th>MN</th> <th>P</th> <th>S</th> <th>SI</th> <th>CU</th> <th>NI</th> <th>CR</th> <th>MO</th> <th>AL</th> <th>N</th> <th>V</th> <th>B</th> <th>TI</th> <th>CB</th> <th>CG</th> <th>CE*</th> </tr> </thead> <tbody> <tr> <td>MA2116</td> <td>HEAT</td> <td>20</td> <td>1.02</td> <td>0.10</td> <td>0.03</td> <td>21</td> <td>0.09</td> <td>0.05</td> <td>10</td> <td>0.02</td> <td>0.28</td> <td>0.03</td> <td>0.000</td> <td>0.002</td> <td>0.002</td> <td></td> <td></td> <td>.41</td> </tr> <tr> <td>MA2116 S500NA</td> <td>PROD</td> <td>20</td> <td>1.09</td> <td>0.14</td> <td>0.06</td> <td>25</td> <td>0.12</td> <td>0.05</td> <td>10</td> <td>0.03</td> <td>0.42</td> <td>0.04</td> <td>0.007</td> <td>0.004</td> <td>0.011</td> <td></td> <td></td> <td>.43</td> </tr> <tr> <td>MA2116 S500NA</td> <td>PROD</td> <td>20</td> <td>1.09</td> <td>0.13</td> <td>0.05</td> <td>25</td> <td>0.12</td> <td>0.05</td> <td>10</td> <td>0.03</td> <td>0.39</td> <td>0.04</td> <td>0.006</td> <td>0.004</td> <td>0.010</td> <td></td> <td></td> <td>.42</td> </tr> <tr> <td colspan="19">** END OF DATA THIS SHEET **</td> </tr> </tbody> </table>								PRODUCT IDENTIFICATION	TYPE	C	MN	P	S	SI	CU	NI	CR	MO	AL	N	V	B	TI	CB	CG	CE*	MA2116	HEAT	20	1.02	0.10	0.03	21	0.09	0.05	10	0.02	0.28	0.03	0.000	0.002	0.002			.41	MA2116 S500NA	PROD	20	1.09	0.14	0.06	25	0.12	0.05	10	0.03	0.42	0.04	0.007	0.004	0.011			.43	MA2116 S500NA	PROD	20	1.09	0.13	0.05	25	0.12	0.05	10	0.03	0.39	0.04	0.006	0.004	0.010			.42	** END OF DATA THIS SHEET **																		
PRODUCT IDENTIFICATION	TYPE	C	MN	P	S	SI	CU	NI	CR	MO	AL	N	V	B	TI	CB	CG	CE*																																																																																				
MA2116	HEAT	20	1.02	0.10	0.03	21	0.09	0.05	10	0.02	0.28	0.03	0.000	0.002	0.002			.41																																																																																				
MA2116 S500NA	PROD	20	1.09	0.14	0.06	25	0.12	0.05	10	0.03	0.42	0.04	0.007	0.004	0.011			.43																																																																																				
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** END OF DATA THIS SHEET **																																																																																																						
*C.E. IS BASED ON THE FOLLOWING EQUATION(S): $CE = C + (MN/5) + (CR+MO+V)/5 + (NI+CU)/15$																																																																																																						



DECIMAL POSITIONS FOR ELEMENTS ARE INDICATED BY THE LEFT MARGIN, VERTICAL DOTTED LINE OR DECIMAL POINT.



UNITED STATES STEEL

TUBULAR PRODUCTS

CERTIFIED TEST REPORT

(IN ACCORDANCE WITH ISO 10474/EN10204/DIN52049 "type 3.1")

DATE: 03/23/11

TIME: 05:19:12

SERIAL NO: L0035412

MILL ORDER/ITEM NO DR00098 01		SHIPPER'S A.D. R83708		P.O. NUMBER 109454-00		0020776											
MATERIAL COND: FULL BODY NORMALIZED				OD: 24.000 (609.600)		WALL: 0.500 (12.700)											
PRODUCT IDENTIFICATION MA2116 S500NA	FLAT	BEND	GRAN SIZE	MIN COLLAPSE	CHARITY V-NOTCH IMPACT TESTING												
					FT-LBS				% SHEAR								
					1	2	3	AVG	1	2	3	AVG					
					DEG F												
** END OF DATA THIS SHEET **					L	B	- 50	FULL	MIN	75	68	71	71	20	20	20	20

LEGEND L - LONGITUDINAL T - TRANSVERSE B - BODY W - WELD HAZ - HEAT AFFECTED ZONE

TEST / INSPECTION		YES	RESULTS / COMMENTS	
FULL LENGTH VISUAL		X		
FULL LENGTH EMI		X	OD X	ODID L X LT 10.0% NOTCH
FULL LENGTH MPI				
FULL LENGTH UT		X	ID X	ODID L X LT 10.0% NOTCH
END AREA INSPECTION (PLAIN END)			MPI	UT
SPECIAL END AREA (SEA) INSP			MPI	UT
FULL LENGTH DRIFT			DRIFT MANDREL SIZE:	

ADDITIONAL NOTES/COMMENTS

MELTED AND MANUFACTURED IN THE USA. NO REPAIRS BY WELDING. NO MERCURY OR MERCURY COMPOUNDS ARE ADDED TO THE STEEL AND ALL MERCURY BEARING EQUIPMENT IS PROTECTED BY A DOUBLE BOUNDARY OF CONTAINMENT.



THIS IS TO CERTIFY THAT THE PRODUCT DESCRIBED HEREIN WAS MANUFACTURED, SAMPLED, TESTED AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION AND FULFILLS THE REQUIREMENTS IN SUCH RESPECTS.

PREPARED BY THE OFFICE OF: R. HARRIS - MANAGER, Q.A.

DATE 03/23/11



S361-1
MK# 1D-10
Reviewed to 2017 ASME Section II

TUBE TEST REPORT

Form QA-003 12/02/09 - Rev 2
Page 1 of 1

ORDER: 040998 004 HEAT: 478063 P.O.: M31010394 PART NO.

SPECIFICATION(S): ASME ASTM SA53/A53-10 GR B SA106/A106-11 GR B
API PSL1 GR B/X42 FORTY FOURTH EDITION
CERTIFIED NACE MR-01-75 DATED 10/15/09

GRADE: 1023M SIZE: 3.500 X 0.600 DRL WPF: 18.60 QUALITY: SEAMLESS HOT FINISH

CONDITION (SPECIAL): FINE GRAIN MELT PRACTICE
TEST METHODS USED: ASTM E415

TEST RESULTS CONFORM TO THE STANDARDS AND SPECIFICATION LISTED ABOVE.

C	Mn	S	P	Si	VC	Ni	Mo	Cu	Al	V	Co	Ti	B
.21	.65	.002	.008	.29	.14	.10	.04	.23	.013	.005	.001	.0020	.0003
.21	.63	.003	.009	.28	.16	.09	.04	.19	.010	.003	.002	.0020	.0001
.21	.65	.003	.009	.30	.15	.09	.04	.19	.013	.003	.002	.0020	.0003

MATERIAL 100% MELTED AND MANUFACTURED IN THE USA.

Specimen	Yield	Tensile	ELNG	R/A	C.E.	Rockwell	Hydrotest
ASTM E8	EUL	KSI	KSI	2"		ASTM E18 Avg	
.750" STR	0.5	49.3	77.4	40.0	.38	77.7 79.2 79.6 78.8 RB	3000 PSI 5 Sec Hold

EN 10204 TYPE 3.1b DATED 01/2005
FLAT(S) - SATISFACTORY
EMI INSPECTION - SATISFACTORY



8/31/12

DATE

Laurie Burette

QUALITY ASSURANCE/KOPPEL

MATERIAL WAS NOT EXPOSED TO MERCURY DURING PROCESSING.
NO WELDING OR WELD REPAIR PERFORMED ON THIS MATERIAL.
MATERIAL IS FREE OF HARMFUL RADIATION.

THIS CERTIFICATION MAY NOT BE REPRODUCED EXCEPT IN FULL.

IPSCO KOPPEL WORKS
P.O. BOX 750
BEAVER FALLS, PA 15010

IPSCO AMBRIDGE WORKS
P.O. BOX 410
AMBRIDGE, PA 15003

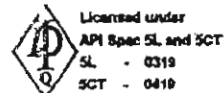
IPSCO BAYTOWN WORKS
2800 SPUR 55
BAYTOWN, TX 77523

5361-1 Reviewed to ASME code Edition 2017
mk# 1D-11

✓ ArcelorMittal South Africa Limited
Tubular Products
273 Genl. Hertzog Rd,
Peacehaven Vereeniging 1939
P O Box 48 Vereeniging 1930
South Africa

MATERIAL TEST CERTIFICATE SEAMLESS TUBE

Telephone +27 (0)16 450 4220
Fax +27 (0)16 423 4906



ISO 9001: 2008

DE-38 5987 QM

Test Certificate
EN 10204:2004 TYPE 3.1

ArcelorMittal

Customer: Order No: 4000023418
Certificate Reference No: 040062154010
Product: FULLY KILLED HOT FINISHED CARBON STEEL SEAMLESS TUBES
Specification: ISO3183-2012/API 5L-2012 L245/L290/B/X42 PSL1 ASTM A53B.12 A106B/C.15 A190.12 ASME SA53B.15 SA106B/C.15 SA53B.15
Product Marking: ARCELORMITTAL SA ISO3183/Spec 5L-0319 MONOGRAM 05-17 ASTM/ASME A/SA106B/C A53B 3.500 0.300 40.000 L245/B L290/X42 PSL1 SMLS TESTED 3000
per CAST NO: 1609658 PROD/O NO: T0442341810 MADE IN SOUTH AFRICA NDE

Customer Order/Contract No: SUS4 155556
Material No: 1000042255
Cast/Heat No: 1609658

Page 1 of 1

General Information

Quantity	Mass	Dimensions			Total Length
		Tube OD	Thickness	Length	
126	51,758.673(lb)	3.500(*)	0.300(*)	40.000 (ft)	5,040.000(ft)

Steel making process	Final Rolling Operation
Basic Oxygen Furnace	As Rolled
	Final hot rolling finished above 1580°F and cooled in still air

Chemical Composition

Element(%)	C	Si	Mn	S	P	Cr	Ni	Mo	Cu	V	Al	Ti	Sn	Cs	N	B	Nb	CE	R22	R24				
Minimum	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Maximum	0.200	-	1.30	0.030	0.030	0.50	0.50	0.150	0.500	-	-	-	-	-	-	-	-	0.41	0.15	0.060				
Heat	0.120	0.16	1.05	0.004	0.013	0.03	0.01	0.001	0.005	0.043	0.030	0.002	0.001	0.0017	0.0026	0.0004	0.0005	0.31	0.05	0.043				
Product	0.1204	0.1620	1.0460	0.0039	0.0128	0.0280	0.0140	0.0010	0.0050	0.0429	0.0300	0.0018	0.0007	0.0017	0.0026	0.0004	0.0005	0.3104	0.0452	0.0434				
Product (ADD)	0.1204	0.1620	1.0460	0.0039	0.0128	0.0280	0.0140	0.0010	0.0050	0.0429	0.0300	0.0018	0.0007	0.0017	0.0026	0.0004	0.0005	0.3104	0.0452	0.0434				

Mechanical Properties

Specification	UTS (Rm)		Yield (0.5%)		% EL 2 inch
	MPa	psi	MPa	psi	
Minimum		70000		42000	30.0
Maximum		-		-	-
(1) Actual		70343		51343	36.0
(2) Actual		70778		51923	39.0
(3) Actual					
(4) Actual					

	UTS (Rm)		Yield (0.5%)		% EL 2 inch
	MPa	psi	MPa	psi	
(5) Actual					
(6) Actual					
(7) Actual					
Orientation & type of tensile test	Longitudinal, Strip				
Width of tensile piece (inch)	0.75 inch				
Orientation of impact test piece					

OTHER TESTS

Category	Result
Hydrostatic	3000 psi for 5 Sec
NDI: EMI	PASS - ASTM E570 - 12.5% NOTCH
NDI: UT	UT not required
HV 22 lbs	150 153 153

Remarks:

Material in accordance with NACE MR0175:2015/ISO15156-2:2015, MR0103:2015. Dimensions to ASME B36.10M-2015.
The material conform to the hot yield strength requirements as per ASME, Sect II, Pt D, Table Y-1, 2015. All the material conform to the visual and dimensional requirements and is made to a suitable fine grain practice.

Quality Assurance Manager: PJ Venter

Date of Release: 2017.05.26

Certified by:

We hereby certify that the material was manufactured, tested and inspected to and fully comply with the requirements of referenced specifications. No changes, amendments or additions may be made to this document. Any changes which are effected shall invalidate this certificate.



3" X 0.300" SMLS A53/API5L/A106
GR B/X-42 PEB DRL

Heat: 1609658
Your PO: 140733

12/10/2018 11:11:00 AM

12/12/2018 FROM: AMERICAN ALLOY STEEL, INC. S.O.#: 619274
P.O.#: 4700687702
Item: 1 (1 PC) 1/2" X 120" X 120"

TO: RYERSON PROCUREMENT CORPORATION
AA FL#: 5210607

NUCOR
PLATE MILL

P.O. Box 279
Winton, NC 27886
(252) 356-3700

Mill Test Report Page 3

1505 River Rd
Cofield, NC 27822
(252) 356-3700

AMERICAN ALLOY
PLATE # 5210607
NUCOR
It's Our Nature.

Issuing Date: 09/20/2018 B/L No.: 514118 Load No.: 522348 Our Order No.: 1592467 Cust. Order No.: 116319-UT
Vehicle No: NOKL 725178 Sold To: AMERICAN ALLOY STEEL INC 6230 N HOUSTON ROSSLYN RD PO BOX 40469 NORTH HOUSTON, TX 77091 Ship To: AMERICAN ALLOY STEEL INC 1124 W 600 NORTH UP-HRSVL-UCRY TRACK 725 STATION UN005 CODEN, UT 84404
Specification: 0.5000" x 120.000" x 480.000" ASTM A516 70/MS60-17/ASME SA516-70/MS60 PVD 2015/2017 Normalized Plate NACE MR0175 Annex 2.1.2 (2015), MR0103 (2010) Section 2.1.2 Compliant (2015) 13.1.1, 13.1.2 Vacuum Degassed

Marking: 116319-UT

Heat No	C	Mn	P	S	Si	Cu	NI	Cr	Mo	Al (tot)	V	Nb	Ti	N	Ca	B	Sn	Cuq	Pom
8605498	0.19	1.02	0.007	0.000	0.18	0.15	0.08	0.08	0.01	0.020	0.004	0.002	0.002	0.0060	0.0042	0.0009	0.008	0.40	0.26

Plate Serial No	Pieces	Tons	Dir.	Tensile Test				Heat Treat			
				Yield (psi)	Tensile (psi)	Elong. % in 2"	Elong. % in 8"	Norm (°F)	Time (min)	Temper (°F)	Time (min)
8605498-02	3	12.25	H-T	49,400	73,300	45.6		1850	23		

Plate Serial No	Pieces	Tons	Dir.	Absorbed Energy (Ft-lbs)				Lateral Expansion (in.)				Shear (%)				Min	Temp (°F)	Slits
				(ft-lbs) 1	(ft-lbs) 2	(ft-lbs) 3	Ave	(in.) 1	(in.) 2	(in.) 3	Ave	(%) 1	(%) 2	(%) 3	Ave			
8605498-02	3	12.25	H-L	119.4	144.0	132.7	132.0	15								-50	10mm	

HOT ROLLED CARBON STEEL PLATE
TEST COUPONS TAKEN FROM HEAT TREATED PLATE
Plate frequency Charpy

Manufactured to fully killed fine grain practice by Electric Arc Furnace. Welding or weld repair was not performed on this material. Mercury has not been used in the direct manufacturing of this material. Produced as continuous cast discrete plate, unless otherwise noted in Specification. For Mexico shipments to Inho-Sales@Nucor.com
Yield by 0.5EUL method unless otherwise specified. Ceq = C+(Mn/6)+(Cr+Mo+V)/5+((Cu+Ni)/15)
Pcm = C+(S/30)+(Mn/20)+(Cu/20)+(Ni/60)+(Cr/20)+(Mo/15)+(V/10)+58
Melted and manufactured in the USA, ISO 9001:2008 certified (#010940) by SRU Quality System Registrar (#0986-00), PED 87723/EC 712 Annex 1, Paris. 4.3 Compliant.
DIN 50049 3.1.8/EN 10204 3.1B(2004), DIN EN 10204 3.1(2005) compliant. For ABS grades only, Quality Assurance certificate 14-MMPQA-723

We hereby certify that the contents of this report are accurate and correct. All test results and expansions performed by the material manufacturer are in compliance with the applicable specifications, including customer specifications.

T. A. Depreux
T. A. Depreux, Metallurgical

9/27/2018 9:23:19 AM



mk# 1D-12, 1D-16, 1D-17, 1E-2
5361
1H-2
ID# 300
PO# 45335

Certified a true copy of the original, retained in our file.
AMERICAN ALLOY STEEL, INC.
Reviewed By:
JK 10/24/2018

1/2 x 120 x 120

Mill Test Report

Page 2

Issuing Date : 10/07/2018 B/L No. : 514849 Load No. : 525223 Our Order No. : 159439/1 Cust. Order No. : 4500893647
Vehicle No: ATW 53005 Sold To: RYERSON PROCUREMENT CORP Ship To: RYERSON INC. DENVER
Specification: 1.0000" x 96.000" x 240.000" PO BOX 91601 6600 HIGHWAY 85
ASTM A516 70-17/ASME SA516 70 SA516-485 PVQ 2015/2017 NACE LUBBOCK, TX 79490 COMMERCE CITY, CO 80022
MR0175 Annex 2.1.2 (2015), MR0103 (2010) Section 2.1.2(2015) 13.1.1, 13.1.2) Compliant
Marking: 160005134

Heat No	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al(toI)	V	Nb	Ti	N	Ca	B	Sn	Ceq	Pcm
8505555	0.20	1.05	0.008	0.000	0.20	0.24	0.10	0.07	0.01	0.039	0.004	0.002	0.002		0.0020	0.0001	0.011	0.41	0.28

Plate Serial No	Pieces	Tons	Tensile Test			
			Dir.	(psi) Yield	(psi) Tensile	Elong. % in 2"
8505555-07	4	13.06	T	45,600	75,500	20.2

5361-1
PL ID # 28 U
mk # 15-14, 1D-13



Manufactured to fully killed fine grain practice by Electric Arc Furnace. Welding or weld repair was not performed on this material. Mercury has not been used in the direct manufacturing of this material. Produced as continuous cast discrete plate as -rolled, unless otherwise noted in Specification. For Mexico shipments: mhc-SalesMX@Nucor.com
Yield by 0.5EUL method unless otherwise specified. $Ceq = C + (Mn/6) + ((Cr + Mo + V)/5) + ((Cu + Ni)/15)$
 $Pcm = C + (Si/30) + (Mn/20) + (Cu/20) + (Ni/60) + (Cr/20) + (Mo/15) + (V/10) + 5B$
Melted and Manufactured in the USA. ISO 9001:2008 certified (#010940) by SRI Quality System Registrar (#0985-09). PED 97/23/EC 7/2 Annex 1, Para. 4.3 Compliant.
DIN 50049 3.1.B/EN 10204 3.1B(2004), DIN EN 10204 3.1(2005) compliant. For ABS grades only, Quality Assurance certificate 14-MMPQA-723

We hereby certify that the contents of this report are accurate and correct. All test results and operations performed by the material manufacturer are in compliance with the applicable specifications, including customer specifications.

T. A. Depretis
T. A. Depretis, Metallurgist

10/7/2018 2:00:14 PM

SSAB

Test Certificate

Form TC1; Revision 3; Date 7 Feb 2018

1770 Bill Sharp Boulevard, Metairie, LA 70001-9412, US

Customer: JOSEPH T. RYERSON & SON, INC. ACCOUNTS PAYABLE DEPT. PO BOX 91601 LABROCK TX 79490-1601		Customer P.O. No.: 4500999993		Mill Order No.: 41-549855-01		Shipping Manifest: MT359173										
Product Description: ASTM A516-70(17)/ASME SA516-70(17)				Ship Date: 12 Oct 18 Cert Date: 12 Oct 18		Cert No: 061736667 (Page 1 of 1)										
Size: 0.750 X 95.00 X 240.0 (IN)																
Tested Pieces			Tensiles			Charpy Impact Tests										
Heat Id	Piece Id	Tested Thickness	Tst Loc (KSI)	YS (KSI)	UTS (KSI)	%KA	Elong %	Tst Dir	Hardness	Abs. Energy (FT-LB)	% Shear	Tst Temp	Tst Dir	Tst Slz (mm)	IMPWT	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
AB1210	C09	0.748 (DISCRT)	55	76	35	T										
Chemical Analysis																
Heat Id	C	Mn	P	S	Si	Tot Al	Sol Al	Cu	Ni	Cr	Mo	Co	V	Ti	B	Nb
AB1210	.17	.99	.010	.002	.17	.028	.026	.28	.11	.08	.02	.001	.030	.002	.0003	.38
KILLED STEEL. MERCURY IS NOT A METALLURGICAL COMPONENT OF THE STEEL AND NO MERCURY WAS INTENTIONALLY ADDED DURING THE MANUFACTURE OF THIS PRODUCT. KILLED STEEL, PRODUCED TO A FINE GRAIN PRACTICE CEV (ITW) = C + Mn/8 + (Cr+Mo+V)/5 + (Ni+Cu)/15 NTR BN 10204.2004 INSPECTION CERTIFICATE 3.1 COMPLIANT 100% MELTED AND MANUFACTURED IN THE USA. NO WELD REPAIR HAS BEEN PERFORMED ON THIS MATERIAL. PRODUCTS SHIPPED: AB1210 C09 PCRR: 2, LBS: 9002																
mk# 1C-19 1D-14 P045335 ID 39U 5361																
8378 SPD QUALITY EATON METAL PRODUCTS COMPANY LLC																
Cust Part #: 160004840								WE HEREBY CERTIFY THAT THIS MATERIAL WAS TESTED IN ACCORDANCE WITH, AND MEETS THE REQUIREMENTS OF, THE APPROPRIATE SPECIFICATION Brian Wales SENIOR METALLURGICAL PRODUCT								

6" 150# A105 RF Blind Flange

Heat : H5912

53512

536(-1)
MK# 1D-18

Reviewed to ASME Section II

R.N. GUPTA & COMPANY LTD., C-55, FOCAL POINT, LUDHIANA -141 010 (INDIA)

RNG

MATERIAL / MILL TEST CERTIFICATE EN 10204 : 2004 - 3.1

NAME OF BUYER
MOUNTAIN WEST
PIPE AND SUPPLY
U.S.A.



CERTIFICATE NO. 11447 DATE 30/08/2017

RAW MATERIAL SPECIFICATION :

SPECIFICATION FOR INSPECTION :

P.O NO. 68434 DT. 14/04/2017

INVOICE NO. RNG/EXP/17-2143 DT. 26/08/2017

MECHANICAL REQUIREMENTS

Sr. No.	Description	Qty (PCS)	Heat No.	Supp. Code	Y.S(Psi) Min 36,000	T.S(Psi) Min 70,000	E% Min 22%	RA% Min 30%	Heat Treatment	Soaking Time (Min.)	Hardness BHN 137-187
33	3/4" 300# BLRF FLGS	50	H 5842	6	49486	79962	32.94	67.16	AS FORGED		160 - 162
34	1 1/2" 150# BLRF FLGS	100	H 5899	6	52525	76814	34.60	64.02	AS FORGED		156 - 158
35	6 1/2" 150# BLRF FLG	77	H 5956	19	51093	81122	34.46	66.48	AS FORGED		152 - 154
36	6 1/2" 150# BLRF FLG	3	H 5912	20	46865	74586	33.20	64.77	AS FORGED		144 - 146
37	3 1/2" 150# BLRF	120	H 5913	20	50056	80353	32.20	65.00	AS FORGED		152 - 154
38	1 1/2" 150# SORF FLGS	100	H 5932	6	48162	79678	31.84	63.52	AS FORGED		148 - 150
39	2 1/2" 150# SORF FLGS	166	H 5915	20	50607	75801	33.14	64.29	AS FORGED		148 - 150
40	2 1/2" 150# SORF FLGS	84	H 5914	20	49683	79640	32.00	65.35	AS FORGED		150 - 152

CHEMICAL REQUIREMENTS

Sr. No.	Heat No.	SPECIFIED ELEMENTS						UNSPECIFIED ELEMENTS				
		C.E. 0.47% Max	C 0.35 Max	Mn 0.60-1.25	P 0.035 Max	S 0.04 Max	Si 0.10 -0.35	Cu 0.40 Max	Ni 0.40 Max	Cr 0.30 Max	Mo 0.12 Max	V 0.05 Max
33	H 5842	0.38	0.21	1.00	0.021	0.011	0.22	0.005	0.008	0.006	0.003	0.003
34	H 5899	0.40	0.21	1.10	0.020	0.013	0.23	0.006	0.014	0.007	0.007	0.003
35	H 5956	0.41	0.20	1.23	0.025	0.019	0.21	0.003	0.010	0.015	0.003	0.002
36	H 5912	0.40	0.20	0.92	0.031	0.018	0.25	0.120	0.070	0.150	0.033	0.004
37	H 5913	0.41	0.21	0.93	0.029	0.016	0.22	0.170	0.057	0.120	0.019	0.004
38	H 5932	0.36	0.20	0.90	0.016	0.009	0.24	0.021	0.014	0.033	0.003	0.003
39	H 5915	0.39	0.19	0.92	0.030	0.016	0.20	0.150	0.065	0.130	0.024	0.004
40	H 5914	0.41	0.20	0.95	0.031	0.015	0.25	0.120	0.071	0.170	0.044	0.005

Material in accordance with NACE MR0175-2003 and NACE MR0103

All Products were manufactured, Sampled, Tested and Inspected Solely by the manufacturer shown on this Test Report in accordance with indicated specification and were found to meet the requirements.

No Weld Repair was performed and all products are free of Weld Repair. All Products are free of Mercury Contamination and Radioactivity.

Note: We hereby confirm that our QA system comply with the requirements of Annex I, section 4.3 of PED 2014/68/EU and it is certified by DNV BUSINESS ASSURANCE vide Certificate No. 4487-2014-CE-IND-DNV GL valid upto 31-03-2020, ISO 9001:2015 Certificate No. is 39752-2008-AQ-IND-RvA Valid upto 22/07/2020. Products also conform to requirements of ASTM A105-05/ASME SA105

ALL NORMALISED MATERIALS ARE HEAT TREATED AT TEMP. 920 DEGREE CENTIGRADE.

For R.N. GUPTA & COMPANY LTD. Page No : 5

METALLURGIST



51480

boltex
mfg. co.

Material Test Reports

Heat Code: **T217**

MOUNTAIN WEST PIPE AND SUPPLY

ITEM						
Ln#	Qty	Description	Mat Spec	Ht Cd	Mill Heat Number	CE
001	1	3" 150 RF BLIND	SA105-18	T217	CM3671639	0.4042

CHEMICAL PROPERTIES																
Ht Cd	C	Si	Mn	P	S	Cr	Al	Cu	Ni	Mo	V	Nb	Sn	N	B	Pb
T217	0.1900	0.2200	1.0500	0.0120	0.0170	0.0700	0.0010	0.2600	0.0700	0.0150	0.0010	0.0010	0.0080	0.0000	0.0001	0.0000
	0.1900	0.2200	1.0500	0.0120	0.0170	0.0700	0.0010	0.2600	0.0700	0.0150	0.0010	0.0010	0.0080	0.0000	0.0001	0.0000

PHYSICAL PROPERTIES										
Ht Cd	Tensl	Yield	%Elong	%RA	HBW	Charpy	FT-Lbs	Lat Expan	%-Shear	Test Temp
T217	80800	48900	36.00	64.85	159/163					

NOTES	
Ht Cd	Note

New Heat Code

All products bearing the "BOLTTEX" name or logo "B" with the heat number prefix listed on the legend below have been manufactured at our Houston, TX facilities from steel melted and forged in the U.S.A. All other products have been manufactured at our Houston, TX facilities from steel melted where indicated.

AR = Arkansas Steel (USA)
NU = Nucor Steel (USA)
WR = Warren Steel (USA)

CM or SI = Commercial Metals Corp. (USA)
RE = Republic Steel (USA)
AB = ABS (Italy)

GER = Gerdau Steel (USA)
TI = Timken Steel (USA)

We certify our flanges are capable of passing a hydrostatic test compatible with their rating and all test results and process information contained herein are correct and true as contained in company records. All flanges meet NACE MRO-175 and/or MRO-100 Latest Revision.

Our quality system has been registered by DNV-GL to ISO 9001, Certificate No.: 142240-2013-AQ-RVA. Test results comply with: EN 10204-3.1. Our flanges satisfy the material requirements for PED 97/23/EC Annex 1-4.3.

Notwithstanding the absence of a signature, the organization submitting either a printed certificate or an EDI transmitted certificate is responsible for content of the report. (ASTM/A 981-04a Section 19.4)

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5361-1
mk# 1D-19



52104



NORTH AMERICAN
STAINLESS

METALLURGICAL TEST REPORT

6870 Highway 42 East
Ghent, KY 41045-9615
(502) 347-6000

Certificate: 464901 01 Mail To:
Customer: 0075 809 RYERSON, INC.
6600 HIGHWAY 85
COMMERCE CITY, CO 80022

Ship To:
RYERSON, INC.
6600 HIGHWAY 85
COMMERCE CITY, CO 80022

Date: 11/29/2018 Page: 1

Steel: 304/304L

Finish: HRAP

Your Order: 4500900845

NAS Order: AN 0822184 01

Corrosion: ASTM A262/15 A 180Bend-OK

PRODUCT DESCRIPTION:

STAINLESS STEEL PLATE, HRAP; UNS 30400/30403
ASTM A240/17, A480/16b, A666/15, ASME SA240/17, SA480/17, SA666/17
CHEM ONLY ON FOLLOWING ASTM: A276/17, A479/17, A484/16, A312/16
CHEM ONLY ON FOLLOWING ASME: SA312/13, SA479/13
AMS 5511H/5513J XMRK; MIL-S-5059D AMD3 (X CRN MEAS); MIL-S-4043B
NACE MR0175/ISO 15156-3:2009 A, MR0103/07; QQS766D-A X MAG PERM
MIN. SOLUTION ANNEAL TEMP 1900F, WATER QUENCHED

REMARKS:

Mat'l is Free of Mercury Contamination. No weld repairs.
EN 10204:2004 3.1; RoHS 1 & 2 Compliant
Material is Free of Radioactive Contamination
Steel Making Process: EAF, AOD, & Cont. Casting
Product Mfg. by a Quality Mgt. Sys. in Conf. w/ISO 9001
*Melted & Manufactured in the USA; Mat'l is DFARS Compliant
*Melted & Manufactured in the USA; Mat'l is DFARS Compliant

Product ID #	Coil #	Thickness	Width	Weight	-----Length-----	Mark	Pieces	COMMODITY CODE NO.
04A19W HC	* 04A19W HC	.5000	60.0000	1,050	PLATE	120.00	11	1 161001129

ANAB, ISO/IEC 17025, Certificate# L2323

CHEMICAL ANALYSIS CM(Country of Melt) ES(Spain) US(United States) ZA(South Africa) JP(Japan)

Chemical Analysis per ASTM A751/14a

HEAT	CM	C %	CR %	CU %	MN %	MO %	N %	NI %	P %	S %
A19W	US	.0198	18.0380	.3980	1.8105	.3280	.0708	8.0105	.0320	.0010
		SI %								
		.2780								

MECHANICAL PROPERTIES

Product ID #	Coil #	1 d o i c r	UTS KSI	20C .2% YS KSI	20C ELONG %-2"	% Hard RB	R of A %
04A19W HC	04A19W HC	F T	87.33	34.59	68.20	80.00	73.25



NAS hereby certifies that the analysis on this certification is correct. Based upon the results and the accuracy of the test methods used, the material meets the specifications stated. These results relate only to the items tested and this report cannot be reproduced, except in its entirety, without the written approval of NAS.

Technical
Dept. Mgr.

KRIS LARK

11/29/2018

outokumpu
high performance stainless steel



PO # 0045289
JOB # 5361-501
HEAT # 441917
MARK # 16.2, 16.3, 16.4

* CERTIFICATION *

Page: 1

10/27/14
HEAT 441917

ORDER 0029146/026

B00023907

SHIP TO:
SOUTHWEST STAINLESS HOUSTON
8505 Monroe
800-231-8268
Houston

TX 77061

----- YOUR ORDER & DATE -----
333678 10/27/14 CUST# SOUSTA02

----- ITEM DESCRIPTION -----
24" SCH80S TP304/TP304L A312

Country of Melt : SWE
Country of Mfg. : USA

----- SPECIFICATIONS -----
ASTM A312-13B/ASME SA312-13
QUALITY SYSTEM CERTIFIED TO:
PED 97/23/EC ANNEX 1, § 4.3
BY TUV SUD INDUSTRIE SERVICE
GMBH, NOTIFIED BODY 0036
TOLERANCE: ASTM A999
LONGITUDINAL WELDED
RANDOM LENGTHS
PLAIN ENDS
DESCALED, PICKLED, AND
PASSIVATED: ASTM A380
Certificate in conformance with EN10204-95 3.1.B / EN10204-2004 3.1
WELDED
MECHANICAL TESTING: ASTM A370
YIELD STRENGTH: 0.2% OFFSET
COLD FINISHED
ELECTRIC FUSION WELDED (EFW)
IM EINVERNEHMEN MIT DEM TUV
SUD INDUSTRIE SERVICE GMBH
WIRD AUF EINE GEGENZEICHNUNG
LAUT SCHREIBEN VOM 05.AUGUST
2008 DURCH TUV SUD INDUSTRIE
SERVICE GMBH VERZICHTET

----- MECHANICAL & OTHER TESTS -----
Tensile strength, KSI (MPa) 85.2 (587)
Yield strength, KSI (MPa) 46.8 (323)
Elongation % in 2 55.0
Guided Bend Face OK
Bend Test
Hydrotest PSI (MPa) 700 (4.83)
NACE MR0175/ISO 15156:09
NACE MR0103-12

----- CHEMICAL COMPOSITION -----
Carbon (C) 0.020
Phosphorus (P) 0.036
Silicon (Si) 0.320
Nickel (Ni) 8.130
Manganese (Mn) 1.550
Sulphur (S) 0.001
Chromium (Cr) 18.330
Nitrogen (N) 0.068

-- Continued --



Reviewed to 2017 ASME Section II

Martha James
Martha James

Outokumpu Stainless Pipe, Inc.

ADDRESS
241 W Clarke Street
Wildwood, Florida 34765-9801

TELEPHONE
(352) 748-1313

TELEFAX
Administration: (352) 748-2751
Purchasing: (352) 748-6576
Production Control: (352) 748-6533
Quality Assurance: (352) 748-6533



COASTAL FLANGE

P.O. BOX 40443
HOUSTON, TX 77240-0443

MATERIAL CERTIFICATION

74561001 MTR #: 857

Page : 1 of 1

SOLD TO:

SHIP TO:

DATE	SALES ORDER #	CUST P.O.#	TAG NUMBER	SPECIFICATION
04/08/2016	160414	S630278		SA105
ITEM #	QTY	ITEM DESCRIPTION	HEAT CODE	
7		36" 150# RF WN XH "B" ASME B16.47	ACDXJ	

CHEMICAL ANALYSIS										
C	Mn	P	S	SI	Cr	Ni	Mo	V	Cu	
.20	.94	.006	.004	.29	.025	.021	.005	.001	.012	

PHYSICAL PROPERTIES						HEAT TREATMENT	
Tensile PSI	Yield PSI	Elongation	REDUCTION OF AREA %	BHN	BHN		
75565	47427	33	60	149	147		



SUPPLEMENTAL INFORMATION

I hereby certify that the reported figures are correct, as contained in the records of the corporation and that the material was manufactured in the United States of America under a ISO:9001:2008 certified Quality Management System. NACE MRO175 EN 10204 3.1

S361-1

MK# 1D-1, 1H-1

Reviewed to ASME 2017 Section II

Production Assistant



Commercial Metal Forming - O
341 West Collins Ave
Orange, CA 92867
PHONE: 714.532.6321
FAX:

PACKING LIST

SHIPMENT NO. 300227
PAGE NO. 3

SALES ORDER	CUSTOMER NO.	P.O. NUMBER	P.O. DATE	S.O. DATE	PLANT
999119	17913	0044997	09/21/18	09/21/18	OCW

SOLD TO: EATON METAL PRODUCTS*
4800 YORK ST.
DENVER, CO 80216

SHIP DATE: 11/16/18

PREPAID&ALLOW-FOB DE

B/L NO. 259767

SHIP TO: EATON METAL PRODUCTS
844 S. CHESTNUT STREET
SALT LAKE CITY, UT 84104
USA

MTR'S WITH SHIPMENT

ITEM	PART NO.	DESCRIPTION	REL REQ DATE	DUE QTY	SHIP QTY
1	4939400121	36"OD X .50"NOM SE 2:1 SA516-70 2"Sf OSB 30 DEG .06"LAND SA516-70 N MTRS 240# (.375"MIN) 1H-3 HEAT: KGH=85005299 SLAB: 08	1 11/05/18	1	1

5361
mk # 1H-3

CARBON STEEL PARTS WHICH WERE COLD
FORMED COMPLY WITH ASME SECTION VIII
DIV. 1 UG-79 & UCS-79D.
PARTS: WERE NOT HEAT TREATED
 WERE HEAT TREATED
ALL PARTS COMPLY WITH UG-81
CERTIFIED BY:



SA516-11U

112

8505299

NUCOR
PLATE MILL

P.O. Box 279
Winton, NC 27986
(252) 356-3700

Mill Test Report Page 1

1505 River Rd
Coffield, NC 27922
(252) 356-3700

NUCOR
It's Our Nature

Issuing Date : 08/15/2018 B/L No. : 509940 Load No. : 520530 Our Order No. : 159120/5 Cust. Order No. : 7331578
Vehicle No: TTPX 804814 Sold To: SAMUEL SON AND CO INC 6415 E CORVETTE ST LOS ANGELES, CA 90040 Ship To: SAMUEL C/O TRISTAR FLC 9600 KAISER WAY BNSF SPUR #2142 FONTANA, CA 92336
Specification: ✓ 0.6000" x 96.000" x 480.000" ASTM A516 70-17/ASME SA516 70 PVQ 2015/2017 Normalized Test Coupons at 1650 F NACE MR0175 Annex 2.1.2 (2015), MR0103 (2010) Section 2.1.2(2015) 13.1.1, 13.1.2
Marking : 1344087

Heat No	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al(tot)	V	Nb	Ti	N	Ca	B	Sn	Ceq	Pcm
---------	---	----	---	---	----	----	----	----	----	---------	---	----	----	---	----	---	----	-----	-----

✓ 8505299	0.19	1.04	0.009	0.001	0.19	0.26	0.09	0.10	0.01	0.030	0.004	0.002	0.003		0.0027	0.0003	0.011	0.41	0.27
-----------	------	------	-------	-------	------	------	------	------	------	-------	-------	-------	-------	--	--------	--------	-------	------	------

Plate Serial No	Pieces	Tons	Dir.	Tensile Test			
				(psi) Yield	(psi) Tensile	Elong. % in 2"	Elong. % in 8"

✓ 8505299-05	6	19.60	T	60,400	77,200	23.8	
KGF			T	51,800	72,200	26.6	N
✓ 8505299-06	6	19.60	T	53,500	77,500	24.0	
KGG			T	51,500	72,900	25.1	N
✓ 8505299-08		13.06	T	52,600	77,100	23.6	
KGH			T	51,200	72,600	27.1	N
✓ 8505299-09	4	13.06	T	52,600	77,300	23.0	
KGI			T	50,600	72,300	26.4	N

5361-1
mk# 14-3



APPROVED
ASME SEC. II
2017 Ed. _____ Ad.
CMF

Test coupons only, normalized 60 minutes per inch of thickness at 1650 F ± 25 F. Hold 30 minutes minimum. ;

Manufactured to fully killed fine grain practice by Electric Arc Furnace. Welding or weld repair was not performed on this material. Mercury has not been used in the direct manufacturing of this material. Produced as continuous cast discrete plate as-rolled, unless otherwise noted in Specification. For Mexico shipments: nhc-SalesMX@Nucor.com
Yield by 0.5EUL method unless otherwise specified. Ceq = C+(Mn/8)+((Cr+Mo+V)/5)+((Cu+Ni)/16)
Pcm = C+(Si/30)+(Mn/20)+(Cu/20)+(Ni/60)+(Cr/20)+(Mo/15)+(V/10)+5B
Melted and Manufactured in the USA. ISO 9001:2008 certified (#010940) by SRI Quality System Registrar (#0965-09). PED 97/23/EC 7/2 Annex 1, Para. 4.3 Compliant.
DIN 50049 3.1.B/EN 10204 3.1B(2004), DIN EN 10204 3.1(2006) compliant. For ABS grades only, Quality Assurance certificate 14-MMPQA-723

We hereby certify that the contents of this report are accurate and correct. All test results and operations performed by the material manufacturer are in compliance with the applicable specifications, including customer specifications.

T. A. Depretis

T. A. Depretis, Metallurgist

8/15/2018 10:10:45 AM

R068850 08/16/18 K

5361-1
MK#1H-4



R.N. GUPTA & COMPANY LTD., C-55, FOCAL POINT, LUDHIANA -141 010 (INDIA)

MATERIAL / MILL TEST CERTIFICATE EN 10204 : 2004 - 3.1

F-MTR-01-01



CERTIFICATE NO. 12560 DATE 27/03/2018

NAME OF BUYER

RAW MATERIAL SPECIFICATION : ASTM A105-14/ASME SA105-13

SPECIFICATION FOR INSPECTION : ANSI/ASME B16.5-2013

P.O NO. 68906 DT. 17/10/2017

INVOICE NO. EXP/17-2448 DT. 23/03/2018

MECHANICAL REQUIREMENTS

Sr. No.	Description	Qty (PCS)	Heat No.	Supp. Code	Y.S (PSI) Min 36,000	Y.S (PSI) Min 70,000	E% Min 22%	RA% Min 30%	Heat Treatment	Soaking Time (Min.)	Hardness BHN 137-187
1	4 160# WNRF XH FLGS	134	H 6336	20	49006	78514	33.40	66.94	AS FORGED		152 - 154
2	4 150# WNRF XH FLGS	1460	H 6342	20	48755	78585	33.70	69.37	AS FORGED		152 - 154
3	4 160# WNRF XH FLGS	1081	H 6343	20	49887	78793	33.70	67.09	AS FORGED		152 - 154

CHEMICAL REQUIREMENTS

Sr. No.	Heat No.	SPECIFIED ELEMENTS					UNSPECIFIED ELEMENTS					
		C.E. 0.47% Max	C 0.35 Max	Mn 0.60-1.25	P 0.035 Max	S 0.04 Max	Si 0.10 -0.35	Cu 0.40 Max	Ni 0.40 Max	Cr 0.30 Max	Mo 0.12 Max	V 0.05 Max
1	H 6336	0.38	0.20	0.89	0.029	0.020	0.24	0.130	0.045	0.092	0.021	0.004
2	H 6342	0.40	0.22	0.93	0.032	0.022	0.24	0.073	0.034	0.075	0.007	0.002
3	H 6343	0.40	0.22	0.93	0.031	0.021	0.23	0.078	0.030	0.077	0.008	0.003



Material in accordance with NACE MRO 175-2015/ISO-15168 and NACE MRO 103-2016

All Products were manufactured, Sampled, Tested and Inspected Satisfactorily by the manufacturer shown on this Test Report in accordance with indicated specification and were found to meet the requirements.

No Weld Repair was performed and all products are free of Weld Repair. All Products are free of Mercury Contamination and Radioactivity.

Note: We hereby confirm that our QA system complies with the requirements of Annex L Section 4.3 of PED 2014/68/EU and it is certified by DNV BUSINESS ASSURANCE vide Certificate No. A437-2014-CE-IND-DNV GL valid upto 31-03-2020, ISO 9001:2015 Certificate No. 1 is 39753-2008-AQ-IND-RvA Valid upto 22/07/2020. Products also conform to requirements of ASTM A105/ASME SA105

For R.N. GUPTA & COMPANY LTD. Page No : 1

METALLURGIST

FVC

an **AFGlobal** Company**Material Test Report**Heat Code: **C1000AF**

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

Sales: (713) 393-4200

ISO 9001:2015 Certified

Eaton Metal Produc	00011756	PO: 0045008	Sales Order: 169271	Line: 5
4800 York Street		Item Code: LWN030150090A001A1	Qty Shipped: 5	
Denver, CO 80216		Item Desc: LWN RF 3"150X9" SA105		
		Mill Heat: A141747		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A				

Element	(%wt)	Ladle	Product	EPCRA	CAS#	Element	(%wt)	Ladle	Product	EPCRA	CAS#
C Carbon	0.18					Cr Chromium	0.10				7440-47-3
Mn Manganese	1.10			✓	7439-96-5	Mo Molybdenum	0.02				
Mn:C	6.1					V Vanadium	0.022				
P Phosphorous	0.007					Cb Columbium	0.000				
S Sulphur	0.005					C.E.	0.40				
Si Silicon	0.24					CuNiCrMoV	0.352				
Cu Copper	0.16			✓	7440-50-8	CrMo	0.120				
Ni Nickel	0.05			✓	7440-02-0						

5361
mk# 1H-5

Mechanical Testing						Other					
Test Lab	AFG					EF	Y				
HBW	156 - 156										
Elg (%)	33										
RA (%)	65										
Tensile Specimen Size (in)	.492										
Tensile (ksi)	77.4										
Yield (ksi)	88.6										
Gauge Length (in)	2										



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1986) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1347385

Certification Date: 10/17/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b

Page 1 of 2

Material Test Report

Heat Code: C1000AF

Forged Vessel Connections

An AFGlobal Company

13770 Industrial Rd. Houston, TX 77015

ISO 9001:2015 Certified

Sales: (713) 393-4200

Eaton Metal Produc 00011756	PO: 0045008	Sales Order: 169271	Line: 5
4800 York Street	Item Code: LWN030150090A001A1	Qty Shipped: 5	
Denver, CO 80216	Item Desc: LWN RF 3"150X9" SA105		
	Mill Heat: A141747		
Spec: ASTM A105/A105M-(18)/ASME SA 105/SA 105M-(17) Section II Part A			

MARK # 1H-5

Product compliant with NACE MR0175/ISO 15156-2:2015, Annex A (A.2.1.2, A2.1.3).

- * No Weld repair performed.
- * Ladle Chemical Analysis results are reported from the raw material suppliers MTR.
- * Tensile taken from a round specimen. Measurement of elongation after fracture.
- * Yield strength was determined using the .2% offset method, unless otherwise specified.
- * All material supplied under this order is certified to be free of mercury contamination and no mercury bearing equipment was used in manufacturing, fabrication or testing.
- * When reported on MTR: Tensile Testing Per ASTM E8; Brinell Hardness Per ASTM E10; Charpy Testing Per ASTM E23
- * AF Global manufactures materials according to a certified Quality Management System conforming to ISO 9001:2015

Unless otherwise noted on PO, Dimensions of all standard pipe flanges and flange fittings (NPS 1/2 to NPS 24) per ASME B16.5-2013, large diameter steel flanges (NPS 26 to 60) per ASME B16.47-2011, Orifice flanges per ASME B16.36-2015.

* FVC FLANGE DIMENSIONS & BOLTING COMPLY - ASME B16.5
SELF-REINFORCING NOZZLES COMPLY WITH SPECIFICATION OF SECTION VIII DIV. 1 OR DIV. 2 PER CUSTOMER DESIGN/FVC DESIGN.



The recording of false, fictitious, or fraudulent statement or entries on this document may be punishable as a felony under federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III) of the Superfund Amendments and Reauthorization Act of 1980 and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Services (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1347385

Certification Date: 10/17/2018

Issued By: John Saucedo

This report is issued in compliance with the requirements of EN10204 3.1 / ISO 10474 3.1.b


Rina Sane - Metallurgical Lab Manager

Page 2 of 2

53617
mk# 1H-7, 1H-6
Reviewed to 2017 ASME Section II

SeAH CSS

SeAH Changwon Integrated Special Steel

147 Jeokhyeon-ro, Seongsan, Changwon, Gyeongnam, Korea

INSPECTION-CERTIFICATE

CUSTOMER :

SUPPLIER : POSCO Processing & Service Co., Ltd

PURCHASE ORDER NO. : 5349

REF. CD: 5349

CERT. NO. : 150430-3043

MANUFACTURE NO. : KPOUJ558A5450

STEEL GRADE : TP304/304L		SPECIFICATION : ASTM A312		MELTING PROCESS : E.A.F.	
SIZE : OD 4 NPS X WT SCH80S X 18 - 20 FT		EDITION/ADDENDA : 11 EDITION / NO ADDENDA		V.O.D.	
ARTICLE : SEAMLESS AUSTENITIC STAINLESS STEEL PIPES		STATE OF DELIVERY : SOLUTION TREATMENT		STRAND CASTING	
		HOT FINISHED, FLAIN END			

Heat No.	Chemical Composition(wt.%)										Non-Metallic Inclusion Test	
	C	SI	MN	P	S	NI	CR					
Spec. MIN.						8.000	18.000					
MAX.	.035	1.000	2.000	.0450	.0300	11.000	20.000					
N08288 L	.013	.270	1.712	.0330	.0067	8.207	18.245					
N08288 P	.014	.264	1.745	.0329	.0073	8.298	18.219					

Test No. (Lot No.)	Tensile Properties				Hardness	Impact Test	Decarburized	Grain	Additional Tests
	Y.S.(KSI)	T.S. (KSI)	EL. (%)	Body HRB		Depth (mm)	Size No.		
	0.2%					TOTAL	FERR.		Flattening test: GOOD Hydrostatic test: GOOD (2300PSI)
Spec. MIN.	30.0	75.0	35.0						
MAX.				90					
5001-1	36.0	85.0	55.0	78					
5001-2	36.0	85.0	54.0	78					

Lot No.	Bundle No.	Length (ft)	Number of Qr.	Total Length (F)	Weight Kg	Case No.	Additional Tests / Remarks
5P04625001	5P046250011	18 - 20	5	98.5	686	F40359	Corrosion Test: GOOD
TOTAL							5

CERTIFY TO ASTM A312-99/ASME SA312-98ED.(00ADD.)TP304/304L, ASTM A376-98/ASME SA376-98ED.(00ADD.)TP304, UNS S30400/S30403
HEAT TREATMENT: 1050 °C FOR 5MIN.(WATER QUENCHED)
HARDNESS ACCORDING TO: NACE MR-0175(02ED.), CORROSION TEST: ACC. TO MIL-P-24691/3
INSPECTION CERTIFICATE DIN 50049 3.1/EN 10204 3.1/ISO 10474 3.1B
EN 10204 Type 3.1 / NO REPAIR WELDING. FREE FROM MERCURY CONTAMINATION.

Our quality system is certified in accordance with ISO 9001: 2008 by ONV.

We here certify, that the material described above has been tested and complies with the terms of the order contract.

J. K. Lee
Team Manager, Quality Assurance Team
DATE : MAY. 01, 2015



5361-1 Reviewed to 2017 ASME Section II
mk# 1C-1, 1J-1

NORMA (INDIA) LIMITED				Works Test Certificate			
48, Site IV Industrial Area, Sahibabad, Ghaziabad-201010 (U.P) INDIA. Tel: 91-120-2896091, 2895404 Fax: 91-120-2895930 E-mail: norma.india@gmail.com							
NORMA/LAB NO-6539/14-15		INVOICE NO. E-400		DATE:-13-10-14			
P. Order. No:	503/005034	Customer:-		Forging specification		ASME SA105 -09 ASTM A105 -12	
Component	20"-150# WNRF XH FLG.			Steel Supplier		Adhunik Metaliks Ltd.	
Drawing No.		Quantity:-		09Nos.		Mill Heat No. 14AJ 145	
Machining STD	ANSI B16.5- 2009 ASME B16.5- 2009						
TEST RESULTS				NORMA HEAT NO-1231			
CHEMICAL COMPOSITION				MECHANICAL PROPERTIES.			
Elements %	Specified Composition	Actual		PROPERTIES	SPECIFIED	OBTAINED	Specified carbon as per Purchase Order 0.25max. Serrated face as per MSS-SP-6 With in limits of 125-250AARH CARBON EQUIVALENT (CE) $CE = C + \frac{Mn}{6} + \frac{Cr}{5} + \frac{Mo}{15} + \frac{Ni}{15} + \frac{Cu}{15}$ MARKING AS PER MSS-SP-25-2008 20"-150 XH SA/A105 1231 B16.5 NORMA INDIA.
		NORMA LAB	MILL T.C.				
Carbon	0.35max.	0.20	0.20	Yield Strength (mpa)	250.00 min.	321.65	
Manganese	0.60-1.05	1.11	1.10	Tensile Strength (mpa)	485.00 min.	521.86	
Silicon	0.10-0.35	0.18	0.20				
Sulphur	0.040max.	0.012	0.015	%Elongation in 50mm / 4D	22.00 min	31.76	
Phosphorous	0.035max.	0.016	0.015	Hardness HB.	187. max.	149-163	
Chromium	0.30max.	0.012	0.014	% Reduction of Area	30.00 min.	61.01	
Nickel	0.40max.	0.009	0.007	Remarks:- We here by certify that the material described here in has been tested in accordance with the applicable specifications referred above and meets the requirements as per EN10204/3.1B & NACE Standard-MR0175-2003. "As per ASTM A105 Table 1 Note:-For each reduction of 0.01% below the specified carbon maximum(0.35%)an increase of 0.06% manganese above the specified maximum (1.05%)will be permitted up to maximum 1.35% & NACE Standard MRO175/ISO15156 Standard Country of Origin-India.			
Copper	0.40max.	0.012	0.009				
Molybdenum	0.12max.	0.004	0.001				
Vanadium	0.080max.	0.004	0.002	Checked by:			Metallurgist
Carbon Equivalent (CE)	0.47max.	0.390	0.387	Certified by:			
							Quality Control Manager



ST&H CORPORATION

NUCOR
PLATE MILL

P.O. Box 279
Winton, NC 27988
(252) 368-3700

Mill Test Report

Page 1

1606 River Rd
Coffield, NC 27922
(252) 368-3700

NUCOR
It's Our Nature

Issuing Date : 09/12/2018 B/L No. : 512940 Load No. : 623425 Our Order No. : 189438/1 Cust. Order No. : 4500893649
Vehicle No: NDKL 725000 Sold To: RYERSON PROCUREMENT CORP Ship To: RYERSON INC. DENVER
Specification: 1.2500" x 96.000" x 240.000" P.O. BOX 91001 5600 HIGHWAY 85
ASTM A36-14/ASTM A709 Grade 35-18/AAASHTO M270 Grade 36/ASME LUBBOCK, TX 79490 COMMERCE CITY, CO 80022
SA36 2015/2017 AASHTO M270-2017 36

Marking : 160005004

Heat No	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al (tot)	V	Nb	Ti	N	Ca	B	Sn	Co	Pcm
8505747	0.20	0.84	0.010	0.001	0.19	0.19	0.08	0.10	0.01	0.025	0.033	0.002	0.011%		0.0042	0.0009	0.011	0.38	0.20
Plate Serial No	Pieces	Tons	Tensile Test																
			Dir.	(psi) Yield	(psi) Tensile	Elong. % in 2"													
8505747-04	3	12.25	T	40,900	69,700	27.2													
			T	41,000	70,100	20.7													



Manufactured to fully killed line grain practice by Electric Arc Furnace. Welding or weld repair was not performed on this material. Mercury has not been used in the direct manufacturing of this material. Produced as continuous cast discrete plate as rolled, unless otherwise noted in Specification. For Mexico shipments, nhc-Sales@Nucor.com
Yield by 0.5EUL method unless otherwise specified. $C_{eq} = C + (Mn/5) + ((Cr+Mo+V)/5) + ((Cu+Ni)/15)$
 $P_{cm} = C + (Si/30) + (Mn/20) + (Cu/20) + (Ni/60) + (Cr/20) + (Mo/15) + (V/10) + B$
Mild and Manufactured in the USA. ISO 9001:2008 certified (R010940) by SRI Quality System Registrar (R0885-09). PED 97/23/UEC 7/2 Annex 1, Para. 4.3 Compliant.
DIN 60040 3.1, DIN EN 10204 3.1D(2004), DIN EN 10204 3.1(2005) compliant. For ABS grades only. Quality Assurance certificate 14-KAMPQA-723

We hereby certify that the contents of this report are accurate and correct. All test results and operations performed by the material manufacturer are in compliance with the applicable specifications, including customer specifications.

T. A. Deputis
T. A. Deputis, Metallurgist

09/12/2018 8:48:15 AM

5361-1
PL ID # 270
mk # 1C-4,5,6
1S-4,5,6

NUCOR
NUCOR CORPORATION
NUCOR STEEL UTAH

Mill Certification
10/11/2016

MTR #: U1-357740
 PO Box 100
 7285 West 21200 North
 PLYMOUTH, UT 84330
 (435) 458-2300
 Fax: (435) 458-2309

Sold To: INTSEL STEEL WEST LLC
 PO BOX 21119
 HOUSTON, TX 77226-1119

Ship To: INTSEL STEEL WEST
 1887 SOUTH 700 WEST
 SALT LAKE CITY, UT 84104
 (801) 433-2210
 Fax: (801) 972-6145

Customer P.O.	SLC-12130	Sales Order	268246.4
Product Group	Merchant Bar Quality	Part Number	3000075024004W0
Grade	A36/A529GR50/CSA44W/50W	Lot #	PL1610567651
Size	3/4" (.7500) Round	Heat #	PL16105676
Product	3/4" (.7500) Round 20'A36/A529-50/44W/50W	B.L. Number	U1-548929
Description	A36/A529-50/44W/50W	Load Number	U1-357740
Customer Spec		Customer Part #	

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Roll Date: 8/13/2016 Melt Date: 8/10/2016 Qty Shipped LBS: 11,895 Qty Shipped Pcs: 396

ASTM A36/A36M-12, A709/709M-13 GR36, ASME SA36-10 Ed '11 Ad.
 ASME SA36-2010 EDITION-2011 ADDENDA
 ASTM A709/A709M-13 GR36 [250]

C	Mn	P	S	Si	Cu	Ni	Cr	Mo	V	Cb
0.19%	0.72%	0.010%	0.045%	0.24%	0.23%	0.09%	0.13%	0.018%	0.0016%	0.000%

Yield 1: 51,498psi

Tensile 1: 73,816psi

Elongation: 28% in 8"(% in 203.3mm)

Yield 2: 50,764psi

Tensile 2: 73,645psi

Elongation 26% in 8"(% in 203.3mm)

Weight Variation 000.0%

Specification Comments: MEETS THE REQUIREMENTS OF: ASTM A36/A36M-12, A529/A529-05 GR50, CSA G40.21-04 GR44W(300W)&GR50W(350W) AASHTO M270/M270M-12 GR36(270), ASME SA36/SA36M-07

Comments: NUCOR - PLYMOUTH IS AN I.S.O. 9001 AND AN A.B.S. CERTIFIED MILL
 CMTR COMPLIES WITH DIN EN 10204 - 3.1

1. ALL MANUFACTURING PROCESSES OF THE STEEL MATERIALS IN THIS PRODUCT, INCLUDING MELTING, CASTING, AND HOT ROLLING HAVE OCCURRED WITHIN THE UNITED STATES. ALL PRODUCTS PRODUCED ARE WELD FREE. MERCURY, IN ANY FORM, HAS NOT BEEN USED IN THE PRODUCTION OR TESTING OF THIS MATERIAL.
 2. PROPOSITION 65 WARNING: THIS PRODUCT CONTAINS A CHEMICAL KNOWN TO THE STATE OF CALIFORNIA TO CAUSE CANCER AND/OR BIRTH DEFECTS OR OTHER REPRODUCTIVE HARM. FOR MORE INFORMATION, PLEASE CALL 1-435-458-2300.

Reviewed to 2017 ASME Section II

5361-1
 MK# 1C-8, 1J-8



Ryan Pennington

Ryan Pennington
 Division Metallurgist

5361-1
mk# 13-13

Reviewed to 2017 ASME Section II



UNITED STATES STEEL CORPORATION

TUBULAR PRODUCTS
CERTIFIED TEST REPORT

(IN ACCORDANCE WITH ISO 10474/EN10204/DIN50049 "type 3.1")

DATE: 11/30/14
TIME: 04:05:47
SERIAL NO: L0054107

MILL ORDER/ITEM NO DRO0652 08		SHIPPER NO. R03446		P.O. NUMBER 10P15701-CA		VEHICLE ID GONK310910																															
SOLD TO ADDRESS				MAIL TO ADDRESS				VENDOR UNITED STATES STEEL CORP LORAIN TUBULAR OPERATIONS 2199 EAST 28TH ST. LORAIN, OH 44055																													
SPECIFICATION AND GRADE PIPE CARBON SMLS STD PIPE API 5L-45TH EDITION DATED 12/1/12 PSL-2 GRADE B AND GRADE X42 R N OR Q ASTM A53-12 GRADE B ASTM A106-13 GRADE B/C SPECIAL OD TOLERANCE ASME SA53-2013 EDITION GRADE B ASME SA106-2013 EDITION GRADE B/C BLK REG MILL COAT PE BEV 30 DEG MEETING ALL THE APPLICABLE REQUIREMENTS OF NACE STANDARD MR-01-75 *ISO 15156-2 2009 ED AND MR-0103-2012 ED																																					
MATERIAL COND: AS ROLLED				O.D.: 20.000 (508.000)		In (mm)		WALL: 0.500 (12.700)		In (mm)																											
PRODUCT IDENTIFICATION		TENSILE TEST TYPE/ ORIENTATION		TEST COND.		GAUGE WIDTH IN		YIELD PSI MIN: 42100 MAX: 71800		EXT % .50		TENSILE PSI MIN: 70000 MAX: 95000		Y/T 0.33		ELONG % (IN 2") MIN: 29.0 MAX: 39.7		HARDNESS SCALE: MIN: 1900 MAX: 1900		MIN HYDRO PSI 1900		DWELL (SEC) 5															
MA6721 F157AA X83582 E795AA		STRIP/L/B STRIP/L/B		AR AR		1.500 1.500		50500 49700		.50 .50		78500 73000		0.65 0.68		39.7 45.5				1900 1900		5 5															
				**		END OF DATA THIS SHEET																															
LEGEND:		L - LONGITUDINAL U - UPSET		T - TRANSVERSE NM - NORMALIZED		QT - QUENCH & TEMPERED SR - STRESS RELIEVED		AR - AS ROLLED TR - THERMO MECHANICAL ROLLED		S - BODY		W - WELD																									
PRODUCT IDENTIFICATION		TYPE		C		Mn		P		S		Si		Cu		Ni		Cr		Mo		Al		N		V		B		Ti		Cb		Co		C.E.*	
																																		MAX			
MA6721		HEAT		19		1.04		0.10		0.03		0.23		0.16		0.08		0.09		0.02		0.025		0.03		0.0003		0.002		0.003				.41			
MA6721 F157AA		PROD		20		1.04		0.07		0.02		0.24		0.15		0.07		0.08		0.03		0.026		0.03		0.0002		0.001		0.001				.42			
MA6721 F157AA		PROD		20		1.04		0.06		0.03		0.24		0.16		0.07		0.08		0.02		0.027		0.03		0.0002		0.001		0.001				.42			
X83582		HEAT		20		1.04		0.08		0.07		0.23		0.02		0.01		0.09		0.01		0.038		0.03		0.0002		0.002		0.001				.40			
X83582 E795AA		PROD		19		1.05		0.04		0.05		0.25		0.02		0.01		0.08		0.01		0.041		0.03		0.0001		0.002		0.003				.40			
X83582 E795AA		PROD		21		1.05		0.03		0.09		0.25		0.01		0.01		0.08		0.01		0.042		0.03		0.0005		0.002		0.006				.41			
																																		**			

*C.E. IS BASED ON THE FOLLOWING EQUATION(S): $CE = C + Mn/6 + (Cr + Mo + V) / 5 + (Ni + Cu) / 15$

DECIMAL POSITIONS FOR ELEMENTS ARE INDICATED BY THE LEFT MARGIN, VERTICAL DOTTED LINE OR DECIMAL POINT. ELEMENTS REPORTED IN MASS FRACTION (%)





UNITED STATES STEEL CORPORATION

TUBULAR PRODUCTS

DATE: 11/30/14

TIME: 04:05:47

SERIAL NO: L0054107

CERTIFIED TEST REPORT

(IN ACCORDANCE WITH ISO 10474/EN10204/DIN50049 "typ 3.1")

MILL ORDER/ITEM NO DR00652 08		SHIPPERS NO. R03446		P.O. NUMBER 10P15701-CA		0019012											
MATERIAL COND: AS ROLLED				O.D.: 20.000 (508.000)				WALL: 0.500 (12.700)									
PRODUCT IDENTIFICATION	FLAT	BEND	GRAIN SIZE	MIN COLLAPSE	DIR	TEST LOC.	TEMP	SIZE	TEST COND.	CHARPY V-NOTCH IMPACT TESTING FT-LBS				% SHEAR			
										1	2	3	AVG	1	2	3	AVG
MA6721 F157AA X83582 E795AA	OK OK				T	B	+ 32	3/4	HIL	58	77	60	65	40	60	50	50
										100	94	104	99	100	100	100	100
** END OF DATA THIS SHEET **																	
LEGEND L - LONGITUDINAL T - TRANSVERSE B - BODY W - WELD HAZ - HEAT AFFECTED ZONE																	
TESTING / INSPECTION INFORMATION																	
TEST / INSPECTION		YES		RESULTS / COMMENTS													
FULL LENGTH VISUAL		X															
FULL LENGTH EMI		X		OD <u>X</u> OD/ID <u> </u> L <u>X</u> LT <u> </u> 10.0% NOTCH													
FULL LENGTH MPI																	
FULL LENGTH UT		X		ID <u>X</u> OD/ID <u> </u> L <u>X</u> LT <u> </u> 10.0% NOTCH													
END AREA INSPECTION (PLAIN END)		X		MPI <u>X</u> UT <u> </u>													
SPECIAL END AREA (SEA) INSP				MPI <u> </u> UT <u> </u>													
FULL LENGTH DRIFT				DRIFT MANDREL SIZE: <u> </u>													
ADDITIONAL NOTES/COMMENTS																	
MELTED AND MANUFACTURED IN THE USA, NO REPAIRS BY WELDING, NO MERCURY COMPOUNDS ARE ADDED TO THE STEEL AND ALL MERCURY BEARING EQUIPMENT IS PROTECTED BY A DOUBLE BOUNDARY OF CONTAINMENT.. MANUFACTURED IN AN ISO 9001 CERTIFIED FACILITY - CERTIFICATE #32022. PRODUCT WAS HOT ROLLED AND HOT FINISHED																	

THIS IS TO CERTIFY THAT THE PRODUCT DESCRIBED HEREIN WAS MANUFACTURED, SAMPLED, TESTED AND/OR INSPECTED IN ACCORDANCE WITH THE SPECIFICATION AND FULFILLS THE REQUIREMENTS IN SUCH RESPECTS.

PREPARED BY THE OFFICE OF: BRAD KOURY - MANAGER, Q.A.

DATE 11/30/14





UNITED STATES STEEL CORPORATION

TUBULAR PRODUCTS
ADDITIONAL COMMENTS SHEET

DATE: 11/30/14

TIME: 04:05:51

PAGE: 1 OF 1

MILL ORDER/ITEM NO. DR00652 08	SHIPPERS NO.	P.O. NUMBER 10P15701-CA	HEAT	SERIAL NUMBER: L0054107
SOLD TO ADDRESS		MAIL TO ADDRESS		VENDOR UNITED STATES STEEL CORP LORAIN TUBULAR OPERATIONS 2199 EAST 28TH ST. LORAIN, OH 44055
HEAT MA6721 - MELTED AT:NUCOR STEEL MEMPHIS, MEMPHIS, TN 38109 HEAT X83582 - MELTED AT:FAIRFIELD WORKS, FAIRFIELD, AL 35064 END OF DATA				

Mill Test Report

Page 2

Issuing Date : 10/07/2018 B/L No. : 514849 Load No. : 525223 Our Order No. : 159439/1 Cust. Order No. : 4500893647
Vehicle No: ATW 53005 Sold To: RYERSON PROCUREMENT CORP Ship To: RYERSON INC. DENVER
Specification: 1.0000" x 96.000" x 240.000" PO BOX 91601 6600 HIGHWAY 85
ASTM A516 70-17/ASME SA516 70 SA516-485 PVQ 2015/2017 NACE LUBBOCK, TX 79490 COMMERCE CITY, CO 80022
MR0175 Annex 2.1.2 (2015), MR0103 (2010) Section 2.1.2(2015) 13.1.1, 13.1.2) Compliant

Marking : 160005134

Heat No	C	Mn	P	S	Si	Cu	Ni	Cr	Mo	Al(tot)	V	Nb	Ti	N	Ca	B	Sn	Ceq	Pcm
8505555	0.20	1.05	0.008	0.000	0.20	0.24	0.10	0.07	0.01	0.039	0.004	0.002	0.002		0.0020	0.0001	0.011	0.41	0.28
Tensile Test																			
Plate Serial No	Pieces	Tons	Dir.	(psi) Yield	(psi) Tensile	Elong. % in 2"	Elong. % in 8"												
8505555-07	4	13.06	T	46,600	75,500	20.2													

5361-1
PL ID # 280
mk # 15-14, 1D-13



Manufactured to fully killed fine grain practice by Electric Arc Furnace. Welding or weld repair was not performed on this material. Mercury has not been used in the direct manufacturing of this material. Produced as continuous cast discrete plate as -rolled, unless otherwise noted in Specification. For Mexico shipments: nhc-SalesMX@Nucor.com

Yield by 0.5EUL method unless otherwise specified. Ceq = C+(Mn/6)+((Cr+Mo+V)/5)+((Cu+Ni)/15)

Pcm = C+(Si/30)+(Mn/20)+(Cu/20)+(Ni/50)+(Cr/20)+(Mo/15)+(V/10)+5B

Melted and Manufactured in the USA. ISO 9001:2008 certified (#010940) by SRI Quality System Registrar (#0985-09). PED 97/23/EC 7/2 Annex 1, Para. 4.3 Compliant. DIN 50049 3.1.B/EN 10204 3.1B(2004), DIN EN 10204 3.1(2005) compliant. For ABS grades only, Quality Assurance certificate 14-MMIPA-723

We hereby certify that the contents of this report are accurate and correct. All test results and operations performed by the material manufacturer are in compliance with the applicable specifications, including customer specifications.

T. A. Deprelis
T. A. Deprelis, Metallurgist

10/7/2018 2:00:14 PM



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736

NDE Reports

				Salt Lake City, UT Denver, CO Billings, MT Farmington, NM				Client: <u>EATON METAL</u> Job Location: <u>SLC, Utah</u> Job Reference: <u>5361-1</u>				Date: <u>3/22/2019</u> Team W.O.: <u>1116-001390</u> Client P.O.: <u>45650</u>																				
				(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115																												
Customer EATON METAL			Type Of Weld Butt Weld			Radiation Source IR- 192 ☒ CO- 60 ☐ X-Ray ☐			Film Type AGFA D5		Film Size 4.5 X 17		Penetrameter Type ASTM WIRE B																			
Specification Boiler/ Pressure Vessel			Drawing Number			Source Strength or MA/KV 87 CI			Emulsion Number 8250802N		Exp. Date 1/1/21		Penetrameter Material Stainless Steel																			
Procedure RT ASME.1 R24			Pipe O.D./ Pipe Thickness .875"		Plate Thickness		Focal Spot Size (F) 0.124"		Exp. Time 2 MIN. 30 SEC.		Single Load ☒ Double Load ☐		Penetrameter Location Source Side ☒ Film Side ☐																			
Acceptance Criteria RT - ASME Sec. VIII			Joint Type Butt Weld		Material Carbon Steel		Thickness With Reinforcement (d) 1.187"		Film Technique SWE/SWV		Shim Material NA		Thickness NA																			
Exposure Technique B			Surface Condition As Welded			Source To Object (D) 20"			Screen Thickness .010"-.010"		ID Placement Lead on Film																					
Viewing Single ☒ Double ☐			Film Processing Auto ☐ Manual ☒						Screen material Lead		Location Marker Placement Film Side ☒ Source Side ☐																					
ISO Line #						Report #																										
			Accept		Reject		Porosity		Slag		Crack		Incomplete Fusion		Incomplete Penetration		Undercut		Burn Through		Surface Indication		Tungsten Inclusion		Concavity							
Weld No.			View		Weld I.D.																											
GS HD/32U			0-1		LK		X																									
GS 32U/37U			0-1		LK				X																							
GS 37U/35U			0-1		LK		X																									
GS 35U/31U			0-1		LK				X																							



Client: _____ Date: _____ NDE Inspector: Andrew Gruber Date: 3/22/2019

Form MS.RT.ASME

"Client has final authority and responsibility for interpretation and acceptance of examination and reports"

④ Salt Lake City, UT	Denver, CO	Billings, MT	Farmington, NM
(801)397-2202	(720)579-0660	(406)371-5822	(505)598-4115

Client:	EATON METAL
Job Location:	SLC, Utah
Job Reference:	5361

Date: 4/2/2019
Team W.O: 1116-001390
Client P.O: 45650

Customer EATON METAL		Type Of Weld Butt Weld		Radiation Source IR- 192 ☒ CO- 60 ☐ X-Ray ☐		Film Type AGFA D5	Film Size 4.5 X 17	Penelrameter Type ASTM WIRE B	
Specification Boiler/ Pressure Vessel		Drawing Number		Source Strength or MA/KV 78 CI		Emulsion Number 8250602N	Exp. Date 1/1/21	Penelrameter Material Stainless Steel	
Procedure RT.ASME.1 R24		Pipe O.D./ Pipe Thickness .875"	Plate Thickness	Focal Spot Size (F) 0.124"	Exp. Time 32 MIN	Single Load ☒ Double Load ☐	Penelrameter Location Source Side ☒ Film Side ☐		
Acceptance Criteria RT - ASME Sec. VIII		Joint Type Butt Weld	Material Carbon Steel	Thickness With Reinforcement (d) 1.187"		Film Technique SWE/SWV	Shim Material NA	Thickness NA	
Exposure Technique B		Surface Condition As Welded		Source To Object (D) 65"		Screen Thickness .010"-.010"	ID Placement Lead on Film		
Viewing Single ☒ Double ☐		Film Processing Auto ☐ Manual ☒		Screen material Lead		Location Marker Placement Film Side ☒ Source Side ☐			
ISO Line #				Report #					

[illegible]

Client: _____
Form MS-RT-ASME

Client:

Date: _____

NDE Inspector

Andrew Gruber

Dale:

4/2/2019

"Client has final authority and responsibility for interpretation and acceptance of examination and reports"





®	Salt Lake City, UT	Denver, CO	Billings, MT	Farmington, NM
	(801)397-2202	(720)579-0660	(406)371-5822	(505)599-4115

Client:	EATON METAL
Job Location:	SLC, Utah
Job Reference:	5361

Date:	4/11/2019
Team W.O.:	1116-001390
Client P.O.:	45850

<u>Customer</u> EATON METAL	<u>Type Of Weld</u> Butt Weld		<u>Radiation Source</u> IR- 192 ☒ CO- 60 ☐ X-Ray ☐		<u>Film Type</u> AGFA D5	<u>Film Size</u> 4.5 X 17	<u>Penetrant Type</u> ASTM WIRE B
<u>Specification</u> Boiler/ Pressure Vessel	<u>Drawing Number</u>		<u>Source Strength or MA/KV</u> 95 CI		<u>Emulsion Number</u> 8250602N	<u>Exp. Date</u> 1/1/21	<u>Penetrant Material</u> Stainless Steel
<u>Procedure</u> RT.ASME.1 R24	<u>Pipe O.D./ Pipe Thickness</u> .875"	<u>Plate Thickness</u>	<u>Focal Spot Size (F)</u> 0.124"	<u>Exp. Time</u> 26 MIN	Single Load ☒ Double Load ☐		<u>Penetrant Location</u> Source Side ☒ Film Side ☐
<u>Acceptance Criteria</u> RT - ASME Sec. VIII	<u>Joint Type</u> Butt Weld	<u>Material</u> Carbon Steel	<u>Thickness With Reinforcement (d)</u> 1.187"		<u>Film Technique</u> SWE/SWV	<u>Shim Material</u> NA	<u>Thickness</u> NA
<u>Exposure Technique</u> B	<u>Surface Condition</u> As Welded		<u>Source To Object (D)</u> 65"		<u>Screen Thickness</u> .010"-.010"	<u>ID Placement</u> Lead on Film	
<u>Viewing</u> Single ☒ Double ☐	<u>Film Processing</u> Auto ☐ Manual ☒				<u>Screen material</u> Lead	<u>Location Marker Placement</u> Film Side ☒ Source Side ☐	
ISO Line #			Report #				

[illegible]

Form MS.RT.ASME

Client:

Date: _____

NDE Inspector

Andrew Gruber

Date:

4/11/2019

"Client has final authority and responsibility for interpretation and acceptance of examination and reports"



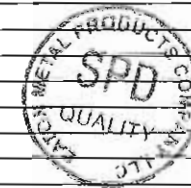
60 Salt Lake City, UT Denver, CO Billings, MT Farmington, NM
(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115

Client: EATON METAL
Job Location: SLC, Utah
Job Reference: 5361-1 Repairs

Date: 3/13/2019
Team W.O.: 1116-001390
Client P.O.: 45650

Customer EATON METAL	Type Of Weld Built Weld	Radiation Source IR- 192 ☒ CO- 60 ☐ X-Ray ☐	Film Type AGFA D5	Film Size 4 5 X 17	Penetrometer Type ASTM WIRE B
Specification Boiler Pressure Vessel	Drawing Number	Source Strength or MA/KV 94 CI	Emulsion Number 8250602N	Exp. Date 1/1/21	Penetrometer Material Stainless Steel
Procedure RT ASME, I R24	Pipe O D / Pipe Thickness .875"	Plate Thickness	Focal Spot Size (F) 0.124"	Exp. Time 2 MIN	Penetrometer Location Source Side ☒ Film Side ☐
Acceptance Criteria RT - ASME Sec VIII	Joint Type Built Weld	Material Carbon Steel	Thickness With Reinforcement (d) 1.187"	Film Technique SWE/SWV	Shim Material NA
Exposure Technique B	Surface Condition As Welded	Source To Object (D) 20"	Screen Thickness 010"- 010"	ID Placement Lead on Film	Location Marker Placement Film Side ☒ Source Side ☐
Viewing Single ☒ Double ☐	Film Processing Auto ☐ Manual ☒		Screen material Lead		

Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrameter Density	Weld Density
LS 34U	0-1	RC	X													2.66	2.24
	8-9	RC		X	X											2.90	2.95
LS 35U	0-1	RC	X			X										2.92	2.69
LS 36U	0-1	RC	X													3.15	3.16
	1-2	RC	X													3.08	3.05
	2-3	RC	X												scuff on film at 3 location	3.18	3.17
	3-4	RC		X				X								3.15	3.16
	4-5	RC	X													2.87	2.89
	5-6	RC	X													2.86	2.84
	6-7	RC	X													2.86	2.88
	7-8	RC	X													3.12	3.11
	8-9	RC	X													3.04	3.07
	9-10	RC	X												scuff om film	3.16	3.20
LS 32U	9-10	RC	X													2.90	2.90
LS 38U	0-1	RC		X	X			X								2.84	2.74
LS 33U	0-1	RC		X	X											2.45	2.94
	1-2	RC		X				X								2.87	2.42
	2-3	RC	X													2.82	2.81
	3-4	RC	X													3.24	3.25
	4-5	RC	X													3.22	3.24
	5-6	RC	X													3.21	3.24
	6-7	RC	X													3.02	2.97
	7-8	RC		X				X								3.02	3.15
	8-9	RC	X			X										3.01	3.12
	9-10	RC	X													2.91	2.01



		Salt Lake City, UT Denver, CO Billings, MT Farmington, NM				Client: EATON METAL		Date: 3/4/2019									
		(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115				Job Location: SLC, Utah Job Reference: 5361-1		Team W.O.: 1116-001390 Client P.O.: 45650									
Customer EATON METAL		Type Of Weld Butt Weld		Radiation Source IR- 192 ☒ CO- 60 ☐ X-Ray ☐		Film Type AGFA D5		Film Size 4.5 X 17		Penetrator Type ASTM WIRE 8							
Specification Boiler/ Pressure Vessel		Drawing Number		Source Strength or MA/KV 102 CI		Emulsion Number 6250602N		Exp. Date 1/1/21		Penetrator Material Stainless Steel							
Procedure RT.ASME 1 R24		Pipe O.D./ Pipe Thickness .875"		Plate Thickness		Focal Spot Size (F) 0.124"		Exp. Time 1 MIN.45 SEC.		Penetrator Location Source Side ☒ Film Side ☐							
Acceptance Criteria RT - ASME Sec. VIII		Joint Type Butt Weld		Material Carbon Steel		Thickness With Reinforcement (d) 1.187"		Film Technique SWE/SWV		Shim Material NA Thickness NA							
Exposure Technique B		Surface Condition As Welded		Source To Object (D) 20"		Screen Thickness .010"-.010"		ID Placement Lead on Film		Location Marker Placement Film Side ☒ Source Side ☐							
Viewing Single ☒ Double ☐		Film Processing Auto ☐ Manual ☒		Report #		Screen material Lead											
ISO Line #																	
Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrator Density	Weld Density
LS 38U	0-1	RC		X				X								2.75	2.77
	1-2	RC	X													2.85	2.80
	2-3	RC	X													2.84	2.85
	3-4	RC	X													2.67	2.69
	4-5	RC	X													2.66	2.68
	5-6	RC	X													2.77	2.85
	6-7	RC	X													3.00	2.99
	7-8	RC	X													2.89	2.78
	8-9	RC	X													2.87	2.84
LS 31U	0-1	RC	X													2.78	2.77
	1-2	RC	X													2.80	2.81
	2-3	RC	X													2.90	2.91
	3-4	RC	X													2.89	2.88
	4-5	RC	X													3.02	3.00
	5-6	RC	X													2.78	2.79
	6-7	RC	X													2.89	2.88
	7-8	RC	X													2.99	3.00
	8-9	RC	X													2.84	2.95
	9-10	RC	X													3.00	3.02
LS 37U	0-1	RC	X													2.87	2.84
	1-2	RC	X													2.78	2.77
	2-3	RC	X													2.80	2.81
	3-4	RC	X													2.90	2.91
	4-5	RC	X													2.89	2.88
	5-6	RC	X													3.02	3.00
	6-7	RC	X													2.78	2.79
	7-8	RC	X													2.89	2.88
	8-9	RC	X													2.99	3.00
	9-10	RC	X													2.84	2.95



				Salt Lake City, UT Denver, CO Billings, MT Farmington, NM				Client: EATON METAL				Date: 3/13/2019					
				(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115				Job Location: SLC, Utah				Team W.O.: 1116-001390					
								Job Reference: 5361-1 Repairs				Client P.O.: 45650					
Customer EATON METAL			Type Of Weld Butt Weld			Radiation Source IR- 192 ☒ CO- 60 ☐ X-Ray ☐			Film Type AGFA D5		Film Size 4.5 X 17		Penetrator Type ASTM WIRE B				
Specification Boiler/ Pressure Vessel			Drawing Number			Source Strength or MA/KV 94 CI			Emulsion Number 8250602N		Exp. Date 1/1/21		Penetrator Material Stainless Steel				
Procedure RT ASME.1 R24			Pipe O.D./ Pipe Thickness .875"			Plate Thickness			Focal Spot Size (F) 0.124"		Exp. Time 2 MIN		Penetrator Location Source Side ☒ Film Side ☐				
Acceptance Criteria RT - ASME Sec. VIII			Joint Type Butt Weld			Material Carbon Steel			Thickness With Reinforcement (d) 1.187"		Film Technique SWE/SWV		Shim Material Thickness NA NA				
Exposure Technique B			Surface Condition As Welded			Source To Object (D) 20"			Screen Thickness .010"-.010"		ID Placement Lead on Film						
Viewing Single ☒ Double ☐			Film Processing Auto ☐ Manual ☒						Screen material Lead		Location Marker Placement Film Side ☒ Source Side ☐						
ISO Line #												Report #					
Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrator Density	Weld Density
LS 34U	0-1	RC	X													2.66	2.24
	8-9	RC		X	X											2.90	2.95
LS 35U	0-1	RC	X			X										2.92	2.69
LS 36U	0-1	RC	X													3.15	3.16
	1-2	RC	X													3.08	3.05
	2-3	RC	X												scuff on film at 3 location	3.18	3.17
	3-4	RC		X				X								3.15	3.16
	4-5	RC	X													2.87	2.89
	5-6	RC	X													2.86	2.84
	6-7	RC	X													2.86	2.88
	7-8	RC	X													3.12	3.11
	8-9	RC	X													3.04	3.07
	9-10	RC	X												scuff on film	3.16	3.20
LS 32U	9-10	RC	X													2.90	2.90
LS 38U	0-1	RC		X	X			X								2.84	2.74
LS 33U	0-1	RC		X	X											2.45	2.94
	1-2	RC		X				X								2.87	2.42
	2-3	RC	X													2.82	2.81
	3-4	RC	X													3.24	3.25
	4-5	RC	X													3.22	3.24
	5-6	RC	X													3.21	3.24
	6-7	RC	X													3.02	2.97
	7-8	RC		X				X								3.02	3.15
	8-9	RC	X													3.01	3.12
	9-10	RC	X													2.91	2.01



(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115

Client: EATON METAL

Date: 3/15/2019

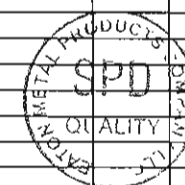
Job Location: SLC, Utah

Team W.O: 1116-001390

Job Reference: 5361-1 Repairs

Client P.O.: 45650

<u>Customer</u> EATON METAL	<u>Type Of Weld</u> Butt Weld		<u>Radiation Source</u> IR- 192 ☒ CO- 60 ☐ X-Ray ☐		<u>Film Type</u> AGFA D5	<u>Film Size</u> 4.5 X 17	<u>Penetrant Type</u> ASTM WIRE B
<u>Specification</u> Boiler/ Pressure Vessel	<u>Drawing Number</u>		<u>Source Strength or MA/KV</u> 94 CI		<u>Emulsion Number</u> 8250602N	<u>Exp. Date</u> 1/1/21	<u>Penetrant Material</u> Stainless Steel
<u>Procedure</u> RT ASME.1 R24	<u>Pipe O.D./ Pipe Thickness</u> .875"	<u>Plate Thickness</u>	<u>Focal Spot Size (F)</u> 0.124"	<u>Exp. Time</u> 2 MIN	<u>Single Load</u> ☒ <u>Double Load</u> ☐		<u>Penetrant Location</u> Source Side ☒ Film Side ☐
<u>Acceptance Criteria</u> RT - ASME Sec. VIII	<u>Joint Type</u> Butt Weld	<u>Material</u> Carbon Steel	<u>Thickness With Reinforcement (d)</u> 1.187"		<u>Film Technique</u> SWE/SWV	<u>Shm Material</u> NA	<u>Thickness</u> NA
<u>Exposure Technique</u> B	<u>Surface Condition</u> As Welded		<u>Source To Object (D)</u> 20"		<u>Screen Thickness</u> .010"- .010"	<u>ID Placement</u> Lead on Film	
<u>Viewing</u> Single ☒ Double ☐	<u>Film Processing</u> Auto ☐ Manual ☒				<u>Screen material</u> Lead	<u>Location Marker Placement</u> Film Side ☒ Source Side ☐	

[illegible]

Client	Date
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NDE Inspector

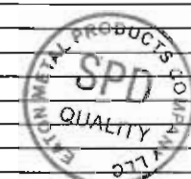
Andrew Gruber

Date: 3/15/2019

Form MS-RT-ASME

"Client has final authority and responsibility for interpretation and acceptance of examination and reports"

TEAM			Salt Lake City, UT Denver, CO Billings, MT Farmington, NM				Client: <u>EATON METAL</u>				Date: <u>3/5/2019</u>						
			(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115				Job Location: <u>SLC, Utah</u>				Team W O: <u>1116-001390</u>						
							Job Reference: <u>5361-1</u>				Client P.O.: <u>45650</u>						
Customer EATON METAL		Type Of Weld Butt Weld		Radiation Source IR-192 ☒ CO-60 ☐ X-Ray ☐		Film Type AGFA D5		Film Size 4 5 X 17		Penetrometer Type ASTM WIRE B							
Specification Boiler/Pressure Vessel		Drawing Number		Source Strength or MA/KV 102 CI		Emulsion Number 8250602N		Exp. Date 1/1/21		Penetrometer Material Stainless Steel							
Procedure RT ASME 1 R24		Pipe O.D. / Pipe Thickness .875"		Plate Thickness		Focal Spot Size (F) 0.124"		Exp. Time 1 MIN 45 SEC		Single Load ☒ Double Load ☐		Penetrometer Location Source Side ☒ Film Side ☐					
Acceptance Criteria RT - ASME Sec. VIII		Joint Type Butt Weld		Material Carbon Steel		Thickness With Reinforcement (d) 1.187"		Film Technique SWE/SWW		Shim Material NA		Thickness NA					
Exposure Technique B		Surface Condition As Welded		Source To Object (D) 20"		Screen Thickness .010"-.010"		Screen material Lead		ID Placement Lead on Film		Location Marker Placement Film Side ☒ Source Side ☐					
Viewing Single ☒ Double ☐		Film Processing Auto ☐ Manual ☒		Report #													
ISO Line #																	
Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrometer Density	Weld Density
LS 33U	0-1	RC		X				X								2.75	2.77
	1-2	RC	X												Scuff mark on film at the 2 location	2.78	2.74
	2-3	RC	X												Scuff mark on film at the 2 location.	2.77	2.77
	3-4	RC		X				X								2.67	2.69
	4-5	RC		X				X								2.66	2.68
	5-6	RC		X				X								2.77	2.85
	6-7	RC		X				X								2.75	2.88
	7-8	RC	X													2.89	2.78
	8-9	RC	X													2.87	2.84
	9-10	RC	X													2.77	2.77
LS 36U	0-1	RC		X				X								2.80	2.81
	1-2	RC		X				X								2.90	2.91
	2-3	RC		X				X								2.89	2.88
	3-4	RC		X				X								3.02	3.00
	4-5	RC		X				X								2.78	2.79
	5-6	RC	X													2.89	2.88
	6-7	RC	X													2.99	3.00
	7-8	RC		X				X								2.84	2.95
	8-9	RC		X				X								3.00	3.02
	9-10	RC	X													2.87	2.84
LS 35U	0-1	RC		X	X											2.78	2.77
	1-2	RC	X													2.66	2.62
	2-3	RC	X													2.90	2.91
	3-4	RC	X													2.50	2.52
	4-5	RC	X													2.55	2.59
	5-6	RC	X													2.60	2.60
	6-7	RC	X													2.89	2.88
	7-8	RC	X													2.78	2.77
	8-9	RC	X													2.75	2.70
	9-10	RC	X														





9 Salt Lake City, UT Denver, CO Billings, MT Farmington, NM
(801)397-2202 (720)579-0660 (406)371-5622 (505)599-4115

Client: EATON METAL
Job Location: SLC, Utah
Job Reference: 5361-1 Repairs

Date: 3/13/2019
Team W.O.: 1116-001390
Client P.O.: 45650

Customer EATON METAL	Type Of Weld Butt Weld	Radiation Source IR- 192 ☒ CO- 60 ☐ X-Ray ☐	Film Type AGFA D5	Film Size 4 5 X 17	Penetrant Type ASTM WIRE 8
Specification Boiler Pressure Vessel	Drawing Number	Source Strength or MA/KV 94 CI	Emulsion Number 8250602N	Exp. Date 1/1/21	Penetrant Material Stainless Steel
Procedure RT ASME 1 R24	Pipe O.D./Pipe Thickness .875"	Plate Thickness	Focal Spot Size (F) 0.124"	Exp. Time 2 MIN	Penetrant Location Source Side ☒ Film Side ☐
Acceptance Criteria RT - ASME Sec. VIII	Joint Type Butt Weld	Material Carbon Steel	Thickness With Reinforcement (d) 1.187"	Film Technique SWE/SWV	Shim Material NA
Exposure Technique 8	Surface Condition As Welded	Source To Object (D) 20"	Screen Thickness .010"-.010"	ID Placement Lead on Film	Location Marker Placement Film Side ☒ Source Side ☐
Viewing Single ☒ Double ☐	Auto ☐ Manual ☒		Lead		

ISO Line #			Report #														Penetrant Density	Weld Density
Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks			
LS 34U	0-1	RC	X													2.66	2.24	
	8-9	RC		X	X											2.90	2.95	
LS 35U	0-1	RC	X			X										2.92	2.69	
LS 36U	0-1	RC	X													3.15	3.16	
	1-2	RC	X													3.08	3.05	
	2-3	RC	X												scuff on film at 3 location	3.18	3.17	
	3-4	RC		X				X								3.15	3.16	
	4-5	RC	X													2.87	2.89	
	5-6	RC	X													2.86	2.84	
	6-7	RC	X													2.86	2.88	
	7-8	RC	X													3.12	3.11	
	8-9	RC	X													3.04	3.07	
	9-10	RC	X												scuff on film	3.16	3.20	
LS 32U	9-10	RC	X													2.90	2.90	
LS 38U	0-1	RC		X	X			X								2.84	2.74	
LS 33U	0-1	RC		X	X											2.45	2.94	
	1-2	RC		X				X								2.87	2.42	
	2-3	RC	X													2.82	2.81	
	3-4	RC	X													3.24	3.25	
	4-5	RC	X													3.22	3.24	
	5-6	RC	X													3.21	3.24	
	6-7	RC	X													3.02	2.97	
	7-8	RC		X				X								3.02	3.15	
	8-9	RC	X			X										3.01	3.12	
	9-10	RC	X													2.91	2.01	



Client: _____ Date: _____ NDE Inspector: Andrew Gruber Date: 3/13/2019
Form MS.RT.ASME

"Client has final authority and responsibility for interpretation and acceptance of examination and reports"

No. B142919

[illegible]

CERTIFIED RADIOGRAPHIC INTERPRETER
1809007N CRI
EXP. 9/01/2021
Jacob Moya
SIGNED: *J. Moya*

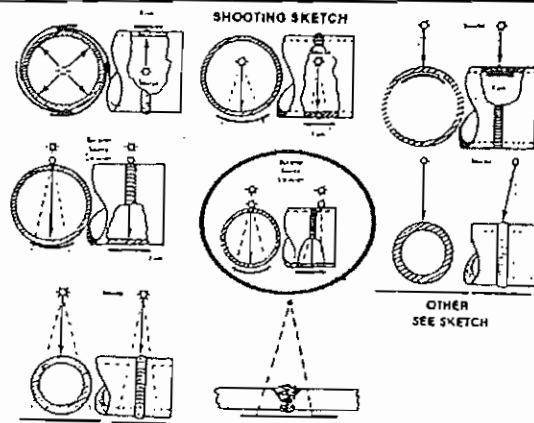
DEFECT CODE		
IP - Incomplete penetration	EI - Elongated Inclusion	RI - Rounded Inclusion
CV - Concavity Root	CX - Convexity Root	DT - Drop Through
IF - Incomplete fusion	UC - Undercut	BT - Burn through
C - Crack	OX - Oxidation	FA - Film Artifact

FILM USED:

1	FILMS	4.5	X	17	TYPE	Agfa d5
	FILMS		X		TYPE	
	FILMS		X		TYPE	

Total hrs.	Total Mileage	Number of Welds
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Brandon Latimer	<i>Bye</i>	11
Radiographer		Level
Cynthia Latimer	<i>Cynthia Latimer</i>	1
Radiographer Ass't		Level
Film delivery		Date



The recorded results are the opinion of the technician to the best of his knowledge based on the information provided to him by the customer at the time of the inspection.

TEAM Salt Lake City, UT Denver, CO Billings, MT Farmington, NM (801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115				Client: <u>EATON METAL</u>				Date: <u>3/5/2019</u>			
				Job Location: <u>SLC, Utah</u>				Team W.O.: <u>1116-001390</u>			
Job Reference: <u>5361-1</u>				Client P.O.: <u>45650</u>							
Customer <u>EATON METAL</u>		Type Of Weld <u>Butt Weld</u>		Radiation Source IR-192 ☒ CO-60 ☐ X-Ray ☐		Film Type <u>AGFA D5</u>		Film Size <u>4.5 X 17</u>		Penetrant Type <u>ASTM WIRE B</u>	
Specification <u>Boiler/ Pressure Vessel</u>		Drawing Number:		Source Strength or MA/KV <u>102</u> <u>CI</u>		Emulsion Number <u>8250602N</u>		Exp. Date <u>1/1/21</u>		Penetrant Material <u>Stainless Steel</u>	
Procedure <u>RT ASME I R24</u>		Pipe O.D./ Pipe Thickness <u>.875"</u>		Plate Thickness		Focal Spot Size (F) <u>0.124"</u>		Exp. Time <u>1 MIN 45 SEC</u>		Penetrant Location Source Side ☒ Film Side ☐	
Acceptance Criteria <u>RT - ASME Sec. VIII</u>		Joint Type <u>Butt Weld</u>		Material <u>Carbon Steel</u>		Thickness With Reinforcement (d) <u>1.187"</u>		Film Technique <u>SWE/SWV</u>		Shim Material <u>NA</u> Thickness <u>NA</u>	
Exposure Technique <u>B</u>		Surface Condition <u>As Welded</u>		Source To Object (D) <u>20"</u>		Screen Thickness <u>010"- .010"</u>		ID Placement <u>Lead on Film</u>			
Viewing Single ☒ Double ☐		Film Processing Auto ☐ Manual ☒				Screen material <u>Lead</u>		Location Marker Placement Film Side ☒ Source Side ☐			
ISO Line #				Report #							

Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrant Density	Weld Density
LS 33U	0-1	RC		X				X								2.75	2.77
	1-2	RC	X												Scuff mark on film at the 2 location.	2.78	2.74
	2-3	RC	X												Scuff mark on film at the 2 location.	2.77	2.77
	3-4	RC		X				X								2.67	2.69
	4-5	RC		X				X								2.66	2.68
	5-6	RC		X				X								2.77	2.85
	6-7	RC		X				X								2.75	2.88
	7-8	RC	X													2.89	2.78
	8-9	RC	X													2.87	2.84
	9-10	RC	X													2.77	2.77
LS 36U	0-1	RC		X				X								2.80	2.81
	1-2	RC		X				X								2.90	2.91
	2-3	RC		X				X								2.89	2.88
	3-4	RC		X				X								3.02	3.00
	4-5	RC		X				X								2.78	2.79
	5-6	RC	X													2.89	2.88
	6-7	RC	X													2.99	3.00
	7-8	RC		X				X								2.84	2.95
	8-9	RC		X				X								3.00	3.02
	9-10	RC	X													2.87	2.84
LS 35U	0-1	RC		X	X											2.78	2.77
	1-2	RC	X													2.66	2.62
	2-3	RC	X													2.90	2.91
	3-4	RC	X													2.50	2.52
	4-5	RC	X													2.55	2.59
	5-6	RC	X													2.60	2.60
	6-7	RC	X													2.89	2.88
	7-8	RC	X													2.78	2.77
	8-9	RC	X													2.75	2.70
	9-10	RC	X														





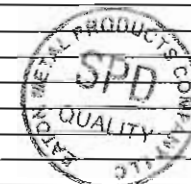
00 Salt Lake City, UT Denver, CO Billings, MT Farmington, NM
(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115

Client: EATON METAL
Job Location: SLC, Utah
Job Reference: 5361-1 Repairs

Date: 3/13/2019
Team W.O.: 1116-001390
Client P.O.: 45650

Customer EATON METAL	Type Of Weld Built Weld	Radiation Source IR-192 ☒ CO-60 ☐ X-Ray ☐	Film Type AGFA D5	Film Size 4.5 X 17	Penetrant Type ASTM WIRE B
Specification Boiler/Pressure Vessel	Drawing Number	Source Strength or MA/KV 94 CI	Emulsion Number 8250602N	Exp. Date 1/1/21	Penetrant Material Stainless Steel
Procedure RT, ASME, 1 R24	Pipe O.D. / Pipe Thickness 875"	Plate Thickness	Focal Spot Size (F) 0.124"	Exp. Time 2 MIN	Penetrant Location Source Side ☒ Film Side ☐
Acceptance Criteria RT - ASME Sec. VIII	Joint Type Built Weld	Material Carbon Steel	Thickness With Reinforcement (d) 1.187"	Film Technique SWE/SWV	Shim Material NA
Exposure Technique B	Surface Condition As Welded	Source To Object (D) 20"	Screen Thickness 010"-010"	Lead on Film	ID Placement
Viewing Single ☒ Double ☐	Film Processing Auto ☐ Manual ☒	Report #	Screen material Lead	Location Marker Placement Film Side ☒ Source Side ☐	

Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrant Density	Weld Density
LS 34U	0-1	RC	X													2.66	2.24
	8-9	RC		X	X											2.90	2.95
LS 35U	0-1	RC	X			X										2.92	2.69
LS 36U	0-1	RC	X													3.15	3.16
	1-2	RC	X													3.08	3.05
	2-3	RC	X												scuff on film at 3 location	3.18	3.17
	3-4	RC		X				X								3.15	3.16
	4-5	RC	X													2.87	2.89
	5-6	RC	X													2.86	2.84
	6-7	RC	X													2.86	2.88
	7-8	RC	X													3.12	3.11
	8-9	RC	X													3.04	3.07
	9-10	RC	X												scuff on film	3.16	3.20
LS 32U	9-10	RC	X													2.90	2.90
LS 38U	0-1	RC		X	X			X								2.84	2.74
LS 33U	0-1	RC		X	X											2.45	2.94
	1-2	RC		X				X								2.87	2.42
	2-3	RC	X													2.82	2.81
	3-4	RC	X													3.24	3.25
	4-5	RC	X													3.22	3.24
	5-6	RC	X													3.21	3.24
	6-7	RC	X													3.02	2.97
	7-8	RC		X				X								3.02	3.15
	8-9	RC	X			X										3.01	3.12
	9-10	RC	X													2.91	2.01



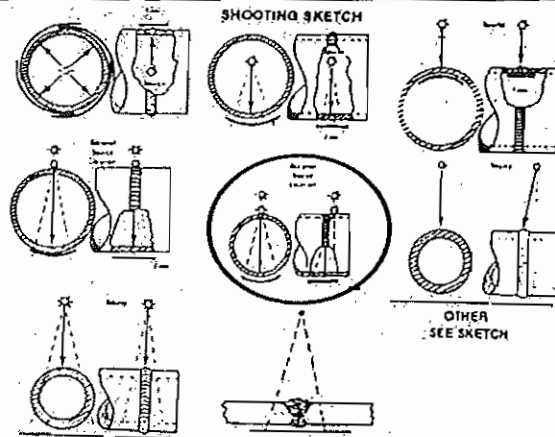
Phone: 208-232-2663 Fax: 208-232-2772

No. BI33019



RI - Rounded Inclusion
DT - Drop Through
BT - Burn through
FA - Film Artifact

Film delivery _____ Date _____



The recorded results are the opinion of the technician to the best of his knowledge based on the information provided to him by the customer at the time of the inspection.

14251 U.S. Highway 30, Pocatello, ID 83202
Phone: 208-232-2663 Fax: 208-232-2772

Radiographic Inspection Report

No. B14-319

[illegible]

Phone: 208-232-2663 Fax: 208-232-2772

Radiographic Inspection Report

No. B133019

[illegible]

DEFECT CODE		
IP - Incomplete penetration	EI - Elongated Inclusion	RI - Rounded Inclusion
CV - Concavity Root	CX - Convexity Root	DT - Drop Through
IF - Incomplete fusion	UC - Undercut	BT - Burn through
C - Crack	OX - Oxidation	FA - Film Artifact

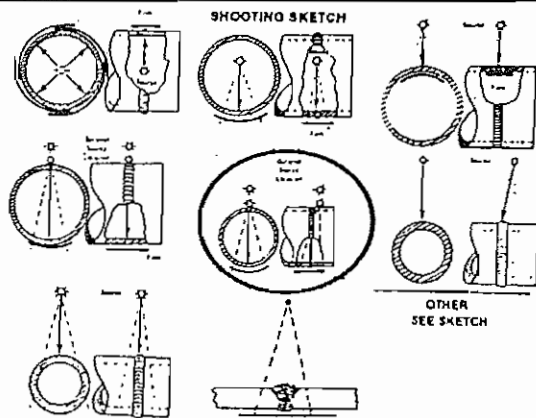
FILM USED:

1	FILMS	4.5	X	17	TYPE	Agfa d5
	FILMS		X		TYPE	
	FILMS		X		TYPE	

Total hrs.	Total Mileage	Number of Welds
------------	---------------	-----------------

Brandon Latimer	Bye	11
Radiographer		Level
Cynthia latimer	Cynthia Latimer	1
Radiographer Ass't		Level
Film delivery		Date

SHOOTING SKETCH



OTHER
SEE SKETCH

The recorded results are the opinion of the technician to the best of his knowledge based on the information provided to him by the customer at the time of the inspection.

14251 U.S. Highway 30, Pocatello, ID 83202
Phone: 208-232-2663 Fax: 208-232-2772

Radiographic Inspection Report

No. 814319

[illegible]

TEAM		Salt Lake City, UT Denver, CO Billings, MT Farmington, NM				Client: EATON METAL		Date: 3/5/2019									
(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115		Job Location: SLC, Utah		Team W.O.: 1116-001390		Job Reference: 5361-1		Client P.O.: 45650									
Customer EATON METAL	Type Of Weld Butt Weld		Radiation Source IR-192 ☒ CO-60 ☐ X-Ray ☐		Film Type AGFA D5	Film Size 4.5 X 17	Penetrameter Type ASTM WIRE 8										
Specification Boiler Pressure Vessel	Drawing Number		Source Strength or MA/KV 102		Emulsion Number 8250602N	Exp. Date 1/1/21	Penetrameter Material Stainless Steel										
Procedure RT ASME 1 R24	Pipe O.D. / Pipe Thickness 875"	Plate Thickness	Focal Spot Size (F) 0.124"	Exp. Time 1 MIN 45 SEC.	Single Load ☒	Double Load ☐	Penetrameter Location Source Side ☒ Film Side ☐										
Acceptance Criteria RT - ASME Sec VIII	Joint Type Butt Weld	Material Carbon Steel	Thickness With Reinforcement (d) 1.187"		Film Technique SWE/SWV		Shim Material NA	Thickness NA									
Exposure Technique B	Surface Condition As Welded		Source To Object (D) 20"		Screen Thickness 010" - 010"		ID Placement Lead on Film										
Viewing Single ☒ Double ☐	Film Processing Auto ☐ Manual ☒		Report #		Screen material Lead		Location Marker Placement Film Side ☒ Source Side ☐										
ISO Line #																	
Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrameter Density	Weld Density
LS 33U	0-1	RC		X				X								2.75	2.77
	1-2	RC	X												Scuff mark on film at the 2 location	2.78	2.74
	2-3	RC	X												Scuff mark on film at the 2 location	2.77	2.77
	3-4	RC		X				X								2.67	2.69
	4-5	RC		X				X								2.66	2.68
	5-6	RC		X				X								2.77	2.85
	6-7	RC		X				X								2.75	2.88
	7-8	RC	X													2.89	2.78
	8-9	RC	X													2.87	2.84
	9-10	RC	X													2.77	2.77
LS 36U	0-1	RC		X				X								2.80	2.81
	1-2	RC		X				X								2.90	2.91
	2-3	RC		X				X								2.89	2.88
	3-4	RC		X				X								3.02	3.00
	4-5	RC		X				X								2.78	2.79
	5-6	RC	X													2.89	2.88
	6-7	RC	X													2.99	3.00
	7-8	RC		X				X								2.84	2.95
	8-9	RC		X				X								3.00	3.02
	9-10	RC	X													2.87	2.84
LS 35U	0-1	RC		X	X											2.78	2.77
	1-2	RC	X													2.66	2.62
	2-3	RC	X													2.90	2.91
	3-4	RC	X													2.50	2.52
	4-5	RC	X													2.55	2.59
	5-6	RC	X													2.60	2.60
	6-7	RC	X													2.89	2.88
	7-8	RC	X													2.78	2.77
	8-9	RC	X													2.75	2.70
	9-10	RC	X														



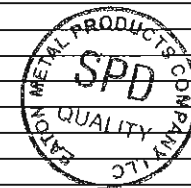
Client: _____ Date: _____ NOE Inspector: **Andrew Gruber** Date: **3/5/2019**
Form MS RT,ASME

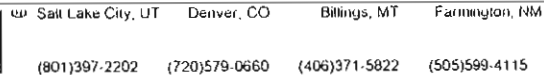
"Client has final authority and responsibility for interpretation and acceptance of examination and reports"

TEAM Salt Lake City, UT Denver, CO Billings, MT Farmington, NM (801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115				Client: EATON METAL				Date: 3/13/2019			
				Job Location: SLC, Utah				Team W.O: 1116-001390			
Job Reference: 5361-1 Repairs				Client P.O.: 45650							

Customer EATON METAL		Type Of Weld Butt Weld		Radiation Source IR- 192 ☒ CO- 60 ☐ X-Ray ☐		Film Type AGFA D5		Film Size 4.5 X 17		Penetrant Type ASTM WIRE B	
Specification Boiler/ Pressure Vessel		Drawing Number		Source Strength or MA/KV 94 CI		Emulsion Number 8250602N		Exp. Date 1/1/21		Penetrant Material Stainless Steel	
Procedure RT ASME 1 R24		Pipe O.D./ Pipe Thickness .875"		Plate Thickness		Focal Spot Size (F) 0.124"		Exp. Time 2 MIN		Penetrant Location Source Side ☒ Film Side ☐	
Acceptance Criteria RT - ASME Sec. VIII		Joint Type Butt Weld		Material Carbon Steel		Thickness With Reinforcement (d) 1.187"		Film Technique SWE/SWV		Shim Material Thickness NA NA	
Exposure Technique B		Surface Condition As Welded		Source To Object (D) 20"		Screen Thickness .010"-.010"		ID Placement Lead on Film		Location Marker Placement Film Side ☒ Source Side ☐	
Viewing Single ☒ Double ☐		Film Processing Auto ☐ Manual ☒		Report #		Screen material Lead					
ISO Line #											

Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrant Density	Weld Density
LS 34U	0-1	RC	X													2.66	2.24
	8-9	RC		X	X											2.90	2.95
LS 35U	0-1	RC	X			X										2.92	2.69
LS 36U	0-1	RC	X													3.15	3.16
	1-2	RC	X													3.08	3.05
	2-3	RC	X												scuff on film at 3 loction	3.18	3.17
	3-4	RC		X				X								3.15	3.16
	4-5	RC	X													2.87	2.89
	5-6	RC	X													2.86	2.84
	6-7	RC	X													2.86	2.88
	7-8	RC	X													3.12	3.11
	8-9	RC	X													3.04	3.07
	9-10	RC	X												scuff om film	3.16	3.20
LS 32U	9-10	RC	X													2.90	2.90
LS 38U	0-1	RC		X	X			X								2.84	2.74
LS 33U	0-1	RC		X	X											2.45	2.94
	1-2	RC		X				X								2.87	2.42
	2-3	RC	X													2.82	2.81
	3-4	RC	X													3.24	3.25
	4-5	RC	X													3.22	3.24
	5-6	RC	X													3.21	3.24
	6-7	RC	X													3.02	2.97
	7-8	RC		X				X								3.02	3.15
	8-9	RC	X			X										3.01	3.12
	9-10	RC	X													2.91	2.01





Client:	EATON METAL
Job Location:	SLC, Utah
Job Reference:	5361-1 Repairs

Date	3/15/2019
Team W.O.	1116-001390
Client P.O.	45650

[illegible]

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Phone: 208-232-2663 Fax: 208-232-2772

No. B133019

The recorded results are the opinion of the technician to the best of his knowledge based on the information provided to him by the customer at the time of the inspection.



00 Salt Lake City, UT Denver, CO Billings, MT Farmington, NM
(801)397-2202 (720)579-0660 (406)371-5822 (505)599-4115

Client: EATON METAL
Job Location: SLC, Utah
Job Reference: 5361-1 Repairs

Date: 3/13/2019
Team W.O: 1116-001390
Client P.O: 45650

Customer EATON METAL	Type Of Weld Butt Weld	Radiation Source IR-192 ☒ CO-60 ☐ X-Ray ☐	Film Type AGFA D5	Film Size 4 5 X 17	Penetrant Type ASTM WIRE B
Specification Boiler/ Pressure Vessel	Drawing Number	Source Strength or MA/KV 94 CI	Emulsion Number 8250602N	Exp. Date 1/1/21	Penetrant Material Stainless Steel
Procedure RT ASME 1 R24	Pipe O.D./ Pipe Thickness 875"	Plate Thickness	Focal Spot Size (F) 0.124"	Exp. Time 2 MIN	Penetrant Location Source Side ☒ Film Side ☐
Acceptance Criteria RT - ASME Sec. VIII	Joint Type Butt Weld	Material Carbon Steel	Thickness With Reinforcement (d) 1.187"	Film Technique SWE/SWV	Shim Material NA
Exposure Technique B	Surface Condition As Welded	Source To Object (d) 20"	Screen Thickness .010"-.010"	ID Placement Lead on Film	Location Marker Placement Film Side ☒ Source Side ☐
Viewing Single ☒ Double ☐	Film Processing Auto ☐ Manual ☒	Report #			

Weld No.	View	Weld I.D.	Accept	Reject	Porosity	Slag	Crack	Incomplete Fusion	Incomplete Penetration	Undercut	Burn Through	Surface Indication	Tungsten Inclusion	Concavity	Remarks	Penetrant Density	Weld Density
LS 34U	0-1	RC	X													2.66	2.24
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LS 35U	0-1	RC	X			X										2.92	2.69
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	3-4	RC		X				X								3.15	3.16
	4-5	RC	X													2.87	2.89
	5-6	RC	X													2.86	2.84
	6-7	RC	X													2.86	2.88
	7-8	RC	X													3.12	3.11
	8-9	RC	X													3.04	3.07
	9-10	RC	X												scuff on film	3.16	3.20
LS 32U	9-10	RC	X													2.90	2.90
LS 38U	0-1	RC		X	X			X								2.84	2.74
LS 33U	0-1	RC		X	X											2.45	2.94
	1-2	RC		X				X								2.87	2.42
	2-3	RC	X													2.82	2.81
	3-4	RC	X													3.24	3.25
	4-5	RC	X													3.22	3.24
	5-6	RC	X													3.21	3.24
	6-7	RC	X													3.02	2.97
	7-8	RC		X				X								3.02	3.15
	8-9	RC	X			X										3.01	3.12
	9-10	RC	X													2.91	2.01



14251 U.S. Highway 30, Pocatello, ID 83202
Phone: 208-232-2663 Fax: 208-232-2772

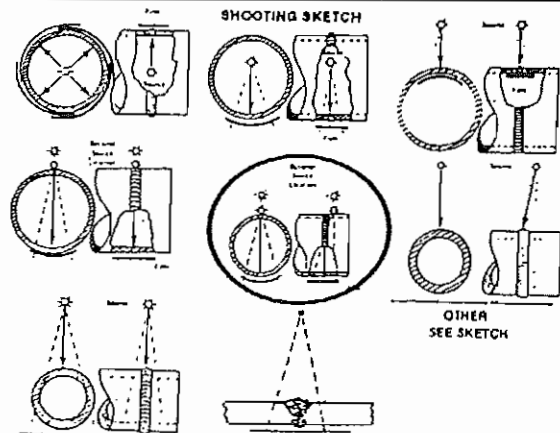
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DEFECT CODE		
IP - Incomplete penetration	EI - Elongated Inclusion	RI - Rounded Inclusion
CV - Concavity Root	CX - Convexity Root	DT - Drop Through
IF - Incomplete fusion	UC - Undercut	BT - Burn through
C - Crack	OX - Oxidation	FA - Film Artifact

1	FILMS	4.5	X	17	TYPE	Agfa d5
	FILMS		X		TYPE	
	FILMS		X		TYPE	

Total hrs.	Total Mileage	Number of Welds
------------	---------------	-----------------

Brandon Latimer	<i>Bye</i>	II
Radiographer		Level
Cynthia latimer	<i>Cynthia Latimer</i>	I
Radiographer Ass't		Level
Film delivery		Date



The recorded results are the opinion of the technician to the best of his knowledge based on the information provided to him by the customer at the time of the inspection.

Phone: 208-232-2663 Fax: 208-232-2772

No. B14319

The recorded results are the opinion of the technician to the best of his knowledge based on the information provided to him by the customer at the time of the inspection.



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736

Weld Procedure Specifications

WELDING PROCEDURE SPECIFICATION (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P1-EM14K1-A **Revision** 0 **Date** 10/27/2014
Supporting PQR No P1G1-P1G2-EM14KT-A20U-1
Welding Process SAW **Type** Machine
Impact Qualified WPS No **to** N/A **at** N/A

JOINTS (QW-402)

		Typical		
Joint Design	All			
Groove Type	Any			
Root Spacing	0" - 3/8"			
Fillet	All			
Root Face	≥ 1/16"			
Backing	Yes			
Backing Type	Weld/Base/Temporary Metal			
Groove Angle	See Typical Joint Details			
Back gouge	Carbon Arc and/or Grind			
Retainers	Prohibited			
Notes That Apply	1 & 2			

Note 1: Customer representative shall accept all weld joint designs specified on job specific drawings.

Note 2: Back gouge and/or grind to sound metal is required when this procedure is used for the first pass in a groove joint that requires cjp.

BASE METALS (QW-403)

Thickness Qualified	1"				
Thickness Range:	Groove	3/16"	to	1-1/2"	Fillet No Min to No Max
P-No	1	Group No	N/A	to	P-No 1 Group No N/A
Maximum Pass Thickness	< 1/2"				

FILLER METALS (QW-404)

SFA #/Specification	5.17
AWS Classification	EM14K
F-No	6
A-No	1
Filler Metal Diameter	3/32" - 1/8"
Filler Metal Product Form	Solid
Filler Metal Trade Name	ESAB Spoolarc 71
Thickness Range:	
Groove	No Min to 1-1/2"
Fillet	No Min to No Max
Electrode-Flux Class	F7A2-EM14K
Flux Trade Name	ESAB OK FLUX 10.71
Flux Type	Neutral
Alloy Flux	N/A
Recrushed Slag	Prohibited
Supplemental Filler	None
Alloy Elements	N/A

ELECTRICAL (QW-409)

Current and Polarity	DCEP
Heat Input (MAX)	N/A
Other	N/A

PREHEAT (QW-406)

Minimum Preheat Temp	100°F Base Metal 3/16" - 1"
Minimum Preheat Temp	200°F Base Metal > 1"
Maximum Interpass Temp	500°F
Preheat Maintenance	Prior During
Other	Maintain until welding is complete

POSITIONS (QW-405)

Position(s) of Groove	1G
Welding Progression	N/A
Position(s) of Fillet	1F, 2F
Other	N/A

WPS No P1-P1-EM14K1-A Revision 0 Date 10/27/2014

Supporting PQR No P1G1-P1G2-EM14KT-A20U-1

POST WELD HEAT TREATMENT (QW-407)

Temperature Range None
Time at Temperature Range None

TECHNIQUE (QW-410)

String or Weave Bead	<u>N/A</u>
Maximum Pass Width	<u>7/8"</u>
Initial Cleaning	<u>Brushing and/or Chipping</u>
Interpass Cleaning	<u>Brushing/Chipping</u>
Multiple or Single Pass (Per Side)	<u>Single or Multiple</u>
Multiple or Single Electrodes	<u>Single</u>
Contact Tube to Work Distance	<u>3/4" - 1"</u>
Electrode Spacing (2 Arcs)	<u>N/A</u>
Angle of Electrode (SAW)	<u>10° Drag - 10° Push</u>
Peening	<u>Prohibited</u>
Oscillation for Automatic/Machine Welding	<u>None</u>

ELECTRICAL (QW-409)

Non-Waveform Controlled Welding

Weld Pass(es)	Process	Filler Metal		Current and Polarity	Amps	Volts	Travel Speed (Ipm)	Heat Input (MAX)
		Class	Diameter					
Root/Hot	SAW	EM14K	3/32" - 1/8"	DCEP	350 - 450	25 - 29	16 - 24	N/A
Hot/Fill	SAW	EM14K	3/32" - 1/8"	DCEP	400 - 500	28 - 32	18 - 22	N/A
Cap	SAW	EM14K	3/32" - 1/8"	DCEP	400 - 450	30 - 32	18 - 20	N/A

Use amps, volts, and travel speed to calculate heat input. Amps x Volts x 60 ÷ Travel Speed = Heat Input

This Weld Procedure Specification was prepared and accepted by

Dan Durtschi

on 10/27/2014

Accepted By _____ Plant 1 Denver, CO

Accepted By _____ Plant 2 Salt Lake City, UT

Accepted By _____ Plant 3 Pocatello, ID



Daniel Durtschi
CWI 11030421
QC1 EXP. 3/1/2017

All units referenced on WPS are in English (Standard, e.g. psi, inches, etc.) unless specifically noted.

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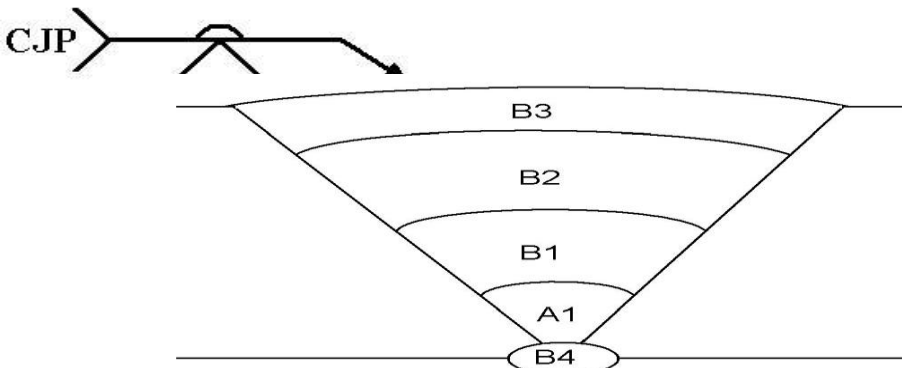
PROCEDURE QUALIFICATION RECORD (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

PQR No. P1G1-P1G2-EM14KT-A20U-1 Date of Welding 6/3/2014
Weld Process(es) (A) GMAWP (B) SAW Type(s) Semiautomatic/Machine

JOINT DETAILS (QW-402)

Joint Design Butt Joint
Groove Type Single V Groove
Root Spacing 0"
Root Face 1/8"
Backing Yes
Backing Type Base Metal/Weld Metal
Groove Angle 60°
Back gouged No
Retainers None



POSITION (QW-405)

Test Position 1G
Progression N/A

BASE METALS (QW-403)

Material Spec (1) A-36 to (2) SA-516-70 P-No 1 Gr# 1 to P-No 1 Gr# 2
Type/Grade, or UNS Number N/A to N/A Heat Treated Condition Hot Rolled
Material Thickness (T) 1" Diameter of Test Coupon N/A

FILLER METALS (QW-404)

	(A)	(B)
SFA Specification	5.18	5.17
AWS Classification	ER70S-6	EM14k
F-No	6	6
A-No	1	1
Filler Metal Trade Name	Lincoln SuperArc L-59	ESAB SpoolArc 71
Filler Metal Product Form	Solid	Solid
Supplemental Filler Metal	None	None
Alloy Elements	N/A	N/A
Electrode Flux Class	N/A	F7A2-EM14K
Flux Trade Name	N/A	ESAB OK FLUX 10.71
Flux Type	N/A	Neutral
Alloy Flux	N/A	N/A
Recrushed Slag Used	N/A	No
Weld Metal Thickness (t)	1/4" Consumed by SAW	1"
Maximum Pass Thickness	1/4"	5/32"

ELECTRODE

Electrode Spacing (2 Arcs)	N/A	3/4" Center to Center
Angle	N/A	Lead 0° Drag, Trail 12° Push
Contact Tube to Work	3/8"	1"

GAS (QW-408)

	Gases	Mixture (%)	Flow Rate (cfh)
Shielding	Ar/CO2	90/10	35
Trailing	None	None	None
Backing	None	None	None
Gas Cup Size	5/8"		

PREHEAT (QW-406)

Minimum Temperature 200
Preheat Maintenance Prior/During

TECHNIQUE (QW-410)

Multipass or Single Pass (per side) (A) Single, (B) Multiple
Single or Multiple Electrodes (A) Single, (B) Multiple
Initial and Interpass Cleaning Brushing/Grinding
Transfer Mode (A) Pulsed-Spray, (B) N/A
Peening Performed None
Maximum Pass Width 1"
Oscillation (Machine) None

POST WELD HEAT TREATMENT (QW-407)

Temperature None
Time None

ELECTRICAL (QW-409)

Pass(es)	Process	Class	Diameter		Current and Polarity		Amps		Volts		Travel Speed (ipm)	Heat Input (J/in)	Interpass Temp (°F)
			Lead	Trail	Lead	Trail	Lead	Trail	Lead	Trail			
A1	GMAWP	ER70S-6	.052"		DCEP		230		23.5		15	21,620	Preheat
B1	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	500	28	30	32	59,625	Preheat
B2	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	500	31	32	32	64,875	390°
B3	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	550	33	33	30	75,900	474°
B4	SAW	EM14K	1/8"	1/8"	DCEP	AC	800	450	35	35	30	87,500	422°

Heat input calculated using QW-409.1 (a), No instantaneous energy readout.

TENSILE TESTS (QW-150)

Specimen No	Width (in)	Thickness (in)	Diameter (in)	Area (in)	Ultimate Total Load (lbs)	Ultimate Stress (psi)	Location of Failure
1	0.746"	0.695"	N/A	0.5185"	38,171	73,500	Base Metal
2	0.745"	0.692"	N/A	0.5155"	38,041	74,000	Base Metal

GUIDED-BEND TESTS (QW-160)

Type and Figure No	Result	Type and Figure No	Result
Transverse Side Bend (QW-462.2)	Pass	Transverse Side Bend (QW-462.2)	Pass
Transverse Side Bend (QW-462.2)	Pass	Transverse Side Bend (QW-462.2)	Pass

TOUGHNESS TESTS (QW-170)

Specimen No	Notch Location	Specimen Size (in)	Notch Size (in)	Test Temp (F)	Impact Values (Ft LBS)	Shear %	Mils	Drop Weight Break
1	Weld Metal	.394x.394	0.315	-20	104	N/A	N/A	N/A
2	Weld Metal	.394x.395	0.315	-20	91	N/A	N/A	N/A
3	Weld Metal	.394x.395	0.315	-20	124	N/A	N/A	N/A
4	HAZ A-36	.394x.394	0.315	-20	83	N/A	N/A	N/A
5	HAZ A-36	.394x.395	0.315	-20	105	N/A	N/A	N/A
6	HAZ A-36	.394x.395	0.315	-20	106	N/A	N/A	N/A
7	HAZ SA-516	.394x.395	0.315	-20	111	N/A	N/A	N/A
8	HAZ SA-516	.394x.395	0.315	-20	82	N/A	N/A	N/A
9	HAZ SA-516	.394x.395	0.315	-20	75	N/A	N/A	N/A

Impact testing performed to ASME VIII**HARDNESS TEST - ROCKWELL B**

Base Metal				Heat Affected Zone			Weld Metal		
A-36	75 Rb	77 Rb	77 Rb	81 Rb	80 Rb	81 Rb	90 Rb	91 Rb	91 Rb
SA-516	88 Rb	77 Rb	77 Rb	93 Rb	91 Rb	90 Rb			

DEPOSITED CHEMICAL ANALYSIS

C	Si	Mn	P	S	Al	V	Cr	Ni	Fe	Ce
0.100	0.590	1.410	0.015	0.013	N/A	N/A	0.051	0.059	N/A	N/A

Chemical Analysis Conforms to A# 1**MATERIAL TRACABILITY**

Item Description	<u>A-36</u>	Heat Number	<u>A2K326</u>	Manufacturer	<u>SSAB</u>
Item Description	<u>SA-516-70</u>	Heat Number	<u>B2G551</u>	Manufacturer	<u>SSAB</u>

WELDING INFORMATION

Welding machine used	<u>(A) Lincoln 455m/STT w/ 25m Feeder box (B) Power Wave AC/DC 1000 w/ Lincoln Power Feed 10A Controller</u>				
Welder Name	<u>Richard Carter</u>	ID Number	<u>28117</u>	Stamp	<u>RC</u>

TESTING INFORMATION

Tests Conducted By	<u>MSI Testing Inc.</u>	Laboratory Test Number	<u>14-154</u>	Date of Testing	<u>6/5/2014</u>
Preparation and welding of test coupon was witnessed by <u>Jacob Mowat</u>					

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX.

This Procedure Qualification Record was prepared and accepted by Jacob Mowat on 6/9/2014

Accepted By _____ Plant 1 Denver, CO
 Accepted By _____ Plant 2 Salt Lake City, UT
 Accepted By _____ Plant 3 Pocatello, ID

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

Uncontrolled copy if not signed by plant representative

 Jacob Mowat
 CWI 13100541
 QC1 EXP. 10/1/2016

WELDING PROCEDURE SPECIFICATION (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P1-EM14K2-A **Revision** 0 **Date** 6/19/2014
Supporting PQR No P1G1-P1G2-EM14KT-A20U-1
Welding Process SAW **Type** Machine
Impact Qualified WPS No **to** N/A **at** N/A

JOINTS (QW-402)

		Typical		
Joint Design	All			
Groove Type	Any			
Root Spacing	0" - 1/4"			
Fillet	Any			
Root Face	0" - 3/8"			
Backing	Yes			
Backing Type	Weld/Base Metal, Temporary			
Groove Angle	See Typical Joint Details			
Back gouge	Yes (Carbon Arc and/or Grind)			
Retainers	Prohibited			
Notes That Apply	1,2			

Note 1: Customer representative shall accept all weld joint designs specified on job specific drawings.

Note 2: Back gouge and/or grind to sound metal is required when this procedure is used for the first pass in a groove joint that requires cjp.

BASE METALS (QW-403)

Thickness Qualified	1"			
Thickness Range:	Groove	3/16"	to	1 - 1/2"
	Fillet	No Min.	to	No Max
P-No	1	Group No	N/A	
Maximum Pass Thickness	≤ 1/2"			
Heat Treated Condition	N/A			

FILLER METALS (QW-404)

SFA #/Specification	5.17
AWS Classification	EM14K
F-No	6
A-No	1
Filler Metal Diameter	3/32" - 5/32"
Filler Metal Product Form	Solid
Filler Metal Trade Name	ESAB Spool Arc 71
Thickness Range:	
Groove	3/16" to 1 - 1/2"
Fillet	No Min. to No Max
Electrode-Flux Class	F7A4-EM14K
Flux Trade Name	ESAB OK 10.71
Flux Type	Neutral
Alloy Flux	N/A
Recrushed Slag	Prohibited
Supplemental Filler	None
Alloy Elements	N/A

ELECTRICAL (QW-409)

Current and Polarity	DCEP
Heat Input (MAX)	85,000 J/in.
Other	None

PREHEAT (QW-406)

Minimum Preheat Temp	100°F Base Metal 3/16" - 1"
Minimum Preheat Temp	200°F Base Metal > 1"
Maximum Interpass Temp	500°F
Preheat Maintenance	Maintian Until Welding is Complete
Other	None

POSITIONS (QW-405)

Position(s) of Groove	1G
Welding Progression	N/A
Position(s) of Fillet	1F, 2F
Other	None

WPS No P1-P1-EM14K2-A Revision 0 Date 6/19/2014

Supporting PQR No P1G1-P1G2-EM14KT-A20U-1

POST WELD HEAT TREATMENT (QW-407)

Temperature Range None

Time at Temperature Range None

Note: Vessels that will be exposed to environments that could cause stress corrosion cracking shall have a minimum hold temperature of 1150°F.

Note: For welds that may be exposed to environments that could cause stress corrosion cracking the minimum PWHT hold time shall be one hour per inch for thicknesses exceeding one inch

Note: A specific PWHT procedure shall be developed for each job.

TECHNIQUE (QW-410)

String or Weave Bead	N/A
Maximum Pass Width	1"
Initial Cleaning	Grinding
Interpass Cleaning	Chipping
Multiple or Single Pass (Per Side)	Single or Multiple pass(es) per side
Multiple or Single Electrodes	Single or Multiple Electrode(s)
Contact Tube to Work Distance	3/4" - 7/8"
Electrode Spacing (2 Arcs)	5-16" - 3/8" Center to Center
Angle of Electrode (SAW)	5° Drag
Peening	Prohibited
Oscillation for Automatic/Machine Welding	No

ELECTRICAL (QW-409)

Non-Waveform Controlled Welding

Weld Pass(es)	Process	Filler Metal		Current and Polarity	Amps	Volts	Travel Speed (ipm)	Heat Input (MAX)
		Class	Diameter					
First Pass	SAW	EM14K	3/32"-5/32"	DCEP	450 - 600	28 - 30	26 - 32	85,000 J/in.
Fill Passes	SAW	EM14K	3/32"-5/32"	DCEP	600 - 700	28 - 33	20 - 30	85,000 J/in.
Cap Passes	SAW	EM14K	3/32"-5/32"	DCEP	550 - 600	33 - 35	24 - 30	85,000 J/in.

Use amps, volts, and travel speed to calculate heat input. Amps x Volts x 60 ÷ Travel Speed = Heat Input

This Weld Procedure Specification was prepared and accepted by Jacob Mowat on 6/19/2014

Accepted By _____ Plant 1 Denver, CO

Accepted By _____ Plant 2 Salt Lake City, UT

Accepted By _____ Plant 3 Pocatello, ID



Jacob Mowat
CWI 13100541
QC1 EXP. 10/1/2016

All units referenced on WPS are in English (Standard, e.g. psi, inches, etc.) unless specifically noted.

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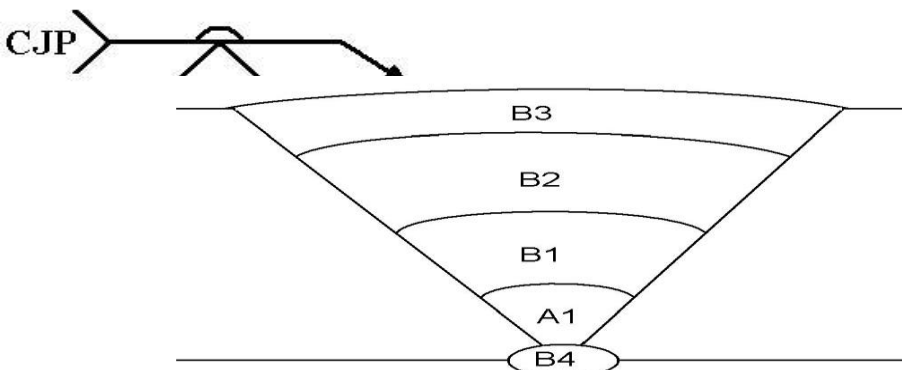
PROCEDURE QUALIFICATION RECORD (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

PQR No. P1G1-P1G2-EM14KT-A20U-1 Date of Welding 6/3/2014
Weld Process(es) (A) GMAWP (B) SAW Type(s) Semiautomatic/Machine

JOINT DETAILS (QW-402)

Joint Design Butt Joint
Groove Type Single V Groove
Root Spacing 0"
Root Face 1/8"
Backing Yes
Backing Type Base Metal/Weld Metal
Groove Angle 60°
Back gouged No
Retainers None



POSITION (QW-405)

Test Position 1G
Progression N/A

BASE METALS (QW-403)

Material Spec (1) A-36 to (2) SA-516-70 P-No 1 Gr# 1 to P-No 1 Gr# 2
Type/Grade, or UNS Number N/A to N/A Heat Treated Condition Hot Rolled
Material Thickness (T) 1" Diameter of Test Coupon N/A

FILLER METALS (QW-404)

	(A)	(B)
SFA Specification	5.18	5.17
AWS Classification	ER70S-6	EM14k
F-No	6	6
A-No	1	1
Filler Metal Trade Name	Lincoln SuperArc L-59	ESAB SpoolArc 71
Filler Metal Product Form	Solid	Solid
Supplemental Filler Metal	None	None
Alloy Elements	N/A	N/A
Electrode Flux Class	N/A	F7A4-EM14K
Flux Trade Name	N/A	ESAB OK FLUX 10.71
Flux Type	N/A	Neutral
Alloy Flux	N/A	N/A
Recrushed Slag Used	N/A	No
Weld Metal Thickness (t)	1/4" Consumed by SAW	1"
Maximum Pass Thickness	1/4"	5/32"

ELECTRODE

Electrode Spacing (2 Arcs)	N/A	3/4" Center to Center
Angle	N/A	Lead 0° Drag, Trail 12° Push
Contact Tube to Work	3/8"	1"

GAS (QW-408)

	Gases	Mixture (%)	Flow Rate (cfh)
Shielding	Ar/CO2	90/10	35
Trailing	None	None	None
Backing	None	None	None
Gas Cup Size	5/8"		

PREHEAT (QW-406)

Minimum Temperature 200
Preheat Maintenance Prior/During

TECHNIQUE (QW-410)

Multipass or Single Pass (per side) (A) Single, (B) Multiple
Single or Multiple Electrodes (A) Single, (B) Multiple
Initial and Interpass Cleaning Brushing/Grinding
Transfer Mode (A) Pulsed-Spray, (B) N/A
Peening Performed None
Maximum Pass Width 1"
Oscillation (Machine) None

POST WELD HEAT TREATMENT (QW-407)

Temperature None
Time None

ELECTRICAL (QW-409)

Pass(es)	Process	Class	Diameter		Current and Polarity		Amps		Volts		Travel Speed (ipm)	Heat Input (J/in)	Interpass Temp (°F)
			Lead	Trail	Lead	Trail	Lead	Trail	Lead	Trail			
A1	GMAWP	ER70S-6	.052"		DCEP		230		23.5		15	21,620	Preheat
B1	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	500	28	30	32	119,625	Preheat
B2	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	500	31	32	32	129,937	390°
B3	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	550	33	33	30	151,800	474°
B4	SAW	EM14K	1/8"	1/8"	DCEP	AC	800	450	35	35	30	175,000	422°

Heat input calculated using QW-409.1 (a), No instantaneous energy readout.

TENSILE TESTS (QW-150)

Specimen No	Width (in)	Thickness (in)	Diameter (in)	Area (in)	Ultimate Total Load (lbs)	Ultimate Stress (psi)	Location of Failure
1	0.746"	0.695"	N/A	0.5185"	38,171	73,500	Base Metal
2	0.745"	0.692"	N/A	0.5155"	38,041	74,000	Base Metal

GUIDED-BEND TESTS (QW-160)

Type and Figure No	Result	Type and Figure No	Result
Transverse Side Bend (QW-462.2)	Pass	Transverse Side Bend (QW-462.2)	Pass
Transverse Side Bend (QW-462.2)	Pass	Transverse Side Bend (QW-462.2)	Pass

TOUGHNESS TESTS (QW-170)

Specimen No	Notch Location	Specimen Size (in)	Notch Size (in)	Test Temp (F)	Impact Values (Ft LBS)	Shear %	Mils	Drop Weight Break
1	Weld Metal	.394x.394	0.315	-20	104	N/A	N/A	N/A
2	Weld Metal	.394x.395	0.315	-20	91	N/A	N/A	N/A
3	Weld Metal	.394x.395	0.315	-20	124	N/A	N/A	N/A
4	HAZ A-36	.394x.394	0.315	-20	83	N/A	N/A	N/A
5	HAZ A-36	.394x.395	0.315	-20	105	N/A	N/A	N/A
6	HAZ A-36	.394x.395	0.315	-20	106	N/A	N/A	N/A
7	HAZ SA-516	.394x.395	0.315	-20	111	N/A	N/A	N/A
8	HAZ SA-516	.394x.395	0.315	-20	82	N/A	N/A	N/A
9	HAZ SA-516	.394x.395	0.315	-20	75	N/A	N/A	N/A

Impact testing performed to ASME VIII**HARDNESS TEST - ROCKWELL B**

Base Metal				Heat Affected Zone			Weld Metal		
A-36	75 Rb	77 Rb	77 Rb	81 Rb	80 Rb	81 Rb	90 Rb	91 Rb	91 Rb
SA-516	88 Rb	77 Rb	77 Rb	93 Rb	91 Rb	90 Rb			

DEPOSITED CHEMICAL ANALYSIS

C	Si	Mn	P	S	Al	V	Cr	Ni	Fe	Ce
0.100	0.590	1.410	0.015	0.013	N/A	N/A	0.051	0.059	N/A	N/A

Chemical Analysis Conforms to A# 1**MATERIAL TRACABILITY**

Item Description	<u>A-36</u>	Heat Number	<u>A2K326</u>	Manufacturer	<u>SSAB</u>
Item Description	<u>SA-516-70</u>	Heat Number	<u>B2G551</u>	Manufacturer	<u>SSAB</u>

WELDING INFORMATION

Welding machine used	<u>(A) Lincoln 455m/STT w/ 25m Feeder box (B) Power Wave AC/DC 1000 w/ Lincoln Power Feed 10A Controller</u>				
Welder Name	<u>Richard Carter</u>	ID Number	<u>28117</u>	Stamp	<u>RC</u>

TESTING INFORMATION

Tests Conducted By	<u>MSI Testing Inc.</u>	Laboratory Test Number	<u>14-154</u>	Date of Testing	<u>6/5/2014</u>
Preparation and welding of test coupon was witnessed by <u>Jacob Mowat</u>					

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX.

This Procedure Qualification Record was prepared and accepted by Jacob Mowat on 6/9/2014

Accepted By _____ Plant 1 Denver, CO
 Accepted By _____ Plant 2 Salt Lake City, UT
 Accepted By _____ Plant 3 Pocatello, ID

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

Uncontrolled copy if not signed by plant representative



Jacob Mowat
 CWI 13100541
 QC1 EXP. 10/1/2016

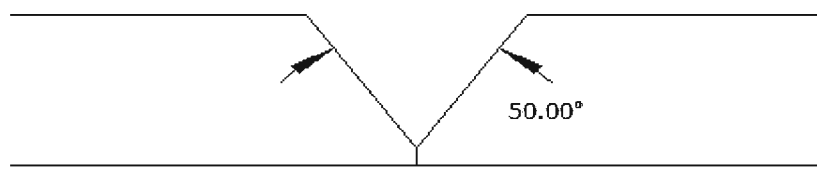
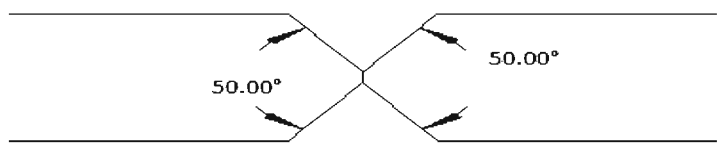
WELDING PROCEDURE SPECIFICATION (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P1-EM14KT-A **Revision** 2 **Date** 12/15/2014
Supporting PQR No P1G1-P1G2-EM14KT-A20U-1
Welding Process SAW **Type** Machine
Impact Qualified WPS No **to** N/A **at** N/A

JOINTS (QW-402)

Typical

Joint Design	All	Single V Groove Joint 
Groove Type	Any	
Root Spacing	0" - 3/16"	
Fillet	Any	
Root Face	1/16" - 3/16"	
Backing	Yes	Double V Groove Joint 
Backing Type	Weld/Base Metal, Temporary	
Groove Angle	50° - 60°	
Back gouge	No or Yes (Carbon Arc and or Grind)	
Retainers	Prohibited	
Notes That Apply	1,2	

Note 1: Customer representative shall accept all weld joint designs specified on job specific drawings.

Note 2: For joints that will not get back gouged a GMAW seal pass is required as shown on page 2.

Thickness Qualified 1"
Thickness Range: Groove 3/16" to 1-1/2" Fillet No Min. to No Max
P-No 1 **Group No** N/A to **P-No** 1 **Group No** N/A
Maximum Pass Thickness ≤ 1/2"

FILLER METALS (QW-404)

SFA #/Specification	5.17
AWS Classification	EM14K
F-No	6
A-No	1
Filler Metal Diameter	1/8"
Filler Metal Product Form	Solid
Filler Metal Trade Name	ESAB Spool Arc 71
Thickness Range:	
Groove	No Min. to 8"
Fillet	No Min. to No Max
Electrode-Flux Class	F7A2-EM14K
Flux Trade Name	ESAB OK Flux 10.71
Flux Type	Neutral
Alloy Flux	N/A
Recrushed Slag	Prohibited
Supplemental Filler	None
Alloy Elements	N/A

ELECTRICAL (QW-409)

Current and Polarity	DCEP/AC
Heat Input (MAX)	95,000 J/In
Other	None

PREHEAT (QW-406)

Minimum Preheat Temp	100°F Base Metal 3/16" - 1"
Minimum Preheat Temp	200°F Base Metal > 1"
Maximum Interpass Temp	550°F
Preheat Maintenance	Maintain Until Welding is Complete
Other	None

POSITIONS (QW-405)

Position(s) of Groove	1G
Welding Progression	N/A
Position(s) of Fillet	1F, 2F
Other	None

POST WELD HEAT TREATMENT (QW-407)

Temperature Range None
Time at Temperature Range None

TECHNIQUE (QW-410)

String or Weave Bead	String
Maximum Pass Width	1"
Initial Cleaning	Brushing and/or Grinding
Interpass Cleaning	Brushing/Chipping
Multiple or Single Electrodes	Single/Multiple (See electrical table)
Multiple or Single Pass Per Side	Single/Multiple (See weld diagrams)
Contact Tube to Work Distance	7/8" - 1"
Electrode Spacing (2 Arcs)	3/4" - 7/8"
Angle of Electrode (SAW)	Lead Arc 0° - Trail Arc 10° to 15° Push
Peening	Prohibited
Oscillation for Automatic/Machine Welding	No

ELECTRICAL (QW-409)**Non-Waveform Controlled Welding****For Single V Groove Joints**

Weld Pass(es)	Process	Filler Metal		Current and Polarity		Amps		Volts		Travel Speed (ipm)	Heat Input (MAX)
		Class	Diameter	Lead	Trail	Lead	Trail	Lead	Trail		
1st Pass	SAW	EM14K	1/8"	DCEP	AC	450 - 550	350 - 450	26 - 28	27 - 29	30 - 34	95,000 J/In
Fill Passes	SAW	EM14K	1/8"	DCEP	AC	650 - 750	500 - 600	28 - 32	30 - 32	30 - 34	95,000 J/In
Cap Passes	SAW	EM14K	1/8"	DCEP	AC	500 - 600	400 - 500	29 - 32	32 - 35	30 - 34	95,000 J/In
*Dig Pass	SAW	EM14K	1/8"	DCEP	N/A	700 - 725	N/A	34 - 35	N/A	29 - 30	95,000 J/In

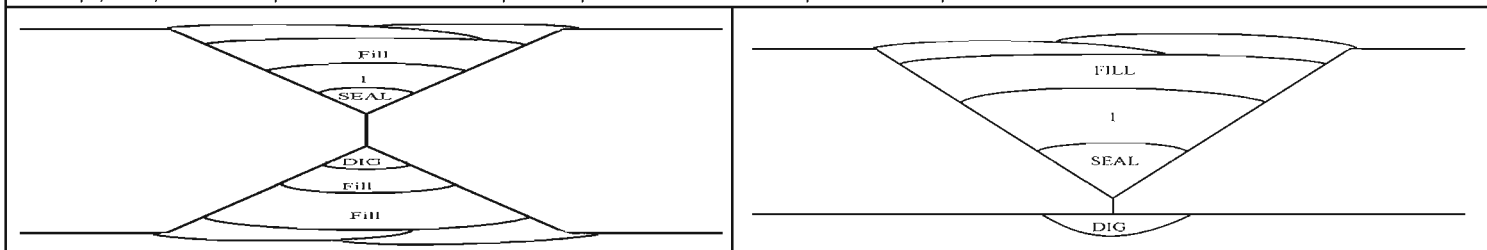
For Double V Groove Joints

Weld Pass(es)	Process	Filler Metal		Current and Polarity		Amps		Volts		Travel Speed (ipm)	Heat Input (MAX)
		Class	Diameter	Lead	Trail	Lead	Trail	Lead	Trail		
1st Pass	SAW	EM14K	1/8"	DCEP	AC	450 - 550	350 - 450	26 - 28	27 - 29	30 - 34	95,000 J/In
Fill Passes	SAW	EM14K	1/8"	DCEP	AC	675 - 800	550 - 650	28 - 32	30 - 32	30 - 34	95,000 J/In
Cap Passes	SAW	EM14K	1/8"	DCEP	AC	500 - 600	400 - 500	29 - 32	32 - 35	30 - 34	95,000 J/In
*Dig Pass	SAW	EM14K	1/8"	DCEP	AC	700 - 800	500 - 550	28 - 30	28 - 31	28 - 30	95,000 J/In

Use WPS P1-P1-GMAWP-A or P1-P1-GMAWP-STT-A for Seal Pass

*Dig Pass is the first SAW pass on opposite side of the seal pass, it shall consume the root face and seal pass

Use amps, volts, and travel speed to calculate heat input. Amps x Volts x 60 ÷ Travel Speed = Heat Input



This Weld Procedure Specification was prepared and accepted by

*Dan Durtschi*on 12/15/2014

Accepted By

Plant 1 Denver, CO

Accepted By

Plant 2 Salt Lake City, UT

Accepted By

Plant 3 Pocatello, ID



Daniel Durtschi
CWI 11030421
QC1 EXP. 3/1/2017

All units referenced on WPS are in English (Standard, e.g. psi, inches, etc.) unless specifically noted.

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PROCEDURE QUALIFICATION RECORD (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

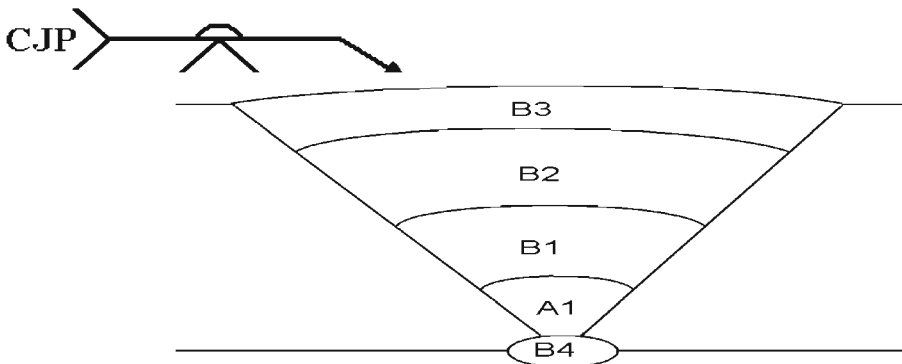
PQR No. P1G1-P1G2-EM14KT-A20U-1 Date of Welding 6/3/2014
Weld Process(es) (A) GMAWP (B) SAW Type(s) Semiautomatic/Machine

JOINT DETAILS (QW-402)

Joint Design Butt Joint
Groove Type Single V Groove
Root Spacing 0"
Root Face 1/8"
Backing Yes
Backing Type Base Metal/Weld Metal
Groove Angle 60°
Back gouged No
Retainers None

POSITION (QW-405)

Test Position 1G
Progression N/A



BASE METALS (QW-403)

Material Spec (1) A-36 to (2) SA-516-70 P-No 1 Gr# 1 to P-No 1 Gr# 2
Type/Grade, or UNS Number N/A to N/A Heat Treated Condition Hot Rolled
Material Thickness (T) 1" Diameter of Test Coupon N/A

FILLER METALS (QW-404)

	(A)	(B)
SFA Specification	5.18	5.17
AWS Classification	ER70S-6	EM14k
F-No	6	6
A-No	1	1
Filler Metal Trade Name	Lincoln SuperArc L-59	ESAB SpoolArc 71
Filler Metal Product Form	Solid	Solid
Supplemental Filler Metal	None	None
Alloy Elements	N/A	N/A
Electrode Flux Class	N/A	F7A2-EM14K
Flux Trade Name	N/A	ESAB OK FLUX 10.71
Flux Type	N/A	Neutral
Alloy Flux	N/A	N/A
Recrushed Slag Used	N/A	No
Weld Metal Thickness (t)	1/4" Consumed by SAW	1"
Maximum Pass Thickness	1/4"	5/32"

ELECTRODE

Electrode Spacing (2 Arcs)	N/A	3/4" Center to Center
Angle	N/A	Lead 0° Drag, Trail 12° Push
Contact Tube to Work	3/8"	1"

GAS (QW-408)

	Gases	Mixture (%)	Flow Rate (cfh)
Shielding	Ar/CO2	90/10	35
Trailing	None	None	None
Backing	None	None	None
Gas Cup Size	5/8"		

PREHEAT (QW-406)

Minimum Temperature 200
Preheat Maintenance Prior/During

TECHNIQUE (QW-410)

Multipass or Single Pass (per side) (A) Single, (B) Multiple
Single or Multiple Electrodes (A) Single, (B) Multiple
Initial and Interpass Cleaning Brushing/Grinding
Transfer Mode (A) Pulsed-Spray, (B) N/A
Peening Performed None
Maximum Pass Width 1"
Oscillation (Machine) None

POST WELD HEAT TREATMENT (QW-407)

Temperature None
Time None

ELECTRICAL (QW-409)

Pass(es)	Process	Class	Diameter		Current and Polarity		Amps		Volts		Travel Speed (ipm)	Heat Input (J/in)	Interpass Temp (°F)
			Lead	Trail	Lead	Trail	Lead	Trail	Lead	Trail			
A1	GMAWP	ER70S-6	.052"		DCEP		230		23.5		15	21,620	Preheat
B1	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	500	28	30	32	59,625	Preheat
B2	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	500	31	32	32	64,875	390°
B3	SAW	EM14K	1/8"	1/8"	DCEP	AC	600	550	33	33	30	75,900	474°
B4	SAW	EM14K	1/8"	1/8"	DCEP	AC	800	450	35	35	30	87,500	422°

Heat input calculated using QW-409.1 (a), No instantaneous energy readout.

TENSILE TESTS (QW-150)

Specimen No	Width (in)	Thickness (in)	Diameter (in)	Area (in)	Ultimate Total Load (lbs)	Ultimate Stress (psi)	Location of Failure
1	0.746"	0.695"	N/A	0.5185"	38,171	73,500	Base Metal
2	0.745"	0.692"	N/A	0.5155"	38,041	74,000	Base Metal

GUIDED-BEND TESTS (QW-160)

Type and Figure No	Result	Type and Figure No	Result
Transverse Side Bend (QW-462.2)	Pass	Transverse Side Bend (QW-462.2)	Pass
Transverse Side Bend (QW-462.2)	Pass	Transverse Side Bend (QW-462.2)	Pass

TOUGHNESS TESTS (QW-170)

Specimen No	Notch Location	Specimen Size (in)	Notch Size (in)	Test Temp (F)	Impact Values (Ft LBS)	Shear %	Mils	Drop Weight Break
1	Weld Metal	.394x.394	0.315	-20	104	N/A	N/A	N/A
2	Weld Metal	.394x.395	0.315	-20	91	N/A	N/A	N/A
3	Weld Metal	.394x.395	0.315	-20	124	N/A	N/A	N/A
4	HAZ A-36	.394x.394	0.315	-20	83	N/A	N/A	N/A
5	HAZ A-36	.394x.395	0.315	-20	105	N/A	N/A	N/A
6	HAZ A-36	.394x.395	0.315	-20	106	N/A	N/A	N/A
7	HAZ SA-516	.394x.395	0.315	-20	111	N/A	N/A	N/A
8	HAZ SA-516	.394x.395	0.315	-20	82	N/A	N/A	N/A
9	HAZ SA-516	.394x.395	0.315	-20	75	N/A	N/A	N/A

Impact testing performed to ASME VIII

HARDNESS TEST - ROCKWELL B

Base Metal				Heat Affected Zone			Weld Metal		
A-36	75 Rb	77 Rb	77 Rb	81 Rb	80 Rb	81 Rb	90 Rb	91 Rb	91 Rb
SA-516	88 Rb	77 Rb	77 Rb	93 Rb	91 Rb	90 Rb			

DEPOSITED CHEMICAL ANALYSIS

C	Si	Mn	P	S	Al	V	Cr	Ni	Fe	Ce
0.100	0.590	1.410	0.015	0.013	N/A	N/A	0.051	0.059	N/A	N/A

Chemical Analysis Conforms to A# 1

MATERIAL TRACABILITY

Item Description	A-36	Heat Number	A2K326	Manufacturer	SSAB
Item Description	SA-516-70	Heat Number	B2G551	Manufacturer	SSAB

WELDING INFORMATION

Welding machine used	(A) Lincoln 455m/STT w/ 25m Feeder box (B) Power Wave AC/DC 1000 w/ Lincoln Power Feed 10A Controller				
Welder Name	Richard Carter	ID Number	28117	Stamp	RC

TESTING INFORMATION

Tests Conducted By	MSI Testing Inc.	Laboratory Test Number	14-154	Date of Testing	6/5/2014
Preparation and welding of test coupon was witnessed by	Jacob Mowat				

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX.

This Procedure Qualification Record was prepared and accepted by Jacob Mowat on 6/9/2014

Accepted By _____ Plant 1 Denver, CO
 Accepted By _____ Plant 2 Salt Lake City, UT
 Accepted By _____ Plant 3 Pocatello, ID



Jacob Mowat
 CWI 13100541
 QC1 EXP. 10/1/2016

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

Uncontrolled copy if not signed by plant representative

EATON METAL PRODUCTS COMPANY LLC

BASE METAL (QW-403)

JOINT (QW-402, QW-405)

POST WELD HEAT TREATMENT (F) (QW-407)

PREHEAT (F) (QW-406)

FCAW

E71T-1

5.20

6

1

Outers

Lincoln Outershield 71 Elite

0.045 / 1/16"

1.5

100% CO₂ - 30-50 CFH

$$\frac{1}{2} - \frac{3}{4}$$

None

None

DCEP

SPRAY

—

STRINGER - Each bead $\leq 5/8"$ wide

MULTIPLE

1

—

1

1/2" -

NONE

ding/Bru

Chipping/Grinding

--	--	--

Interpass cleaning not considered peening
Refer to Appendix WPS for all other variables.
Non Wave From Controlled Welding.
This WPS is only used for material which does not require notch-toughness testing.
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APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 4/28/2014 Revision: 9

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supersedes this document if a conflict exists.

QW-402

- 1 Customer Representative shall accept all weld joint designs on job specific drawings.
- 2 Retainers prohibited.
- 3 Root spacing shall be sufficient to allow for complete joint penetration.
- 4 Bevel angle for groove welds that can only be accessed from one side (i.e. no backgouge/grind) shall be 30° or greater.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-407 PWHT When Required

- 1 For vessels that are exposed to environments that could cause stress corrosion cracking; a minimum hold time of 1 hour at a minimum temperature of 1150°F shall be applied.
- 2 For welds that may be exposed to environments that could cause stress corrosion cracking the minimum PWHT hold time shall be one hour per inch for thicknesses exceeding one inch

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

UG-84

For weld procedures used when impact tests are required, production material must:

- a Be of the same P-Number and Group Number with the exception allowed by QW-403.5(c)
- b Be in the same heat treated condition
- c Meet the minimum notch toughness requirements

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No P1G1-P1G2-FCAW-A20L Date 11/11/2009 Revision 1

BASE METAL (QW-403) Material Form <u>PLATE</u> Thickness* <u>0.75</u> Material Spec <u>SA-36</u> P # <u>1</u> Gr # <u>1</u> Material Spec <u>SA-516-70N</u> P # <u>1</u> Gr # <u>2</u> * Weld thickness = to plate thickness PREHEAT (F) (QW-406) Minimum Temperature <u>50</u> Maximum Interpass Temperature <u>300</u> Preheat Maintenance <u>PRIOR / DURING</u>	JOINT (QW-402, QW-405) Type <u>DOUBLE BEVEL</u> Groove Angle <u>40</u> Root Opening <u>0</u> Root Face <u>1/8</u> Backgouge <u>YES</u> Back Welded <u>YES</u> Test Position <u>3G</u> Vertical Progression <u>UPHILL</u> POST WELD HEAT TREATMENT (F) (QW-407) Temperature Range <u>-</u> Time Range <u>-</u>
--	--

PROCESS / TYPE	FCAW	-
FILLER METAL (QW-404)		
AWS Classification	E71T-1	-
SFA# / AWS Specification	5.20	-
F #	6	-
A # or Chemical Composition	1	-
Filler Metal Trade Name	-	-
Filler Metal Diameter	0.045	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	100% CO ₂ , 35CFH	-
Gas Cup Size	5/8"	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	-	-
ELECTRICAL (QW-409)		
Current	DCEP	-
GMAW, FCAW		
Transfer Mode	SPRAY	-
GTAW		
Electrode Type	-	-
Electrode Size	-	-
TECHNIQUE (QW-410)		
Beads	STRINGER	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	1/2" - 1"	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ALL	FCAW	E71T-1	0.045	DCEP	210	24	6	50,400	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = **50,400 J/in** = $\frac{\text{Amps} \times \text{Volts} \times 60}{\text{Travel Speed}}$

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No

P1G1-P1G2-FCAW-A20L

Date 11/11/2009 Revision

1

TENSILE TEST (QW-150)

SPECIMEN NO.	WIDTH (IN)	THICK (IN)	AREA (SQIN)	ULTIMATE TOTAL LOAD	ULTIMATE STRESS (PSI)	LOCATION OF FAILURE
A	0.754	0.73	0.550	38,160	69,382	BASE METAL SA-36
B	0.746	0.721	0.538	37,040	68,848	BASE METAL SA-36
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
(4) QW-462.2 SIDE BEND	PASS	-	-
-	-	-	-

TOUGHNESS TEST (QW-170)

SPECIMEN NO.	NOTCH LOCATION	NOTCH TYPE	TEST TEMP (F)	IMPACT VALUES (FT-LBS)	LATERAL EXP.		DROP WEIGHT BREAK
					SHEAR %	MILS	
1	WELD	V-NOTCH	-20	63	40	0.051	NO
2	WELD	V-NOTCH	-20	65	40	0.055	NO
3	WELD	V-NOTCH	-20	89	60	0.071	NO
4	SA-36 HAZ	V-NOTCH	-20	16	20	0.014	NO
5	SA-36 HAZ	V-NOTCH	-20	29	20	0.03	NO
6	SA-36 HAZ	V-NOTCH	-20	22	20	0.026	NO
7	SA-516-70	V-NOTCH	-20	18	20	0.017	NO
8	SA-516-70	V-NOTCH	-20	22	20	0.023	NO
9	SA-516-70	V-NOTCH	-20	18	20	0.018	NO
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-

HARDNESS TEST - Brinell BHN

BASE METAL				HEAT AFFECTED ZONE			WELD METAL		
	1	2	3	1	2	3	1	2	3
SA-36	130	127	-	172	159	-	190	165	-
SA-516-70	162	162	-	200	180	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

N1: Interpass cleaning not considered peening.

N2: Refer to Appendix PQR for all other variables.

N3:

N4:

N5: Original PQR "CS-129-DS, 5-5-95"

Welder Name: V. NGUYEN

Stamp: W ID Number: 218

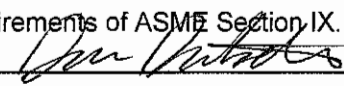
Tests Conducted By: CMS, EMP

Laboratory Test Number: C-45-259

PQR was done and welding of coupon was witnessed by:

EATON METAL PRODUCTS COMPANY

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY 



Daniel Durtschi

CWI 11030421

QC1 EXP. 3/1/2014

PLANT 1 DENVER, CO

ACCEPTED BY

ACCEPTED BY

PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY

PLANT 3 POCATELLO, ID

Page 2 of 2

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APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimins used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P1-GMAWP-AL Date 11/17/2011 Revision 5
 Supporting PQR No(s) P1G1-P1G2-GMAWP-L59-A50L, P1G1-P1G2-GMAWP-L59-A50U

BASE METAL (QW-403)		JOINT (QW-402, QW-405)	
P # <u>1</u>	Gr # <u>-</u> to P # <u>1</u> Gr # <u>-</u>	Groove <u>ALL</u>	Fillet <u>ANY / ALL</u>
Thickness Range <u>3/16</u>	to <u>1 1/2</u>	Position <u>ANY</u>	Fillet Weld Size <u>ALL</u>
Backing <u>YES</u>	Backing Material <u>WELD / BASE METAL</u>	Progression <u>UPHILL</u>	
POST WELD HEAT TREATMENT (F) (QW-407)		PREHEAT (F) (QW-406)	
Temperature Range <u>None</u>		Minimum Temperature <u>50<1.25" - 200>1.25"</u>	
Time Range <u>None</u>		Maximum Interpass Temperature <u>450</u>	
		Preheat Maintenance <u>PRIOR / DURING</u>	

PROCESS / TYPE	GMAW-P	-
FILLER METAL (QW-404)		
AWS Classification	ER70S-6	-
SFA# / AWS Specification	ASME SFA-5.18	-
F #	6	-
A # or Chemical Composition	1	-
Filler Metal Trade Name	LINCOLN SUPERARC L-59	-
Filler Metal Diameter	0.045" / 0.052"	-
Maximum Weld Metal Thickness	1.5"	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	90% Ar 10%CO2 / 35min	-
Gas Cup Size	1/2" - 3/4"	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	-	-
ELECTRICAL (QW-410)		
Current	DCEP	-
GMAW, FCAW		
Transfer Mode	PULSED SPRAY	-
GTAW		
Electrode Type	-	-
Electrode Size	-	-
TECHNIQUE (QW-410)		
Beads	STRINGER - Each bead ≤ 5/8" wide	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	1/2 - 3/4"	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-



Daniel Durtschi
 CWI 11030421
 QC1 EXP 3/1/2014

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Maximum Heat Input for any Diameter = J/in
ANY	GMAW-P	ER70S-6	0.045"	DCEP	Any	Any	Any	-	By <i>Daniel Durtschi</i>
ANY	GMAW-P	ER70S-6	0.052"	DCEP	Any	Any	Any	-	Accepted By PLANT 1 DEN
-	-	-	-	-	-	-	-	-	
-	-	-	-	-	-	-	-	-	
-	-	-	-	-	-	-	-	-	Accepted By PLANT 2 SLC

Interpass cleaning not considered peening.

Refer to Appendix WPS for all other variables.

This WPS is only used for material that does not require notch-toughness testing
 Lincoln Invertec V350 PRO, Pulsed MIG Steel 0.045, 237 SPD, 180 WFS -3.0 arc control

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Accepted By PLANT 3 POC

APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 11/10/2011 Revision: 5

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.
- 3 Root spacing shall be sufficient to allow for complete joint penetration.
- 4 Bevel angle for groove welds shall be 30° or greater.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-407 PWHT When Required

- 1 For vessels that are exposed to environments that could cause stress corrosion cracking; a minimum hold time of 1 hour at a minimum temperature of 1150°F shall be applied.

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

UG-84

For weld procedures used when impact tests are required, production material must:

- a Be of the same P-Number and Group Number with the exception allowed by QW-403.5(c)
- b Be in the same heat treated condition
- c Meet the minimum notch toughness requirements

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P1G1-P1G2-GMAWP-L59-A50L Date 4/12/2011 Revision 0

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PLATE	Thickness*	3/8	Type	SINGLE V	Groove Angle	50
Material Spec	SA-516-70	P #	1	Gr #	2	Root Opening	0
Material Spec	SA-36	P #	1	Gr #	1	Root Face	1/16
*Weld thickness = to plate thickness				Backgouge	YES	Back Welded	YES
PREHEAT (F) (QW-406)				Test Position	3G	Vertical Progression	UPHILL
Minimum Temperature	50° F			80° INCLINATION ANGLE			
Maximum Interpass Temperature	450° F			POST WELD HEAT TREATMENT (F) (QW-407)			
Preheat Maintenance	NONE			Temperature Range	None		
				Time Range	None		

PROCESS / TYPE	GMAW-P	-
FILLER METAL (QW-404)		
AWS Classification	ER70S-6	-
SFA# / AWS Specification	ASME SFA-5.18	-
F #	6	-
A # or Chemical Composition	1	-
Filler Metal Trade Name	LINCOLN SUPERARC L-59	-
Filler Metal Diameter	0.045"	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	90% Ar 10%CO2 / 35min	-
Gas Cup Size	5/8"	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	-	-
ELECTRICAL (QW-409)		
Current	DCEP	-
GMAW, FCAW		
Transfer Mode	PULSED SPRAY	-
GTAW		
Electrode Type	-	-
Electrode Size	-	-
TECHNIQUE (QW-410)		
Beads	STRINGER	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	1/2-3/4	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ROOT	GMAWP	ER70S-6	.045	DCEP	150	18.5	8	20,813	-
FILL/COVER	GMAWP	ER70S-6	.045	DCEP	170	20.5	6.5	32,169	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = 32,169 J/in = $\frac{\text{Amps} \times \text{Volts} \times 60}{\text{Travel Speed}}$

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No. _____ P1G1-P1G2-GMAWP-L59-A50L Date 4/12/2011 Revision 0

TENSILE TEST (QW-150)

SPECIMEN NO.	WIDTH (IN)	THICK (IN)	AREA (SQIN)	ULTIMATE TOTAL LOAD	ULTIMATE STRESS (PSI)	FAILURE LOCATION
1	0.753	0.352	0.2651	18,988	71,638	BASE METAL SA36
2	0.751	0.342	0.2568	18,961	73,824	BASE METAL SA36
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
(4) SIDE BEND, QW-462.2	ALL PASS	-	-
-	-	-	-

TOUGHNESS TEST (QW-170)

SPECIMEN NO.	NOTCH LOCATION	NOTCH TYPE	TEST TEMP (F)	IMPACT VALUES (FT-LBS)	LATERAL EXP.		DROP WEIGHT BREAK
					SHEAR %	MILS	
WELD 1	WELD	V-NOTCH	-55°	35	-	-	-
WELD 2	WELD	V-NOTCH	-55°	30	-	-	-
WELD 3	WELD	V-NOTCH	-55°	45	-	-	-
HAZ 36-1	HAZ	V-NOTCH	-55°	50	-	-	-
HAZ 36-2	HAZ	V-NOTCH	-55°	58	-	-	-
HAZ 36-3	HAZ	V-NOTCH	-55°	44	-	-	-
HAZ 516-1	HAZ	V-NOTCH	-55°	120	-	-	-
HAZ 516-2	HAZ	V-NOTCH	-55°	106	-	-	-
HAZ 516-3	HAZ	V-NOTCH	-55°	110	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-

HARDNESS TEST - Rockwell Hardness, B Scale

BASE METAL				HEAT AFFECTED ZONE			WELD METAL		
	1	2	3	1	2	3	1	2	3
SA516-70	80.5	82.0	82.9	90.0	88.0	87.0	86.0	87.5	86.0
SA36	80.0	80.0	79.5	83.0	81.0	80.0	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

N1: Interpass cleaning not considered peening.

N2: Refer to Appendix PQR for all other variables.

N3:

N4: Lincoln Invertec V350Pro: Pulsed MIG Steel 0.045, SPD=237, WFS=180

N5: Test Plate: SA516-70, Nucor Heat# 9106648; SA36, SSAB Heat# A0J024

Welder Name: Daniel Durtschi Stamp: DD ID Number: 1240
 Tests Conducted By: MSI Testing, Inc. Laboratory Test Number: 11-089 #1
 PQR was done and welding of coupon was witnessed by: Eaton Metal Products Company LLC

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY

[Signature]



Daniel Durtschi
 CWI 11030421
 QC1 EXP. 3/1/2014
 PLANT 1 DENVER, CO

ACCEPTED BY

ACCEPTED BY

ACCEPTED BY

PLANT 2 SALT LAKE CITY, UT

PLANT 3 POCATELLO, ID

APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimins used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P1G1-P1G2-GMAWP-L59-A50U Date 4/12/2011 Revision 0

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PLATE	Thickness*	3/4	Type	SINGLE V	Groove Angle	50
Material Spec	SA-516-70	P #	1	Gr #	2	Root Opening	0
Material Spec	SA-36	P #	1	Gr #	1	Root Face	1/16
*Weld thickness = to plate thickness				Backgouge	YES	Back Welded	YES
PREHEAT (F) (QW-406)				Test Position	3G	Vertical Progression	UPHILL
Minimum Temperature	50° F			60° INCLINATION ANGLE			
Maximum Interpass Temperature	450° F			POST WELD HEAT TREATMENT (F) (QW-407)			
Preheat Maintenance	NONE			Temperature Range	None		
				Time Range	None		

PROCESS / TYPE	GMAW-P	-
FILLER METAL (QW-404)		
AWS Classification	ER70S-6	-
SFA# / AWS Specification	ASME SFA-5.18	-
F #	6	-
A # or Chemical Composition	1	-
Filler Metal Trade Name	LINCOLN SUPERARC L-59	-
Filler Metal Diameter	0.045"	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	90% Ar 10%CO2 / 35min	-
Gas Cup Size	5/8	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	-	-
ELECTRICAL (QW-409)		
Current	DCEP	-
GMAW, FCAW		
Transfer Mode	PULSED SPRAY	-
GTAW		
Electrode Type	-	-
Electrode Size	-	-
TECHNIQUE (QW-410)		
Beads	STRINGER	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	1/2-3/4	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ROOT	GMAWP	ER70S-6	.045	DCEP	150	18.5	8	20,813	-
FILL	GMAWP	ER70S-6	.045	DCEP	170	20.5	6.5	32,169	-
COVER-	GMAWP	ER70S-6	.045	DCEP	150	18.5	8	20,813	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = **32,169 J/in** = Amps x Volts x 60
Travel Speed

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No. _____ P1G1-P1G2-GMAWP-L59-A50U Date 4/12/2011 Revision 0

TENSILE TEST (QW-150)

SPECIMEN NO.	WIDTH (IN)	THICK (IN)	AREA (SQIN)	ULTIMATE TOTAL LOAD	ULTIMATE STRESS (PSI)	FAILURE LOCATION
1	0.75	0.716	0.5370	40,496	75,412	BASE METAL SA36
2	0.752	0.72	0.5414	40,534	74,863	BASE METAL SA36
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
(4) SIDE BEND, QW-462.2	ALL PASS	-	-
-	-	-	-

TOUGHNESS TEST (QW-170)

SPECIMEN NO.	NOTCH LOCATION	NOTCH TYPE	TEST TEMP (F)	IMPACT VALUES (FT-LBS)	LATERAL EXP.		DROP WEIGHT BREAK
					SHEAR %	MILS	
WELD 1	WELD	V-NOTCH	-50°	94	-	-	-
WELD 2	WELD	V-NOTCH	-50°	82	-	-	-
WELD 3	WELD	V-NOTCH	-50°	90	-	-	-
HAZ 36-1	HAZ	V-NOTCH	-50°	20	-	-	-
HAZ 36-2	HAZ	V-NOTCH	-50°	60	-	-	-
HAZ 36-3	HAZ	V-NOTCH	-50°	98	-	-	-
HAZ 516-1	HAZ	V-NOTCH	-50°	180	-	-	-
HAZ 516-2	HAZ	V-NOTCH	-50°	146	-	-	-
HAZ 516-3	HAZ	V-NOTCH	-50°	140	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-

HARDNESS TEST - Rockwell Hardness, B Scale

	BASE METAL			HEAT AFFECTED ZONE			WELD METAL		
	1	2	3	1	2	3	1	2	3
SA516-70	82.0	82.0	80.5	90.0	89.0	91.0	91.0	92.0	94.5
SA36	80.5	80.5	81.0	94.5	94.0	95.0	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

- N1: Interpass cleaning not considered peening.
 N2: Refer to Appendix PQR for all other variables.
 N3:
 N4: Lincoln Invertec V350Pro: Pulsed MIG Steel 0.045, SPD=237, WFS=180
 N5: Test Plate: SA516-70, Ipsco Heat# B7L791 SA36, EVRAZ Heat# NT7695

Welder Name: Daniel Durtschi Stamp: DD ID Number: 1240
 Tests Conducted By: MSI Testing, Inc. Laboratory Test Number: 11-089 #2
 PQR was done and welding of coupon was witnessed by: Eaton Metal Products Company LLC

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY

[Signature]



Daniel Durtschi
 CWI 11030421
 QCT EXP. 3/1/2014

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimins used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

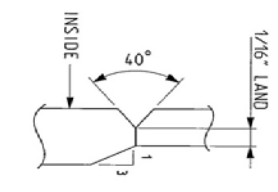
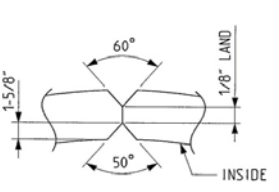
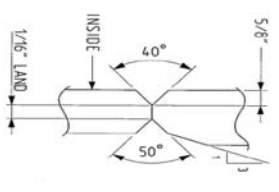
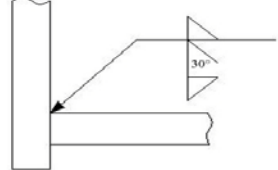
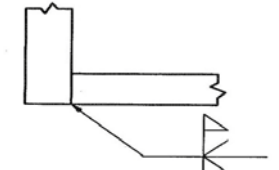
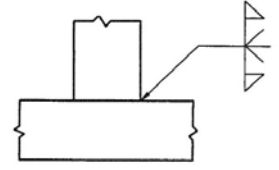
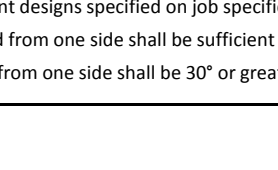
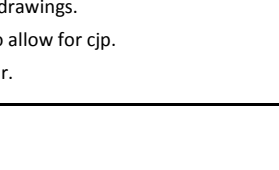
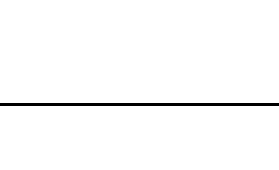
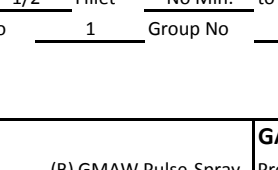
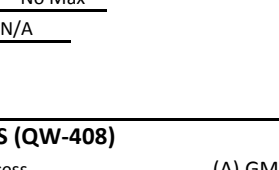
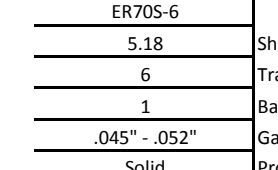
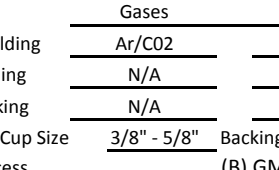
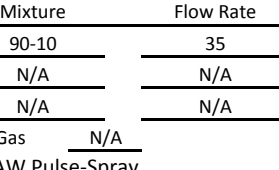
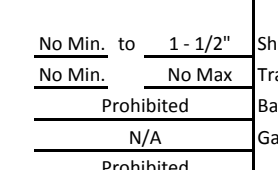
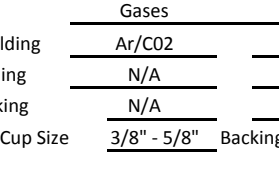
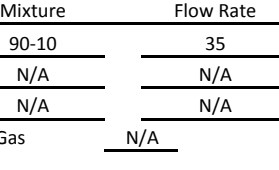
ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P1-GMAWP-STT-A Revision 1 Date 5/17/2017
 Supporting PQR No P1G1-P1G2-GMAWP-STT-A50U-1
 Welding Process GMAW Type Semi-Automatic
 Impact Qualified WPS No to N/A at N/A

JOINTS (QW-402)		Typical		
Joint Design	All			
Groove Type	Any			
Root Spacing	0 - 3/8"			
Fillet	Any			
Root Face	0 - 1/8"			
Backing	None			
Backing Type	N/A			
Groove Angle	See Typical Joint Details			
Back gouge	When Applicable (Carbon Arc/Grind)			
Retainers	None			
Notes That Apply	1,2,3			

Note 1: Customer representative shall accept all weld joint designs specified on job specific drawings.

Note 2: Root spacing for grooves that will only be welded from one side shall be sufficient to allow for cjp.

Note 3: Bevel angle for grooves that will only be welded from one side shall be 30° or greater.

BASE METALS (QW-403)

Thickness Qualified 3/4"
 Thickness Range: Groove 3/16" to 1 - 1/2" Fillet No Min. to No Max
 P-No 1 Group No N/A to P-No 1 Group No N/A
 Maximum Pass Thickness 3/16"
 Heat Treated Condition N/A

FILLER METALS (QW-404)

	(A) GMAW STT Short Arc	(B) GMAW Pulse-Spray
Process	ER70S-6	ER70S-6
AWS Classification	5.18	5.18
SFA #/Specification	6	6
F-No	1	1
A-No	.045" - .052"	.045" - .052"
Filler Metal Diameter	Solid	Solid
Thickness Range:		
Groove	No Min. to 3/16"	No Min. to 1 - 1/2"
Fillet	N/A to N/A	No Min. No Max
Supplemental Filler	Prohibited	Prohibited
Alloy Elements	N/A	N/A
Consumable Inserts	Prohibited	Prohibited

GAS (QW-408)

	(A) GMAW STT Short Arc	
	Gases	Mixture
Process	Ar/C02	90-10
Shielding	N/A	N/A
Trailing	N/A	N/A
Backing	N/A	N/A
Gas Cup Size	3/8" - 5/8"	Backing Gas N/A
Process	(B) GMAW Pulse-Spray	
	Gases	Mixture
Shielding	Ar/C02	90-10
Trailing	N/A	N/A
Backing	N/A	N/A
Gas Cup Size	3/8" - 5/8"	Backing Gas N/A

PREHEAT (QW-406)

Minimum Preheat Temp 150°F
 Maximum Interpass Temp 450°F
 Preheat Maintenance Maintain until welding is complete
 Other

POSITIONS (QW-405)

Position(s) of Groove All
 Welding Progression (A) Root pass Downhill (B) Fill and Cap Uphill
 Position(s) of Fillet All
 Other

WPS No P1-P1-GMAWP-STT-A Revision 1 Date 5/17/2017
 Supporting PQR No P1G1-P1G2-GMAWP-STT-A50U-1

POST WELD HEAT TREATMENT (QW-407)

Temperature Range _____ None _____
 Time at Temperature Range _____ N/A _____

TECHNIQUE (QW-410)**(A) GMAW STT Short Arc****(B) GMAW Pulse-Spray**

String or Weave Bead	String	String or Weave
Maximum Pass Width	5/16"	9/16"
Initial Cleaning	Brushing and/or Grinding	Brushing and/or Grinding
Interpass Cleaning	Brushing/Chipping	Brushing/Chipping
Multiple or Single Pass (Per Side)	Single	Multiple
Multiple or Single Electrodes	Single	Single
Contact Tube to Work Distance	1/4" - 1/2"	3/8" - 5/8"
Electrode Spacing (2 Arcs)	N/A	N/A
Angle of Electrode (SAW)	N/A	N/A
Peening	Prohibited	Prohibited

ELECTRICAL (QW-409)**Waveform Controlled Welding****FLAT**

Weld Pass(es)	Process and Transfer Mode	Filler Metal		Current Type and	Amps	Volts	Travel Speed	Input (MAX)
		Class	Diameter					
Root	GMAW Pulse-Short	ER70S-6	.045" - .052"	DCEP	120 - 160	12.5 - 14	9 - 14	15,083 J/In
Fill	GMAW Pulse-Spray	ER70S-6	.045" - .052"	DCEP	160 - 220	20 - 22	9 - 18	46,682 J/In
Cap	GMAW Pulse-Spray	ER70S-6	.045" - .052"	DCEP	160 - 200	21 - 22	8 - 18	46,682 J/In

OUT OF POSITION

Weld Pass(es)	Process and Transfer Mode	Filler Metal		Current Type and	Amps	Volts	Travel Speed	Input (MAX)
		Class	Diameter					
Root	GMAW Pulse-Short	ER70S-6	.045" - .052"	DCEP	120 - 160	12.5 - 14	9 - 14	15,083 J/In
Fill	GMAW Pulse-Spray	ER70S-6	.045" - .052"	DCEP	130 - 160	18 - 21.5	6 - 10	46,682 J/In
Cap	GMAW Pulse-Spray	ER70S-6	.045" - .052"	DCEP	120 - 150	18 - 21.5	5 - 12	46,682 J/In

Welding machine Lincoln V350 Pro and DC-600 use amps, volts, and travel speed to calculate heat input. $\text{Amps} \times \text{Volts} \times 60 \div \text{Travel Speed} = \text{Heat Input}$

Welding machines Lincoln 355 and 455 use instantaneous energy readout to calculate heat input. $\text{Total Joules} \div \text{Bead Length} = \text{Energy}$

This Weld Procedure Specification was prepared and accepted by _____



on 5/17/17

Accepted By _____ Plant 1 Denver, CO

Accepted By _____ Plant 2 Salt Lake City, UT

Accepted By _____ Plant 3 Pocatello, ID

All units referenced on WPS are in English (Standard, e.g. psi, inches, etc.) unless specifically noted.

Uncontrolled copy if not signed by plant representative

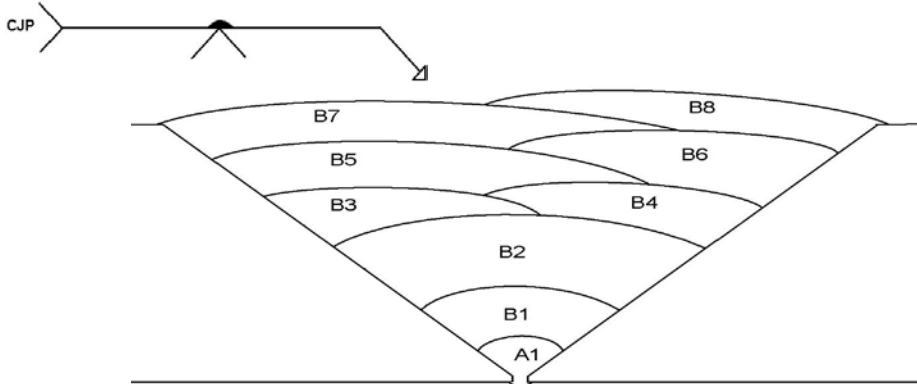
PROCEDURE QUALIFICATION RECORD (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

PQR No. P1G1-P1G2-GMAWP-STT-A50U-1 Date of Welding 5/12/2014
Weld Process(es) GMAW - GMAWP Type(s) Semi-Automatic

JOINT DETAILS (QW-402)

Joint Design Butt Joint
Groove Type Single V Groove
Root Spacing 3/32"
Root Face 1/32"
Backing None
Backing Type N/A
Groove Angle 70°
Back gouged No
Retainers None



POSITION (QW-405)

Test Position 3G
Progression Root:Downhill Fill/Cap:Uhill

BASE METALS (QW-403)

Material Spec (1) A36 to (2) SA-516-70 P-No 1 Gr# 1 to P-No 1 Gr# 2
Type/Grade, or UNS Number N/A to N/A Heat Treated Condition Hot Rolled
Material Thickness (T) 3/4" Diameter of Test Coupon N/A

FILLER METALS (QW-404)

	(A)	(B)
SFA Specification	5.18	5.18
AWS Classification	ER70S-6	ER70S-6
F-No	6	6
A-No	1	1
Filler Metal Trade Name	Lincoln Super Arc L-59	Lincoln Super Arc L-59
Filler Metal Product Form	Solid	Solid
Supplemental Filler Metal	None	None
Electrode Flux Class	N/A	N/A
Flux Trade Name	N/A	N/A
Flux Type	N/A	N/A
Recrushed Slag Used	N/A	N/A
Weld Metal Thickness (t)	3/16"	9/16"
Maximum Pass Thickness	3/16"	3/16"

ELECTRODE

Tungsten Type/Size	N/A	N/A
Consumable Insert Used	N/A	N/A
Electrode Spacing (2 Arcs)	N/A	N/A
Angle	5° Drag	5° Push
Contact Tube to Work	3/8"	3/8"

GAS (QW-408)

	Gases	Mixture (%)	Flow Rate (cfh)
Shielding	Ar/CO2	90-10	35
Trailing	N/A	N/A	N/A
Backing	N/A	N/A	N/A
Gas Cup Size	1/2"		

PREHEAT (QW-406)

Minimum Temperature 150° F
Preheat Maintenance Prior During

TECHNIQUE (QW-410)

Multipass or Single Pass (per side) Multiple
Single or Multiple Electrodes Single
Initial and Interpass Cleaning Brushing/Grinding
Peening Performed No
Maximum Pass Width 9/16"
Oscillation (Machine) N/A
In Chamber Welding (GTAW) N/A

POST WELD HEAT TREATMENT (QW-407)

Temperature None
Time N/A
Other N/A

ELECTRICAL (QW-409)

Pass(es)	Process	Transfer Mode	Class	Diameter	Current & Polarity	Amps	Volts	Travel Speed (ipm)	Heat Input (J/in)	String or Weave	Interpass Temp (°F)
A1	GMAW	Pulse-Short	ER70S-6	.052"	DCEP	162	13.5	8.7	15,083	String	Preheat
B1	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	140	21.2	5.9	30,183	Weave	180°
B2	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	145	22	4.1	46,682	Weave	225°
B3	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	163	21.5	5.9	29,735	Weave	250°
B4	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	138	21.1	5.1	34,256	Weave	322°
B5	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	148	21.8	5.2	37,227	Weave	330°
B6	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	145	21.6	5.1	36,847	Weave	362°
B7	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	140	21.6	4.2	43,200	Weave	Preheat
B8	GMAW	Pulse-Spray	ER70S-6	.052"	DCEP	145	21.8	4.8	39,512	Weave	260°

Heat input calculated using QW-409.1 (a) Voltage X Amperage X 60 / by Travel Speed

TENSILE TESTS (QW-150)

Specimen No	Width (in)	Thickness (in)	Diameter (in)	Area (in)	Ultimate Total Load (lbs)	Ultimate Stress (psi)	Location of Failure
1	0.745	0.738		0.5498	40,022	72,793	Base Metal
2	0.749	0.742		0.5580	41,168	74,069	Base Metal

GUIDED-BEND TESTS (QW-160)

Type and Figure No	Result	Type and Figure No	Result
QW 462.2	Pass	QW 462.2	Pass
QW 462.2	Pass	QW 462.2	Pass

TOUGHNESS TESTS (QW-170)

Specimen No	Notch Location	Specimen Size (in)	Notch Size (in)	Test Temp (F)	Impact Values (Ft LBS)	Shear %	Mils	Drop Weight Break
Top 1	Weld Metal	.395 x .395	0.315	-50°	73	N/A	N/A	N/A
Top 2	Weld Metal	.394 x .395	0.314	-50°	43	N/A	N/A	N/A
Top 3	Weld Metal	.394 x .395	0.315	-50°	53	N/A	N/A	N/A
Bottom 1	Weld Metal	.395 x .395	0.315	-50°	65	N/A	N/A	N/A
Bottom 2	Weld Metal	.395 x .395	0.315	-50°	40	N/A	N/A	N/A
Bottom 3	Weld Metal	.394 x .395	0.314	-50°	63	N/A	N/A	N/A
HAZ 1	A36	.395 x .395	0.315	-50°	28	N/A	N/A	N/A
HAZ 2	A36	.394 x .395	0.315	-50°	27	N/A	N/A	N/A
HAZ 3	A36	.395 x .395	0.315	-50°	29	N/A	N/A	N/A
HAZ 1	SA-516-70	.395 x .394	0.315	-50°	31	N/A	N/A	N/A
HAZ 2	SA-516-70	.395 x .395	0.315	-50°	32	N/A	N/A	N/A
HAZ 3	SA-516-70	.395 x .395	0.314	-50°	28	N/A	N/A	N/A

Impact testing performed to ASME VIII

DEPOSITED CHEMICAL ANALYSIS

C	Si	Mn	P	S	Al	V	Cr	Ni	Fe	Ce
0.082	0.860	1.320	<.010	0.016	N/A	N/A	0.044	0.031	Rem	N/A

Chemical Analysis Conforms to A# 1

MATERIAL TRACABILITY

Item Description	<u>A36</u>	Heat Number	<u>E3J357</u>	Manufacturer	<u>SSAB</u>
Item Description	<u>SA-516-70</u>	Heat Number	<u>516998</u>	Manufacturer	<u>JSW</u>

WELDING INFORMATION

Welding machine used	Lincoln 455 STT W/ 25 M Feeder				
Welder Name	Clair Neff	ID Number	28005	Stamp	CN

TESTING INFORMATION

Tests Conducted By	<u>MSI Testing Inc.</u>	Laboratory Test Number	<u>14-136</u>	Date of Testing	<u>5/21/2014</u>
Preparation and welding of test coupon was witnessed by	<u>Jacob Mowat</u>				

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX.

Jacob Mowat

This Procedure Qualification Record was prepared and accepted by _____ on 5/22/2014

Accepted By _____ Plant 1 Denver, CO
 Accepted By _____ Plant 2 Salt Lake City, UT
 Accepted By _____ Plant 3 Pocatello, ID

All units referenced on PQR are in English (Standard, I.e. psi, inches, etc.) unless specifically noted.

Uncontrolled copy if not signed by plant representative



Jacob Mowat
 CWI 13100541
 QC1 EXP. 10/1/2016

WELDING PROCEDURE SPECIFICATION (ASME)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P1-GTAW-AL Date 12/17/2009 Revision 2Supporting PQR No(s) P1G1-P1G2-GTAW-A50L**BASE METAL (QW-403)**P # 1 Gr # - to P # 1 Gr # -
Thickness Range 1/16 to 0.56
Backing NO Backing Material -**JOINT (QW-402, QW-405)**Groove ANY Fillet ANY
Progression UPHILL Fillet Weld Size ANY**POST WELD HEAT TREATMENT (F) (QW-407)**Temperature Range -
Time Range -**PREHEAT (F) (QW-406)**Minimum Temperature 50
Maximum Interpass Temperature 500
Preheat Maintenance PRIOR / DURING**PROCESS / TYPE****GTAW****FILLER METAL (QW-404)**AWS Classification ER70S-6
SFA# / AWS Specification 5.18
F # 6
A # or Chemical Composition 1
Filler Metal Trade Name LINCOLN ER70S-6
Filler Metal Diameter 3/32
Maximum Weld Metal Thickness 0.56**SHIELDING (QW-408)**Electrode-Flux (Class) -
Flux Trade Name / Type -
Shielding Gas / CFH 100% ARGON - 30-60CFH
Gas Cup Size ANY
Trailing Gas / CFH -
Backing Gas / CFH -**ELECTRICAL (QW-410)**Current DCEN**GMAW, FCAW**Transfer Mode -**GTAW**Electrode Type EWL a-1.5, 1.5% Lanthana (GOLD)
Electrode Size 3/32**TECHNIQUE (QW-410)**Beads WEAVE
Pass MULTIPLE
Number of Electrodes 1**ELECTRODE SPACING**Longitudinal -
Angle -
Contact Tube to Work Distance -
Peening NONE
Interpass Cleaning MANUAL / MECHANICAL

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)
ANY	GTAW	ER70S-6	3/32	DCEN	150max	15max	1min	-
-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-

Maximum Heat Input for any Diameter =	150 J/in
By	JASON J. HART 02030171
Accepted By PLANT 1 DEN	CWI
Accepted By PLANT 2 SLC	
Accepted By PLANT 3 POC	

Interpass cleaning not considered peening.

Refer to Appendix WPS for all other variables.

This WPS is only used for material which does not require notch-toughness testing.

APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 4

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

Uncontrolled copy if actual signature not signed by plant representative.

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P1G1-P1G2-GTAW-A50L Date 12/16/2009 Revision 1

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PIPE	Thickness*	0.28	Type	SINGLE BEVEL	Groove Angle	60
Material Spec	SA-106B	P #	1	Gr #	1	Root Opening	1/8
Material Spec	SA-106C	P #	1	Gr #	2	Root Face	1/16
* Weld thickness = to pipe thickness				Backgouge	NO	Back Welded	NO
PREHEAT (F) (QW-406)				Test Position	5G	Verticle Progression	UPHILL
Minimum Temperature	50			POST WELD HEAT TREATMENT (F) (QW-407)			
Maximum Interpass Temperature	500			Temperature Range	-		
Preheat Maintenance	PRIOR / DURING			Time Range	-		

PROCESS / TYPE	GTAW	-
FILLER METAL (QW-404)		
AWS Classification	ER70S-6	-
SFA# / AWS Specification	5.18	-
F #	6	-
A # or Chemical Composition	1	-
Filler Metal Trade Name	LINCOLN ER70S-6	-
Filler Metal Diameter	3/32	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	100% ARGON - 45 CFH	-
Gas Cup Size	5	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	-	-
ELECTRICAL (QW-409)		
Current	DCEN	-
GMAW, FCAW		
Transfer Mode	-	-
GTAW		
Electrode Type	EWTh-2, 2% THORIA	-
Electrode Size	3/32	-
TECHNIQUE (QW-410)		
Beads	WEAVE	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	-	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ANY	GTAW	ER70S-6	3/32	DCEN	110-150	10-15	1-3	135,000	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = 135,000 J/in = $\frac{\text{Amps} \times \text{Volts} \times 60}{\text{Travel Speed}}$

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No

P1G1-P1G2-GTAW-A50L

Date 12/16/2009 Revision

1

TENSILE TEST (QW-150)

SPECIMEN NO.	WIDTH (IN)	THICK (IN)	AREA (SQIN)	ULTIMATE TOTAL LOAD	ULTIMATE STRESS (PSI)	LOCATION OF FAILURE
1	0.744	0.214	0.159	12,823	80,648	BASE METAL
2	0.748	0.211	0.158	12,670	80,190	BASE METAL
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
(2) QW-462.3a FACE BEND	PASS	(2) QW-462.3a ROOT BEND	PASS
-	-	-	-
-	-	-	-

TOUGHNESS TEST (QW-170)

SPECIMEN NO.	NOTCH LOCATION	NOTCH TYPE	TEST TEMP (F)	IMPACT VALUES (FT-LBS)	LATERAL EXP.		DROP WEIGHT BREAK
					SHEAR %	MILS	
WELD 1	WELD METAL	V-NOTCH	-50	13 (26)	-	-	NO
WELD 2	WELD METAL	V-NOTCH	-50	10 (20)	-	-	NO
WELD 3	WELD METAL	V-NOTCH	-50	18 (36)	-	-	NO
HAZ 1	HAZ	V-NOTCH	-50	33 (66)	-	-	NO
HAZ 2	HAZ	V-NOTCH	-50	36 (72)	-	-	NO
HAZ 3	HAZ	V-NOTCH	-50	29 (58)	-	-	NO
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-

HARDNESS TEST - Rockwell B Hardness

HARDNESS TEST - Rockwell B Hardness									
BASE METAL				HEAT AFFECTED ZONE			WELD METAL		
	1	2	3	1	2	3	1	2	3
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

N1: Interpass cleaning not considered peening.

N2: Refer to Appendix PQR for all other variables.

N3:

N4:

N5:

N6: Impact specimens: 1/2 size "Actual Values (Full Size Conversion)"

N7: Pipe Test: USS Heat# X84474 Dual Certified SA-106 B/C

Welder Name: CLAIR NEFF

Stamp: C

ID Number: 8005

Tests Conducted By: MSI TESTING, INC.

Laboratory Test Number: 05-078

PQR was done and welding of coupon was witnessed by:

EATON METAL PRODUCTS COMPANY LLC

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY

[Signature]



Daniel Durtschi

CWI 11030421

QC1 EXP. 3/1/2014

ACCEPTED BY

PLANT 1 DENVER, CO

ACCEPTED BY

PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY

PLANT 3 POCATELLO, ID

APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimins used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P8-FCAW-AL Date 11/12/2009 Revision 1Supporting PQR No(s) P1-P8-FCAW-AL**BASE METAL (QW-403)**P # 8 Gr # - to P # 1 Gr # -
Thickness Range 0.1875 to 2.5
Backing YES Backing Material WELD/BASE METAL**JOINT (QW-402, QW-405)**Groove ALL Fillet ALL
Progression UPHILL Fillet Weld Size ANY**POST WELD HEAT TREATMENT (F) (QW-407)**Temperature Range -
Time Range -**PREHEAT (F) (QW-406)**Minimum Temperature 50
Maximum Interpass Temperature 350
Preheat Maintenance -**PROCESS / TYPE****FCAW****FILLER METAL (QW-404)**AWS Classification E309LT-1
SFA# / AWS Specification 5.22
F # 6
A # or Chemical Composition 8
Filler Metal Trade Name -
Filler Metal Diameter 0.045
Maximum Weld Metal Thickness 2.5**SHIELDING (QW-408)**Electrode-Flux (Class) -
Flux Trade Name / Type -
Shielding Gas / CFH 100% CO2 - 35CFH
Gas Cup Size 1/2 - 3/4
Trailing Gas / CFH -
Backing Gas / CFH -**ELECTRICAL (QW-410)**Current DCEP**GMAW, FCAW**Transfer Mode SPRAY**GTAW**Electrode Type -
Electrode Size -**TECHNIQUE (QW-410)**Beads STRINGER - Each bead ≤ 5/8" wide
Pass MULTIPLE
Number of Electrodes 1**ELECTRODE SPACING**Longitudinal -
Angle -
Contact Tube to Work Distance 3/4 - 1 1/4
Peening NONE
Interpass Cleaning MANUAL / MECHANICAL

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)
ANY	FCAW	E309LT-1	0.045	DCEP	125-220	24-29	8-16	-
-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-

Maximum Heat Input for any Diameter = <u>100 J/in</u>
By <u>JASON J. HART</u>
<u>02030171</u>
Accepted By PLANT 1 <u>CDEN</u>
Accepted By PLANT 2 SLC
Accepted By PLANT 3 POC

Interpass cleaning not considered peening.

Refer to Appendix WPS for all other variables.

This WPS is only used for material which does not require notch-toughness testing.

Uncontrolled copy if actual signature not signed by plant representative.

APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 4

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No. _____ P1-P8-FCAW-AL Date 11/12/2009 Revision 1

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PLATE	Thickness*	1.25	Type	GROOVE	Groove Angle	60
Material Spec	SA240-304	P #	8	Gr #	1	Root Opening	-
Material Spec	SA516-70	P #	1	Gr #	2	Root Face	1/16
* Weld thickness = to plate thickness				Backgouge	YES	Back Welded	YES
				Test Position	1G	Vertical Progression	-
PREHEAT (F) (QW-406)				POST WELD HEAT TREATMENT (F) (QW-407)			
Minimum Temperature		50		Temperature Range		-	
Maximum Interpass Temperature		350		Time Range		-	
Preheat Maintenance		PRIOR / DURING					

PROCESS / TYPE	FCAW	
FILLER METAL (QW-404)		
AWS Classification	E309LT-1	-
SFA# / AWS Specification	5.22	-
F #	6	-
A # or Chemical Composition	8	-
Filler Metal Trade Name	-	-
Filler Metal Diameter	0.045	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	100% CO2 - 35CFH	-
Gas Cup Size	3/4	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	-	-
ELECTRICAL (QW-409)		
Current	DCEP	-
GMAW, FCAW		
Transfer Mode	SPRAY	-
GTAW		
Electrode Type	-	-
Electrode Size	-	-
TECHNIQUE (QW-410)		
Beads	STRINGER	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	3/4 - 1 1/4	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ALL	FCAW	E309LT-1	0.045	DCEP	150	27	12-20	20,250	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = 20,250 J/in = Amps x Volts x 60 / Travel Speed

EATON METAL PRODUCTS COMPANY LLC

PQR No P1-P8-FCAW-AL Date 11/12/2009 Revision 1

TENSILE TEST (QW-150)

[illegible]

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
QW-462.2 SIDE BEND	PASS	QW-462.2 SIDE BEND	PASS
QW-462.2 SIDE BEND	PASS	QW-462.2 SIDE BEND	PASS

TOUGHNESS TEST (QW-170)

[illegible]

HARDNESS TEST - Brinell Hardness

[illegible]

N1: Interpass cleaning not considered peening.

N2: Refer to Appendix PQR for all other variables.

N3:

N4:

N5: Original PQR - P1-P8-DS Rev 1 3/31/94

Welder Name: R. CARTER Stamp: 8 ID Number: 699

Tests Conducted By: CMS Laboratory Test Number: C-34-247

PQR was done and welding of coupon was witnessed by: EATON METAL PRODUCTS COMPANY

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY

ACCEPTED BY: PLANT 1 DENVER, CO

ACCEPTED BY PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY PLANT 3 POCA TELLO. ID Page 2 of 2

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APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimins used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME)

EATON METAL PRODUCTS COMPANY LLC

WPS No P1-P8-GMAWP-A Date 1/11/2017 Revision 2

Supporting PQR No(s) P1-P8-GMAWP-A

BASE METAL (QW-403)		JOINT (QW-402, QW-405)	
P # <u>1</u>	Gr # <u>-</u> to P # <u>8</u> Gr # <u>-</u>	Groove <u>ALL + 3G≤60°</u>	Fillet <u>ALL</u>
Thickness Range <u>3/16</u>	to <u>8</u>	Progression <u>UPHILL</u>	Fillet Weld Size <u>ANY</u>
Backing <u>YES</u>	Backing Material <u>BASE/WELD METAL</u>	60-Degree Inclination Angle <u>MAX</u>	
Type: <u>Semi-Automatic</u>		PREHEAT (F) (QW-406)	
POST WELD HEAT TREATMENT (F) (QW-407)		Minimum Temperature <u>50</u>	
Temperature Range <u>-</u>		Maximum Interpass Temperature <u>350</u>	
Time Range <u>-</u>		Preheat Maintenance <u>PRIOR / DURING</u>	

PROCESS / TYPE	GMAWP	
FILLER METAL (QW-404)		
AWS Classification	<u>ER309L</u>	
SFA# / AWS Specification	<u>5.9</u>	
F #	<u>6</u>	
A # or Chemical Composition	<u>8</u>	
Filler Metal Trade Name	<u>-</u>	
Filler Metal Diameter	<u>0.045</u>	
Maximum Weld Metal Thickness	<u>8</u>	
SHIELDING (QW-408)		
Electrode-Flux (Class)	<u>-</u>	
Flux Trade Name / Type	<u>-</u>	
Shielding Gas / CFH	<u>98% Ar - 2%CO2 / 35CFH min</u>	
Gas Cup Size	<u>1/2 - 3/4</u>	
Trailing Gas / CFH	<u>-</u>	
Backing Gas / CFH	<u>-</u>	
ELECTRICAL (QW-410)		
Current	<u>DCEP</u>	
GMAW, FCAW		
Transfer Mode	<u>PULSED SPRAY</u>	
GTAW		
Electrode Type	<u>-</u>	
Electrode Size	<u>-</u>	
TECHNIQUE (QW-410)		
Beads	<u>STRINGER - Each bead ≤ 5/8" wide</u>	
Pass	<u>MULTIPLE</u>	
Number of Electrodes	<u>1</u>	
ELECTRODE SPACING		
Longitudinal	<u>-</u>	
Angle	<u>-</u>	
Contact Tube to Work Distance	<u>1/2 - 1</u>	
Peening	<u>NONE</u>	
Interpass Cleaning	<u>MANUAL / MECHANICAL</u>	

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Maximum Heat Input for any Diameter = <u>-</u> J/in
ANY/ALL	GMAWP	ER309L	0.045	DCEP	170-210	24-28	4-12	-	By <u>John H. Hest</u>
-	-	-	-	-	-	-	-	-	Accepted By PLANT 1 DEN
-	-	-	-	-	-	-	-	-	Accepted By PLANT 2 SLC
-	-	-	-	-	-	-	-	-	Accepted By PLANT 3 POC

Interpass cleaning not considered peening.
Refer to Appendix WPS for all other variables.
Only weld joint details accepted by the Company Representative shall be used.
This WPS is only used for material which does not require notch-toughness testing.
Lincoln Invertec V-350Pro Pulsed MIG Stainless 0.045, 175WFS, 180SPD
Uncontrolled copy if actual signature not signed by plant representative.

APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 4

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____	PLANT 1 DENVER, CO
ACCEPTED BY _____	PLANT 2 SALT LAKE CITY, UT
ACCEPTED BY _____	PLANT 3 POCATELLO, ID

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PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No

P1-P8-GMAWP-A

Date 11/13/2009 Revision

1

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PLATE	Thickness*	1.5	Type	V-GROOVE	Groove Angle	50
Material Spec	SA516-70	P #	1	Gr #	2	Root Opening	0
Material Spec	SA240-304L	P #	8	Gr #	1	Root Face	1/8
* Weld thickness = to plate thickness				Backgouge	YES	Back Welded	YES
PREHEAT (F) (QW-406)				Test Position	3G	Vertical Progression	UPHILL
Minimum Temperature	50			45° INCLINATION ANGLE			
Maximum Interpass Temperature	350			POST WELD HEAT TREATMENT (F) (QW-407)			
Preheat Maintenance	PRIOR / DURING			Temperature Range	-		
				Time Range	-		

PROCESS / TYPE	GMAWP	
FILLER METAL (QW-404)		
AWS Classification	ER309LSi	-
SFA# / AWS Specification	5.9	-
F #	6	-
A # or Chemical Composition	8	-
Filler Metal Trade Name	Lincoln Murex 309LSi	-
Filler Metal Diameter	0.045	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	98% Ar - 2%CO2 / 35CFH min	-
Gas Cup Size	5/8	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	-	-
ELECTRICAL (QW-409)		
Current	DCEP	-
GMAW, FCAW		
Transfer Mode	PULSED SPRAY	-
GTAW		
Electrode Type	-	-
Electrode Size	-	-
TECHNIQUE (QW-410)		
Beads	STRINGER	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	1/2 - 1	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ROOT	GMAWP	ER309L	0.045	DCEP	190	26	10	29,640	-
MID	GMAWP	ER309L	0.045	DCEP	190	26	7	42,343	-
CAP	GMAWP	ER309L	0.045	DCEP	190	26	5	59,280	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = 59,280 J/in = $\frac{\text{Amps} \times \text{Volts} \times 60}{\text{Travel Speed}}$

EATON METAL PRODUCTS COMPANY LLC

P1-P8-GMAWP-A

Date 11/13/2009 Revision 1

[illegible]

N5: Test Plate: Jindal Stainless Corporation Heat #:1F0088 / Ipsco Heat #A4E165

Page 2 of 2

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APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimens used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME)

EATON METAL PRODUCTS COMPANY LLC

WPS No _____ P1-P8-GTAW-AL Date 12/17/2009 Revision 1
Supporting PQR No(s) _____ P1-P8-GTAW-AL

BASE METAL (QW-403)

P # 1 Gr # - to P # 8 Gr # -
Thickness Range 1/16 to 0.436
Backing NO Backing Material -

JOINT (QW-402, QW-405)

Groove ANY Fillet ALL
Progression UPHILL Fillet Weld Size ANY

POST WELD HEAT TREATMENT (F) (QW-407)

Temperature Range -
Time Range -

PREHEAT (F) (QW-406)

Minimum Temperature 50
Maximum Interpass Temperature 350
Preheat Maintenance PRIOR / DURING

PROCESS / TYPE

GTAW

FILLER METAL (QW-404)

AWS Classification
SFA# / AWS Specification
F #
A # or Chemical Composition
Filler Metal Trade Name
Filler Metal Diameter
Maximum Weld Metal Thickness

ER309L

5.9

6

8

-

3/32

0.436

SHIELDING (QW-408)

Electrode-Flux (Class)
Flux Trade Name / Type
Shielding Gas / CFH
Gas Cup Size
Trailing Gas / CFH
Backing Gas / CFH

100%Argon / 30-60CFH

ANY

100%Argon / 10-30CFH

ELECTRICAL (QW-410)

Current
GMAW, FCAW

DCEN

Transfer Mode

GTAW

Electrode Type
Electrode Size

EWL a-1.5, 1.5% Lanthana (GOLD)

3/32

TECHNIQUE (QW-410)

Beads
Pass
Number of Electrodes

WEAVE

MULTIPLE

1

ELECTRODE SPACING

Longitudinal
Angle
Contact Tube to Work Distance
Peening
Interpass Cleaning

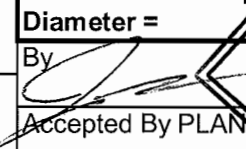
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-

-

NONE

MANUAL / MECHANICAL

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Maximum Heat Input Diameter =
ANY/ALL	GTAW	ER309L	3/32	DCEN	150max	15max	1min	-	By  JASON J. HART 02030171
-	-	-	-	-	-	-	-	-	Accepted By PLANT 1 DEN
-	-	-	-	-	-	-	-	-	Accepted By PLANT 2 SLC
-	-	-	-	-	-	-	-	-	Accepted By PLANT 3 POC

Interpass cleaning not considered peening.
Refer to Appendix WPS for all other variables.
This WPS is only used for material which does not require notch-toughness testing

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APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 4

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO
ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT
ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P1-P8-GTAW-AL Date 12/16/2009 Revision 1

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PIPE	Thickness*	0.218	Type	SINGLE BEVEL	Groove Angle	60
Material Spec	SA312-304L	P #	8	Gr #	1	Root Opening	3/32
Material Spec	SA53 Tp.E Gr.B	P #	1	Gr #	1	Root Face	1/16
*Weld thickness = to pipe thickness				Backgouge	NO	Back Welded	NO
PREHEAT (F) (QW-406)				POST WELD HEAT TREATMENT (F) (QW-407)			
Minimum Temperature	50			Temperature Range	-		
Maximum Interpass Temperature	350			Time Range	-		
Preheat Maintenance	PRIOR / DURING						

PROCESS / TYPE	GTAW	-
FILLER METAL (QW-404)		
AWS Classification	ER309L	-
SFA# / AWS Specification	5.9	-
F #	6	-
A # or Chemical Composition	8	-
Filler Metal Trade Name	-	-
Filler Metal Diameter	3/32	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	100%Argon / 45CFH	-
Gas Cup Size	5	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	100%Argon / 20CFH	-
ELECTRICAL (QW-409)		
Current	DCEN	-
GMAW, FCAW		
Transfer Mode	-	-
GTAW		
Electrode Type	EWTh-2, 2% THORIA	-
Electrode Size	3/32	-
TECHNIQUE (QW-410)		
Beads	WEAVE	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	-	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ALL	GTAW	ER309L	3/32	DCEN	110-150	10-15	1-3	135,000	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = 135,000 J/in = $\frac{\text{Amps} \times \text{Volts} \times 60}{\text{Travel Speed}}$

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No. _____ P1-P8-GTAW-AL Date 12/16/2009 Revision 1

TENSILE TEST (QW-150)

SPECIMEN NO.	WIDTH (IN)	THICK (IN)	AREA (SQIN)	ULTIMATE TOTAL LOAD	ULTIMATE STRESS (PSI)	LOCATION OF FAILURE
1-1	0.75	0.193	0.145	9,188	63,475	BASE METAL - SA53
1-2	0.748	0.195	0.146	9,357	64,151	BASE METAL - SA53
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
(2) QW-462.3 FACE BENDS	PASS	(2) QW-462.3 ROOT BENDS	PASS
-	-	-	-

TOUGHNESS TEST (QW-170)

SPECIMEN NO.	NOTCH LOCATION	NOTCH TYPE	TEST TEMP (F)	IMPACT VALUES (FT-LBS)	LATERAL EXP.		DROP WEIGHT BREAK
					SHEAR %	MILS	
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-

HARDNESS TEST - Rockwell B

BASE METAL				HEAT AFFECTED ZONE			WELD METAL		
	1	2	3	1	2	3	1	2	3
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

N1: Interpass cleaning not considered peening.

N2: Refer to Appendix PQR for all other variables.

N3:

N4:

N5: Test Pipe: SA312-304L =TaChen Heat# 707585, SA53 Type E Grade B = Ipsco Heat# 267234

Welder Name: STAN NEFF Stamp: SN ID Number: 8002

Tests Conducted By: MSI TESTING, INC. Laboratory Test Number: 09-083

PQR was done and welding of coupon was witnessed by: EATON METAL PRODUCTS COMPANY LLC

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY

ACCEPTED BY

ACCEPTED BY

ACCEPTED BY

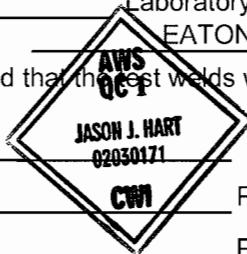
PLANT 1 DENVER, CO

PLANT 2 SALT LAKE CITY, UT

PLANT 3 POCATELLO, ID

Page 2 of 2

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APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimens used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME)**EATON METAL PRODUCTS COMPANY LLC**WPS No P8-P8-GMAWP-A Date 10/16/2018 Revision 3Supporting PQR No(s) P8-P8-GMAWP-A, P8-P8-GMAWP-A-1**BASE METAL (QW-403)**P # 8 Gr # N/A to P # 8 Gr # N/A
Thickness Range 3/16 to 8
Backing YES Backing Material BASE/WELD METAL**JOINT (QW-402, QW-405)**Groove ALL Fillet ALL
Position ANY Fillet Weld Size ANY
Progression UPHILL**POST WELD HEAT TREATMENT (F) (QW-407)**Temperature Range NONE
Time Range NONE**PREHEAT (F) (QW-406)**Minimum Temperature 100
Maximum Interpass Temperature 400
Preheat Maintenance PRIOR / DURING**PROCESS / TYPE****GMAWP****GMAWP****FILLER METAL (QW-404)**AWS Classification
SFA# / AWS Specification
F #
A # or Chemical Composition
Filler Metal Trade Name
Filler Metal Product Form
Filler Metal Diameter
Maximum Weld Metal ThicknessER3XX5.968N/ASOLID0.0458**SHIELDING (QW-408)**Electrode-Flux (Class)
Flux Trade Name / Type
Shielding Gas / CFHN/AN/A98% Ar - 2%CO2 / 35CFH min or
98% Ar - 2% O2 / 35CFH min1/2 - 3/4N/AN/A

Gas Cup Size

Trailing Gas / CFH

Backing Gas / CFH

ELECTRICAL (QW-410)

Current

DCEP**GMAW, FCAW**

Transfer Mode

PULSED SPRAY**GTAW**

Electrode Type

N/A

Electrode Size

N/A**TECHNIQUE (QW-410)**

Beads

STRINGER - Each bead $\leq$ 5/8" wide

Pass

MULTIPLE

Number of Electrodes

1**ELECTRODE SPACING**

Longitudinal

N/A

Angle

N/A

Contact Tube to Work Distance

1/2 - 1

Peening

NONE

Interpass Cleaning

MANUAL / MECHANICAL

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Maximum Heat Input for any Diameter = N/A J/in
ANY/ALL	GMAWP	ER3XX	0.045	DCEP	160-210	22-24	14-20	N/A	By <u>10/16/18</u>
-	-	-	-	-	-	-	-	-	Accepted By PLANT 1 DEN
-	-	-	-	-	-	-	-	-	
-	-	-	-	-	-	-	-	-	

Interpass cleaning not considered peening.

Refer to Appendix WPS for all other variables.

Refer to Appendix SS for filler metal selection.

This WPS is only used for material which does not require notch-toughness testing.

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Accepted By PLANT 2 SLC

Accepted By PLANT 3 POC

APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 12/12/2011 Revision: 6

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.
- 3 Root spacing shall be sufficient to allow for complete joint penetration.
- 4 Bevel angle for groove welds that can only be accessed from one side (i.e. no backgouge/grind) shall be 30° or greater.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-407 PWHT When Required

- 1 For vessels that are exposed to environments that could cause stress corrosion cracking; a minimum hold time of 1 hour at a minimum temperature of 1150°F shall be applied.

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

UG-84

For weld procedures used when impact tests are required, production material must:

- a Be of the same P-Number and Group Number with the exception allowed by QW-403.5(c)
- b Be in the same heat treated condition
- c Meet the minimum notch toughness requirements

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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APPENDIX SS

EATON METAL PRODUCTS COMPANY LLC

STAINLESS STEEL

BASE - FILLER METAL COMPATABILITY CHART

DATE 1/13/2005 REVISION 0

FILLER METAL	BASE MATERIAL					
	304	304 to 316	316	321	321 to 347	347
308	X					
316	X	X	X			
317		X	X			
321				X	X	X
347				X	X	X

When low Carbon content base material required use "L" grade filler metal.
ER3XX, Si grade filler metal may be used for better wetting and bead contour.

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No P8-P8-GMAWP-A Date 2/22/2012 Revision 2

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PLATE	Thickness*	1.5	Type	V-GROOVE	Groove Angle	50
Material Spec	SA240-304L	P #	8	Gr #	1	Root Opening	0
Material Spec	SA240-304L	P #	8	Gr #	1	Root Face	1/16"
* Weld thickness = to plate thickness				Backgouge	YES	Back Welded	YES
PREHEAT (F) (QW-406)				POST WELD HEAT TREATMENT (F) (QW-407)			
Minimum Temperature	200			Test Position	1G	Vertical Progression	N/A
Maximum Interpass Temperature	300			Temperature Range	NONE		
Preheat Maintenance	PRIOR / DURING			Time Range	NONE		

PROCESS / TYPE	GMAWP	
FILLER METAL (QW-404)		
AWS Classification	ER316LSi	-
SFA# / AWS Specification	5.9	-
F #	6	-
A # or Chemical Composition	8	-
Filler Metal Trade Name	Lincoln Bluemax 316LSi	-
Filler Metal Product Form	SOLID	-
Filler Metal Diameter	0.045	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	N/A	-
Flux Trade Name / Type	N/A	-
Shielding Gas / CFH	98% Ar - 2%CO2 / 35CFH min	-
Gas Cup Size	5/8	-
Trailing Gas / CFH	N/A	-
Backing Gas / CFH	N/A	-
ELECTRICAL (QW-409)		
Current	DCEP	-
GMAW, FCAW		
Transfer Mode	PULSED SPRAY	-
GTAW		
Electrode Type	N/A	-
Electrode Size	N/A	-
TECHNIQUE (QW-410)		
Beads	STRINGER	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	N/A	-
Angle	N/A	-
Contact Tube to Work Distance	1/2 - 1	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ROOT	GMAWP	ER308LSi	0.045	DCEP	200-210	23-24	18	16,800	-
MID	GMAWP	ER308LSi	0.045	DCEP	200-210	23-24	14-16	21,600	-
CAP	GMAWP	ER308LSi	0.045	DCEP	200-210	23-24	14-16	21,600	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = 21,600 J/in = Amps x Volts x 60
Travel Speed

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P8-P8-GMAWP-A Date 2/22/2012 Revision 2

TENSILE TEST (QW-150)

SPECIMEN NO.	WIDTH (IN)	THICKNESS (IN)	AREA (SQIN)	ULTIMATE TOTAL LOAD	ULTIMATE STRESS (PSI)	LOCATION OF FAILURE
1	0.750	0.750	0.5625	39,940	71,004	BASE METAL
2	0.750	0.750	0.5625	40,050	71,200	BASE METAL
3	0.750	0.750	0.5625	40,165	71,404	BASE METAL
4	0.750	0.750	0.5625	39,785	70,729	BASE METAL
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-
-	-	-	-	-	-	-

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
(8) QW-462.2 SIDE BEND	PASS	-	-
-	-	-	-

TOUGHNESS TEST (QW-170)

SPECIMEN NO.	NOTCH LOCATION	NOTCH TYPE	TEST TEMP (F)	IMPACT VALUES (FT-LBS)	LATERAL EXP.		DROP WEIGHT BREAK
					SHEAR %	MILS	
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-

HARDNESS TEST - Rockwell B

BASE METAL				HEAT AFFECTED ZONE			WELD METAL		
	1	2	3	1	2	3	1	2	3
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

- N1: Interpass cleaning not considered peening.
 N2: Refer to Appendix PQR for all other variables.
 N3:
 N4:
 N5: Test Plate: ENCORE METALS, HEAT #5RE5

Welder Name: Clair Neff Stamp: CN ID Number: 8005
 Tests Conducted By: MSI Testing, Inc. Laboratory Test Number: EATON-12-001
 PQR was done and welding of coupon was witnessed by: Eaton Metal Products Company LLC

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY *[Signature]* 2/23/12  Daniel Durtschi
 CWI 11030421
 QC1 EXP. 3/1/2014
 PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

PROCEDURE QUALIFICATION RECORD (ASME IX)

EATON METAL PRODUCTS COMPANY LLC

PQR No. P8-P8-GMAWP-A-1 Date of Welding 9/19/2018
Weld Process(es) GMAWP Type(s) Semiautomatic

JOINT DETAILS (QW-402)		
Joint Design	Butt Joint	
Groove Type	Single V	
Root Spacing	0	
Root Face	1/16"	
Backing	Yes	
Backing Type	Base Metal	
Groove Angle	50°	
Back gouged	Yes	
Retainers	None	
POSITION (QW-405)		
Test Position	1G	
Progression		

BASE METALS (QW-403)														
Material Spec	(1)	SA-240	to	(2)	SA-240	P-No	8	Gr#	1	to	P-No	8	Gr#	1
Type/Grade, or UNS Number		304/304L	to		304/304L	Heat Treated Condition					None			
Material Thickness (T)		1.5"				Diameter of Test Coupon					N/A			

FILLER METALS (QW-404)		(A)	(B)	GAS (QW-408)			
SFA Specification		5.9		Shielding	Gases	Mixture (%)	Flow Rate (cfh)
AWS Classification		ER316LSi		Trailing	AR/O2	98/2	35
F-No		6		Backing	None	None	None
A-No		8		Gas Cup Size	None	None	None
Filler Metal Trade Name		OK Autrod 316LSi		5/8"			
Filler Metal Product Form		Solid		PREHEAT (QW-406)			
Supplemental Filler Metal		N/A		Minimum Temperature			
Alloy Elements		N/A		Preheat Maintenance			
Weld Metal Thickness (t)		3/16"		Prior/During			
Maximum Pass Thickness		3/16"		TECHNIQUE (QW-410)			
ELECTRODE				Multipass or Single Pass (per side)			
Tungsten Type		N/A		Single or Multiple Electrodes			
Tungsten Size		N/A		Initial and Interpass Cleaning			
Consumable Insert Used		No		Peening Performed			
Electrode Spacing (2 Arcs)		N/A		Maximum Pass Width			
Angle		N/A		Oscillation (Machine)			
Contact Tube to Work		1/2" to 1"		In Chamber Welding (GTAW)			
				POST WELD HEAT TREATMENT (QW-407)			
				Temperature			
				Time			
				Other			

ELECTRICAL (QW-409)											
Pass(es)	Process	Transfer Mode	Class	Diameter	Current & Polarity	Amps	Volts	Travel Speed (ipm)	Heat Input (J/in)	String or Weave	Interpass Temp (°F)
1	GMAWP	Pulse-Spray	ER316LSi	0.045"	DCEP	208	23	16	17,900	String	Preheat
2	GMAWP	Pulse-Spray	ER316LSi	0.045"	DCEP	201	23	16	17,300	Weave	228°
3-6	GMAWP	Pulse-Spray	ER316LSi	0.045"	DCEP	202	23	15	18,600	Weave	290° Max
7-10	GMAWP	Pulse-Spray	ER316LSi	0.045"	DCEP	209	23	14	20,600	Weave	280° Max
11-14	GMAWP	Pulse-Spray	ER316LSi	0.045"	DCEP	203	24	15	19,500	Weave	285° Max
15-19	GMAWP	Pulse-Spray	ER316LSi	0.045"	DCEP	205	23	15	18,900	Weave	275° Max
20-23	GMAWP	Pulse-Spray	ER316LSi	0.045"	DCEP	222	23	15	20,400	Weave	280° Max

Heat input calculated using QW-409.1 (c)1, Instantaneous energy readout.

TENSILE TESTS (QW-150)

Specimen No	Width (in)	Thickness (in)	Diameter (in)	Area (in)	Ultimate Total Load (lbs)	Ultimate Stress (psi)	Location of Failure
Top -1	0.749	0.796	N/A	0.5962	56,046	94,000	WM
Top -2	0.745	0.791	N/A	0.5893	55,196	93,500	WM
Bottom -1	0.750	0.796	N/A	0.5970	56,008	94,000	WM
Bottom -2	0.749	0.795	N/A	0.5955	55,758	93,500	WM

GUIDED-BEND TESTS (QW-160)

Type and Figure No	Result	Type and Figure No	Result
QW-462.2 Side Bend	Pass	QW-462.2 Side Bend	Pass
QW-462.2 Side Bend	Pass	QW-462.2 Side Bend	Pass

TOUGHNESS TESTS (QW-170)

[illegible]

Impact testing performed to	ASME VIII
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HARDNESS TEST - ROCKWELL B

Base Metal				Heat Affected Zone			Weld Metal		

DEPOSITED CHEMICAL ANALYSIS

[illegible]

Chemical Analysis Conforms to A#

MATERIAL TRACABILITY

Item Description	SA-240 304/304L	Heat Number	M6N6	Manufacturer	North American Stainless
Item Description	SA-240 304/304L	Heat Number	M6N6	Manufacturer	North American Stainless

WELDING INFORMATION

Welding machine used	Lincoln 455M/STT w /25m Feeder Box				
Welder Name	Richard Carter	ID Number	-	Stamp	RC

TESTING INFORMATION

Tests Conducted By MSI Laboratory Test Number 18-408 Date of Testing 9/24/2018
Preparation and welding of test coupon was witnessed by Sean Dunn

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME IX.

This Procedure Qualification Record was prepared and accepted by on 10-15-18

Accepted By Plant 1 Denver, CO

Accepted By Plant 2 Salt Lake City, UT

Accepted By Plant 3 Pocatello, ID

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

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APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimins used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCA TELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME)

EATON METAL PRODUCTS COMPANY LLC

WPS No P8-P8-GTAW-AL Date 12/17/2009 Revision 4
Supporting PQR No(s) P8-P8-GTAW-AL

BASE METAL (QW-403)

P # 8 Gr # - to P # 8 Gr # -
Thickness Range 1/16 to 0.56
Backing NO Backing Material -

JOINT (QW-402, QW-405)

Groove DOUBLE BEVEL Fillet ANY
Progression UPHILL Fillet Weld Size ANY

POST WELD HEAT TREATMENT (F) (QW-407)

Temperature Range -
Time Range -

PREHEAT (F) (QW-406)

Minimum Temperature 50
Maximum Interpass Temperature 350
Preheat Maintenance PRIOR / DURING

PROCESS / TYPE

GTAW

FILLER METAL (QW-404)

AWS Classification
SFA# / AWS Specification
F #
A # or Chemical Composition
Filler Metal Trade Name
Filler Metal Diameter
Maximum Weld Metal Thickness

*ER3XX

5.9

6

8

-

1/16, 3/32, 1/8

0.56"

SHIELDING (QW-408)

Electrode-Flux (Class)
Flux Trade Name / Type
Shielding Gas / CFH
Gas Cup Size
Trailing Gas / CFH
Backing Gas / CFH

100% Ar, 50CFH Max

ANY

100% Ar, 15-30CFH

ELECTRICAL (QW-410)

Current
GMAW, FCAW

DCEN

Transfer Mode

-

GTAW

Electrode Type
Electrode Size

EWL-1.5, 1.5% Lanthana (GOLD)

3/32

TECHNIQUE (QW-410)

Beads
Pass
Number of Electrodes

WEAVE

MULTIPLE

1

ELECTRODE SPACING

Longitudinal
Angle
Contact Tube to Work Distance
Peening
Interpass Cleaning

-

-

-

NONE

MANUAL / MECHANICAL

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)
ANY/ALL	GTAW	*ER3XX	1/16	DCEN	150max	15max	1min	-
ANY/ALL	GTAW	*ER3XX	3/32	DCEN	150max	15max	1min	-
ANY/ALL	GTAW	*ER3XX	1/8	DCEN	150max	15max	1min	-
-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-

Maximum Heat Input Diameter =	By <u>JASON J. HART</u> 02030171
Accepted By PLANT <u>CWEM</u>	
Accepted By PLANT 2 SLC	
Accepted By PLANT 3 POC	

Interpass cleaning not considered peening.

Refer to Appendix WPS for all other variables.

Refer to Appendix SS for filler metal selection.

This WPS is only used for material which does not require notch-toughness testing.

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APPENDIX SS

EATON METAL PRODUCTS COMPANY LLC

STAINLESS STEEL

BASE - FILLER METAL COMPATABILITY CHART

DATE 1/13/2005 REVISION 0

		BASE MATERIAL				
FILLER METAL	304	304 to 316	316	321	321 to 347	347
308	X					
316	X	X	X			
317		X	X			
321				X	X	X
347				X	X	X

When low Carbon content base material required use "L" grade filler metal.
ER3XX, Si grade filler metal may be used for better wetting and bead contour.

APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 4

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P8-P8-GTAW-AL Date 12/16/2009 Revision 3

BASE METAL (QW-403)				JOINT (QW-402, QW-405)			
Material Form	PIPE	Thickness*	0.28	Type	SINGLE BEVEL	Groove Angle	60
Material Spec	SA-312-TP304L	P #	8	Gr #	1	Root Opening	1/8
Material Spec	SA-312-TP304L	P #	8	Gr #	1	Root Face	1/16
*Weld thickness = to pipe thickness				Backgouge	YES	Back Welded	YES
				Test Position	5G	Vertical Progression	UPHILL
PREHEAT (F) (QW-406)				POST WELD HEAT TREATMENT (F) (QW-407)			
Minimum Temperature	50			Temperature Range	-		
Maximum Interpass Temperature	350			Time Range	-		
Preheat Maintenance	PRIOR / DURING						

PROCESS / TYPE	GTAW	-
FILLER METAL (QW-404)		
AWS Classification	ER308L	-
SFA# / AWS Specification	5.9	-
F #	6	-
A # or Chemical Composition	8	-
Filler Metal Trade Name	-	-
Filler Metal Diameter	3/32	-
SHIELDING (QW-408)		
Electrode-Flux (Class)	-	-
Flux Trade Name / Type	-	-
Shielding Gas / CFH	100% Ar, 45CFH	-
Gas Cup Size	3 - 5	-
Trailing Gas / CFH	-	-
Backing Gas / CFH	100% Ar, 30CFH	-
ELECTRICAL (QW-409)		
Current	DCEN	-
GMAW, FCAW		
Transfer Mode	-	-
GTAW		
Electrode Type	EWTh-2, 2% THORIA	-
Electrode Size	3/32	-
TECHNIQUE (QW-410)		
Beads	WEAVE	-
Pass	MULTIPLE	-
Number of Electrodes	1	-
ELECTRODE SPACING		
Longitudinal	-	-
Angle	-	-
Contact Tube to Work Distance	-	-
Peening	NONE	-
Interpass Cleaning	MANUAL / MECHANICAL	-

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ALL	GTAW	ER308L	3/32	DCEN	110-150	10-15	1-3	135,000	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = 135,000 J/in = $\frac{\text{Amps} \times \text{Volts} \times 60}{\text{Travel Speed}}$

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P8-P8-GTAW-AL Date 12/16/2009 Revision 3

[illegible]

GUIDED BEND TEST (QW-160)			
FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
(2) QW-462.3(a) FACE BEND	PASS	(2) QW-462.3(a) ROOT BEND	PASS
-	-	-	-

[illegible][illegible]

N1: Interpass cleaning not considered peening.
N2: Refer to Appendix PQR for all other variables.
N3:
N4:
N5:

Welder Name: ROBERT BLEVINS Stamp: B ID Number: 774
 Tests Conducted By: MSI TESTING, INC. Laboratory Test Number: 03-318
 PQR was done and welding of coupon was witnessed by:  EATON METAL PRODUCTS COMPANY

We certify that the statements in this record are correct and the AWS test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.

BY [Signature] JASON J. HART
ACCEPTED BY _____ 02030171
_____ CWT

ACCEPTED BY PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY PLANT 3 POCA TELLO, ID

Page 2 of 2

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APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimens used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

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WELDING PROCEDURE SPECIFICATION (ASME)

EATON METAL PRODUCTS COMPANY LLC

WPS No P8-P8-SMAW-A Date 12/15/2009 Revision 4
Supporting PQR No(s) P8G1-P8G1-SMAW-A

BASE METAL (QW-403)

P # 8 Gr # - to P # 8 Gr # -
Thickness Range .1875 to 8
Backing YES Backing Material BASE/WELD METAL

JOINT (QW-402, QW-405)

Groove ANY Fillet ANY
Progression UPHILL Fillet Weld Size ALL

POST WELD HEAT TREATMENT (F) (QW-407)

Temperature Range -
Time Range -

PREHEAT (F) (QW-406)

Minimum Temperature 50
Maximum Interpass Temperature 350
Preheat Maintenance PRIOR / DURING

PROCESS / TYPE

SMAW

FILLER METAL (QW-404)

AWS Classification E3XX
SFA# / AWS Specification 5.4
F # 5
A # or Chemical Composition 8
Filler Metal Trade Name -
Filler Metal Diameter ANY
Maximum Weld Metal Thickness 8

SHIELDING (QW-408)

Electrode-Flux (Class) -
Flux Trade Name / Type -
Shielding Gas / CFH -
Gas Cup Size -
Trailing Gas / CFH -
Backing Gas / CFH -

ELECTRICAL (QW-410)

Current DCEP

GMAW, FCAW

Transfer Mode -

GTAW

Electrode Type -

Electrode Size -

TECHNIQUE (QW-410)

Beads STRINGER - Each bead $\leq 5/8$ " wide

Pass MULTIPLE

Number of Electrodes 1

ELECTRODE SPACING

Longitudinal -

Angle -

Contact Tube to Work Distance -

Peening NONE

Interpass Cleaning MANUAL / MECHANICAL

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Maximum Heat Input for any Diameter = By
ANY/ALL	SMAW	E3XXL	5/32	DCEP	90-140	26-32	7-12	-	Accepted By PLANT 1 DEN
ANY/ALL	SMAW	E3XXL	1/8	DCEP	60-120	20-25	4-8	-	Accepted By PLANT 2 SLC
ANY/ALL	SMAW	E3XXL	3/32	DCEP	40-100	19-24	3-8	-	Accepted By PLANT 3 POC
-	-	-	-	-	-	-	-	-	
-	-	-	-	-	-	-	-	-	

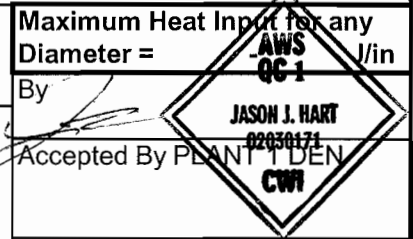
Interpass cleaning not considered peening.

Refer to appendix WPS for all other variables.

Refer to Appendix SS for filler metal selection.

This WPS is only used for material which does not require notch-toughness testing.

Uncontrolled copy if actual signature not signed by plant representative.



APPENDIX SS

EATON METAL PRODUCTS COMPANY LLC

STAINLESS STEEL

BASE - FILLER METAL COMPATABILITY CHART

DATE 1/13/05 REVISION 0

	BASE MATERIAL					
FILLER METAL	304	304 to 316	316	321	321 to 347	347
308	X					
316	X	X	X			
317		X	X			
321				X	X	X
347				X	X	X

When low Carbon content base material required use "L" grade filler metal.
ER3XX, Si grade filler metal may be used for better wetting and bead contour.

APPENDIX WPS (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 4

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Welding Procedure Specification.

** Any information on actual WPS supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers prohibited.

QW-403

- 1 No pass greater than 1/2" allowed. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts prohibited. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

The brand specific filler and/or flux listed on the WPS shall not be substituted.

Applicable to WPS with Post Weld Heat Treatment (PWHT)

A specific PWHT procedure shall be developed for each job.

All units referenced on WPS are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO
ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT
ACCEPTED BY _____ PLANT 3 POCATELLO, ID

Uncontrolled copy if actual signature not signed by plant representative.

PROCEDURE QUALIFICATION RECORD (ASME)

EATON METAL PRODUCTS COMPANY LLC

PQR No _____ P8G1-P8G1-SMAW-A Date 12/15/2009 Revision 3

BASE METAL (QW-403) Material Form <u>PLATE</u> Thickness* <u>1 1/2 & 1/2</u> Material Spec <u>SA-240, 304 & 316</u> P # <u>8</u> Gr # <u>1</u> Material Spec <u>SA-240, 304 & 316</u> P # <u>8</u> Gr # <u>1</u> *Weld thickness = to plate thickness				JOINT (QW-402, QW-405) Type <u>SINGLE BEVEL</u> Groove Angle <u>50</u> Root Opening <u>1/16</u> Root Face <u>1/16</u> Backgouge <u>YES</u> Back Welded <u>YES</u> Test Position <u>1G</u> Verticle Progression <u>-</u>			
PREHEAT (F) (QW-406) Minimum Temperature <u>50</u> Maximum Interpass Temperature <u>350</u> Preheat Maintenance <u>PRIOR / DURING</u>				POST WELD HEAT TREATMENT (F) (QW-407) Temperature Range <u>-</u> Time Range <u>-</u>			

PROCESS / TYPE	SMAW 304SS BASE	SMAW 316SS BASE
FILLER METAL (QW-404)		
AWS Classification	<u>E308L</u>	<u>E308L</u>
SFA# / AWS Specification	<u>5.4</u>	<u>5.4</u>
F #	<u>5</u>	<u>5</u>
A # or Chemical Composition	<u>8</u>	<u>8</u>
Filler Metal Trade Name	<u>-</u>	<u>-</u>
Filler Metal Diameter	<u>5/32</u>	<u>3/32, 1/8</u>
SHIELDING (QW-408)		
Electrode-Flux (Class)	<u>-</u>	<u>-</u>
Flux Trade Name / Type	<u>-</u>	<u>-</u>
Shielding Gas / CFH	<u>-</u>	<u>-</u>
Gas Cup Size	<u>-</u>	<u>-</u>
Trailing Gas / CFH	<u>-</u>	<u>-</u>
Backing Gas / CFH	<u>-</u>	<u>-</u>
ELECTRICAL (QW-409)		
Current	<u>DCEP</u>	<u>DCEP</u>
GMAW, FCAW		
Transfer Mode	<u>-</u>	<u>-</u>
GTAW		
Electrode Type	<u>-</u>	<u>-</u>
Electrode Size	<u>-</u>	<u>-</u>
TECHNIQUE (QW-410)		
Beads	<u>STRINGER / WEAVE</u>	<u>STRINGER / WEAVE</u>
Pass	<u>MULTIPLE</u>	<u>MULTIPLE</u>
Number of Electrodes	<u>1</u>	<u>1</u>
ELECTRODE SPACING		
Longitudinal	<u>-</u>	<u>-</u>
Angle	<u>-</u>	<u>-</u>
Contact Tube to Work Distance	<u>-</u>	<u>-</u>
Peening	<u>NONE</u>	<u>NONE</u>
Interpass Cleaning	<u>MANUAL / MECHANICAL</u>	<u>MANUAL / MECHANICAL</u>

Pass or Weld Layer (s)	Process	Filler Metal Class	Filler Metal Diameter	Current Type & Polarity	Amps	Volts	Travel Speed (ipm)	Max Heat Input (J/in)	Remarks
ANY	SMAW	E308L	5/32	DCEP	130	30	7-12	-	-
ANY	SMAW	E316L	1/8	DCEP	120	22	4-8	-	-
ANY	SMAW	E316L	3/32	DCEP	90	22	3-8	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-

MAXIMUM HEAT INPUT FOR ANY DIAMETER = - J/in = $\frac{\text{Amps} \times \text{Volts} \times 60}{\text{Travel Speed}}$

EATON METAL PRODUCTS COMPANY LLC

PQR No P8G1-P8G1-SMAW-A Date 12/15/2009 Revision 3

TENSILE TEST (QW-150)

SPECIMEN NO.	WIDTH (IN)	THICK (IN)	AREA (SQIN)	ULTIMATE TOTAL LOAD	ULTIMATE STRESS (PSI)	LOCATION OF FAILURE
1	0.754	1.508	1.137	103,000	90,587	WELD METAL
2	0.753	1.508	1.136	102,900	90,619	WELD METAL
T-1	1.014	0.506	0.513	46,400	90,434	BASE METAL
T-2	0.995	0.507	0.504	45,000	89,203	BASE METAL
-	-	-	-	-	-	-
-	-	-	-	-	-	-

GUIDED BEND TEST (QW-160)

FIGURE NO AND TYPE	RESULTS	FIGURE NO AND TYPE	RESULTS
4 @ QW-462.2 SIDE BEND	PASS	2 @ QW-462.3(a) FACE BEND	PASS
-	-	2 @ QW-462.3(a) ROOT BEND	PASS
-	-	-	-

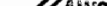
TOUGHNESS TEST (QW-170)

[illegible]

HARDNESS TEST - Brinell Hardness

[illegible]

N1: Interpass cleaning not considered peening.
N2: Refer to Appendix PQR for all other variables.
N3:
N4:
N5:
N6:
N7: Original PQR's: SS-115 1994, SS-106 1982

Welder Name: R. CARTER, BILL DERY Stamp: 8, D ID Number: 699, 236
 Tests Conducted By: CMS, COMERCIAL TESTING LAB. Laboratory Test Number: C-14-4, SS-106-D-82
 PQR was done and welding of coupon was witnessed by:  EATON METAL PRODUCTS COMPANY

We certify that the statements in this record are correct and that the test welds were prepared, welded, and tested in accordance with the requirements of ASME Section IX.
BY  

ACCEPTED BY _____  PLANT 1 DENVER, CO

ACCEPTED BY PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY PLANT 3 POCA TELLO, ID

Page 2 of 2

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APPENDIX PQR (ASME)
EATON METAL PRODUCTS COMPANY LLC

Date: 6/3/2009 Revision: 3

* This appendix addresses any Essential, Supplementary Essential, and Nonessential variables not mentioned on the Procedure Qualification Test Record.

** Any information on actual PQR supercedes this document if a conflict exists.

QW-402

- 1 Approved joints shall be on detailed drawings for individual jobs.
- 2 Retainers not used for weld test.

QW-403

- 1 No pass greater than 1/2" used in weld test. (FCAW, GMAW, SAW, SMAW)

QW-404

- 1 Consumable inserts not used for weld test. (GTAW)
- 2 Filler metal used with weld test. (GTAW)
- 3 Supplemental filler material not used in weld test. (FCAW, GMAW, SAW)
- 4 Recrushed slag not used in weld test. (SAW)
- 5 Flux not used in weld test. (FCAW, GMAW)

QW-410

- 1 Backgouge performed with air carbon arc, plasma, and/or grinder.
- 2 Oscillation not used with automatic or machine welding. (FCAW, GMAW, GTAW, SAW)
- 3 Out of chamber welding only. (GTAW)
- 4 a FCAW - semiautomatic
b SMAW - manual
c SAW - machine
d GTAW - manual

Full size impact test specimens used. (10mm x 10mm)

All units referenced on PQR are in English (Standard, i.e. psi, inches, etc.) unless specifically noted.

ACCEPTED BY _____ PLANT 1 DENVER, CO

ACCEPTED BY _____ PLANT 2 SALT LAKE CITY, UT

ACCEPTED BY _____ PLANT 3 POCATELLO, ID

Uncontrolled copy if actual signature not signed by plant representative.



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

(303) 296-4800 FAX: (303) 296-5736



Eaton Metal Products Company LLC

ENGINEERS DESIGNERS FABRICATORS
PETROLEUM EQUIPMENT

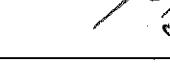
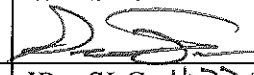
(303) 296-4800 FAX: (303) 296-5736

Inspection Records

EATON METAL PRODUCTS COMPANY LLC

INSPECTION TEST PLAN

Job No.	Customer	PO No.	Serial No.	Tag No.	National Board No.	Rev No. / Date
5361-1	Anadarko	4500100246	TBD	V-1000	TBD	Rev 0 11/27/18

INSPECTION ITEM	SIGN / DATE			REMARKS
	EMP QC	*AI	CUSTOMER	
PRE-FABRICATION				
AI HOLD POINT	H-SLC 3-15-19 	H-SLC 3/15/19 	3/15/19 WV	*EITHER HEAD/SHELL FITUP
APPROVED ITP	H - SLC 11-27-18 	11/28/18 	3/15/19 WV	ITP shall be completed for inspection points prior to opening job with the AI
APPROVED DRAWINGS	IP - SLC 11-27-18 	W - SLC 11/28/18 	H - SLC 3/15/19 WV	Drawings shall be approved by customer prior to opening job with the AI. The drawings shall be identified on the Drawing Summary Sheet. Rev A
APPROVED CALCULATIONS	H - SLC 11-27-18 	W - SLC 11/28/18 	H - SLC By APK	Calculations shall be approved by the customer prior to opening job with the AI. Hydro Summary Sheet shall accompany the calcs for the AI review. Nameplate sketch (no serial or NB numbers) shall accompany the calcs for the AI review.
APPROVED WELDING PROCEDURES	W - SLC 11-27-18 	W - SLC 11/28/18 	IP - SLC By APK WVT 3/15/19	Weld Procedures used shall be listed on approved drawings.
WELDER QUALIFICATIONS	W - SLC 11-27-18 		IP - SLC By MON 3/15/19	Available for review in each shop of fabrication.
NDE PROCEDURES	IP - SLC 11-27-18 		IP - SLC MON 3/15/19	NDE Procedures shall be reviewed and accepted by EMP QC TEAM
PREPLANNING MEETING	H - SLC 11-27-18 	H - SLC  11/28/18	WV 3/15/19	Meeting with EMP QC and AI to start job and establish hold points during fabrication. Job summary at the end of this ITP shall describe the approximate fabrication scope for each vessel in each plant

EATON METAL PRODUCTS COMPANY LLC

INSPECTION TEST PLAN

INSPECTION ITEM	SIGN / DATE			REMARKS
	EMP QC	*AI	CUSTOMER	
INPROCESS FABRICATION				
VISUAL INSPECTION (INTERNAL COMPLETED VESSEL)	H – POC 5.1.19 J. Mount	H – POC 5/1/19 Z	H – POC 5/24/2019	All surfaces and welds shall be visually examined during fabrication by QC All surfaces and welds shall be visually examined during fabrication by the AI after all welding is completed. Inspection shall take place prior to Hydro test.
VISUAL INSPECTION (EXTERNAL) COMPLETED VESSEL	H – POC 5.15.19 J. Mount	H – POC 5/15/19 Z	H – POC 5/15/19 W	All surfaces and welds shall be visually examined during fabrication by QC All surfaces and welds shall be visually examined during fabrication by the AI after all welding is completed.
COMPONENT FITUP	IP – SLC 3-29-19 J. Mount		IP - SLC W 3/29-19	All fit-up shall be within the tolerances specified in EMP Vessel Fabrication Tolerance specification
NONDESTRUCTIVE EXAMINATION				Acceptance per ASME Section VIII, Division 1 code.
RT/PAUT	H - SLC 4-19-19 J. Mount	W - SLC 4/19/19 Z	IP - SLC W 6/12/19	100% All Long Seams Spot All Girth Seams
RT/PAUT	H - POC 5.1.19 J. Mount	W - POC 5/1/19 Z	IP - POC W 6/26/19	Spot Closing Seam HSH
FINAL DIMENSIONAL	H – POC 5.15.19 J. Mount		IP - POC 5-15-19 W	All dimensions of finished vessel shall conform to the approved drawings within the tolerance of EMP Vessel Fabrication Tolerance specification
HYDRO TEST	H – POC 4/23/19 J. Mount	H – POC 4/23/19 Z	W - POC 4/22/19 W	Test shall be performed at 325 psig Temperature shall be 40°F min Hold time shall be 1 hour Test shall be recorded with a chart recorder The chart shall be signed by the operator and the serial number of the chart recorder and/or gauge used shall be noted on chart.
Water Boot				
Main Vessel	5.15.19 J. Mount	5/15/19 Z	5/15/19 W	

EATON METAL PRODUCTS COMPANY LLC

INSPECTION TEST PLAN

INSPECTION ITEM	SIGN / DATE			REMARKS
	EMP QC	*AI	CUSTOMER	
PAINT	H - POC 5.17.19 <i>J. Mount</i>		MO 7/24/2019	Surface preparation and paint shall be verified AND DOCUMENTED in accordance with P-Sheet from Engineering
FINAL CLEAN	H - POC 5.17.19 <i>J. Mount</i>		MO 7/24/2019	The ID of the vessel shall be swept out and free of blast media
SHIPPING PREPARATION	H - POC 5.17.19 <i>J. Mount</i>		MO 7/24/2019	Vessel prepared to ship with the following items All flange faces protected with covers ✓ Extra studs, nuts, and gaskets supplied with vessel ✓ All manway covers with davits secured ✓ All cribbing and supports ready for loading ✓
DOCUMENTATION				
MATERIAL TEST REPORTS (MTR)	H - SLC 4-19-19 <i>J. Mount</i>	W - SLC 4/19/19 <i>J. Mount</i>	4/12/19 MO	All pressure boundary and attachments to pressure boundary shall have an MTR or C of C.
WELD MAP DESCRIPTION (SLC SCOPE)	H - SLC 4-19-19 <i>J. Mount</i>	H - SLC 4/19/19 <i>J. Mount</i>	✓	All pressure boundary and attachments to pressure boundary welds shall have welder ID and WPS used documented
WELD MAP DESCRIPTION (POC SCOPE)	H - POC 5.17.19 5.15.19 <i>J. Mount</i>	H - POC 5/15/19 <i>J. Mount</i>	5/19/19 MO	All pressure boundary and attachments to pressure boundary welds shall have welder ID and WPS used documented
DOCUMENT INDEX LOG	H - POC 5.15.19 <i>J. Mount</i>	H - POC 5/15/19 <i>J. Mount</i>	✓	Document Index Log Initialed by QAM and AI
NDE REPORTS	H - SLC/POC 5.17.19 5.15.19 <i>J. Mount</i>		5/19/19 MO	All NDE performed on the vessel shall have a report documenting acceptance.
NONCONFORMANCE REPORTS (NCR)	H - SLC/POC 5.15.19 <i>J. Mount</i>	H - SLC/POC 5/15/19 <i>J. Mount</i>	N/A	All NCRs cleared for vessel
NAME PLATE	NONE H - POC 5.15.19 <i>J. Mount</i>	H - POC 5/15/19 <i>J. Mount</i>	5/19/19 MO	Stamped and a picture taken for records

EATON METAL PRODUCTS COMPANY LLC

INSPECTION TEST PLAN

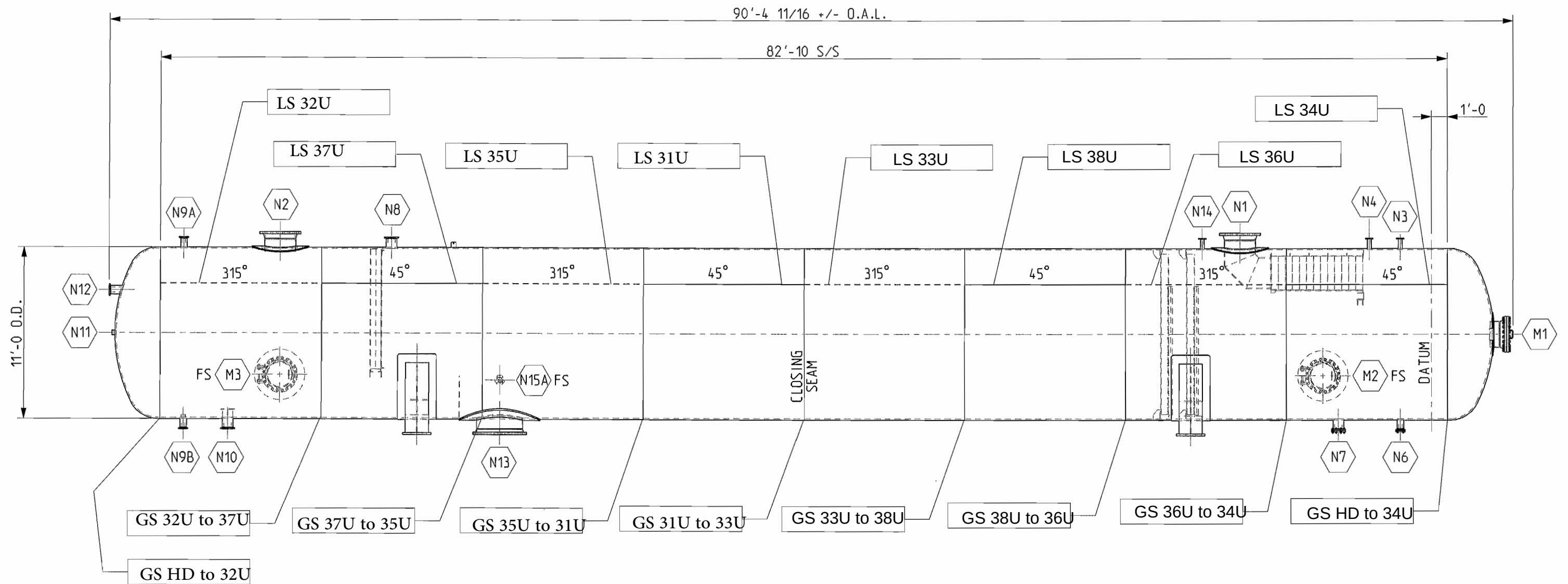
INSPECTION ITEM	SIGN / DATE			REMARKS
	EMP QC	*AI	CUSTOMER	
ASME CODE DATA SHEET	H - POC 5.15.19 <i>J. Mount</i>	H - POC 5/15/19 <i>[Signature]</i>	5/15/19 MOT	Completed and signed by AI U/A
FINAL DOCUMENT PACKAGE	H - POC 5.17.19 <i>J. Mount</i>		7/24/2019 <i>[Signature]</i>	Final document package to include: Document Index Log ✓ Manufacturers Data Report (U-1A) ✓ Nameplate Picture ✓ Manufacturers Drawings ✓ Design Calculations ✓ MTRs ✓ WPS/PQR ✓ NDE Records ✓ Completed ITP ✓ Weld Map Description ✓ Hydro Test Record ✓ NCRs N/A
COMPLETED ITP	H - POC 5.17.19 <i>J. Mount</i>		7/24/2019 <i>[Signature]</i>	All items requiring above shall be initialed by EMP QC and any items noted shall be initialed by the AI and Customer.
RELEASE FOR SHIPMENT	H - POC 5.17.19 <i>J. Mount</i>		7/24/2019 <i>[Signature]</i>	Documentation for the customer allowing the vessel to ship to job site. To be signed, reviewed and approved by ship inspector as well by customer

EATON METAL PRODUCTS COMPANY LLC

INSPECTION TEST PLAN

SUMMARY

PLANT 2 (SLC) SCOPE: (SLC, UT) Fabricate 2 Halves	PLANT 3 (POC) SCOPE: (Pocatello, ID) Closing Seam Hydro Vessel Paint Vessel	Inspection Legend: H = Hold Point IP = In Process Inspection W = Witness Point * = AI to set Hold points at beginning of job
---	---	---



Nozzle	Qty	Size	Rating	Face	Type	Service	Remarks
M3	1	20"	150#	RF	WN	MANWAY	w/ HINGE
M2	1	20"	150#	RF	WN	MANWAY	w/ HINGE
M1	1	20"	150#	RF	WN	MANWAY	w/ HINGE
N18	1	3"	150#	RF	LWN	DRAIN (IN BOOT)	
N17A/B	2	3"	150#	RF	LWN	SPARE LEVEL (IN BOOT)	
N16	1	4"	150#	RF	WN	WATER OUTLET (IN BOOT)	w/ INT PIPE
N15B/C	2	3"	150#	RF	LWN	LEVEL GAUGE (IN BOOT)	
N15A	1	3"	150#	RF	WN	LEVEL (BOOT INTERFACE)	
N14	1	2"	150#	RF	LWN	HP DRAIN RECYCLE	
N13	1	36"	150#	RF	WN	BOOT	SERIES "B"
N12	1	4"	150#	RF	LWN	LAHH	
N11	1	2"	6000#	FNPT	CPLG	SPARE	
N10	1	6"	150#	RF	LWN	LIQUID OUTLET (OIL)	w/ V.B.
N9A/B	2	3"	150#	RF	LWN	BRIDLE	w/ STINGER (N9B)
N8	1	6"	150#	RF	LWN	PSV	
N7	1	6"	150#	RF	LWN	DRAIN	w/ BLIND
N6	1	3"	150#	RF	LWN	DRAIN	w/ BLIND
N4	1	2"	150#	RF	LWN	PUMP RECYCLE	
N3	1	2"	150#	RF	LWN	VRU RECYCLE	
N2	1	24"	150#	RF	WN	OUTLET	
N1	1	24"	150#	RF	WN	INLET	w/ OIFFUSER

NOZZLE SCHEDULE

APPROVED
FOR CONSTRUCTION
DATE 11/8/18 BY *ES*

No.	Date	By	Chk'd	Revision	Description
				EATON METAL PRODUCTS CO LLC	
				DENVER -- SALT LAKE CITY	
				WELD MAP	
				132" OD x 82'-10" S/S INLET SLUG CATCHER	
				P.O. # 4500100246 - TAG # V-1000	
				Loc: JOHNSTOWN COMPRESSOR STATION, COLORADO	
				Cust: ANADARKO E&P ONSHORE LLC	
				EMP	
				Job No. 5361-S01	
				Dwg. No. D-5361-1WM	



Drawn By: RT
Date: 10/23/2018
Chk'd By: *ES*
Date: 11/8/18

EATON METAL PRODUCTS COMPANY LLC

IN-PROCESS INSPECTION RECORD AND WELD MAP DESCRIPTION

JOB NUMBER 5361-1

VESSEL SERIAL NUMBER _____

DESCRIPTION	FIT-UP	WELDER ID & PROCEDURE KEY		VISUAL ACCEPT	NDE ACCEPT/TYPE		
Weld GS HD /32U Girth Seam MK 1-1 to 1-3 Head to Shell	SLC #2 RS DG	INSIDE LK II	OUTSIDE LK II	SLC #2 Lead RK QC DG	RT Spot SD		
Weld LS 32U Long Seam MK 1-3 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		
Weld GS 32U/37U Girth Seam MK 1-3 to 1-2 Shell to Shell	SLC #2 RS DG	INSIDE LK II	OUTSIDE LK II	SLC #2 Lead RK QC DG	RT Spot SD		
Weld LS 37U Long Seam MK 1-2 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		
Weld GS 37U/35U Girth Seam MK 1-2 to 1-2 Shell to Shell	SLC #2 RS DG	INSIDE CC II	OUTSIDE LK II	SLC #2 Lead RK QC DG	RT Spot SD		
Weld LS 35U Long Seam MK 1-2 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		
Weld GS 35U/31U Girth Seam MK 1-2 to 1-3 Shell to Shell	SLC #2 RS DG	INSIDE CC II	OUTSIDE CC II	SLC #2 Lead RK QC DG	RT Spot SD		
Weld LS 31U Long Seam MK 1-3 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		
Weld GS 31U/33U Girth Seam MK 1-3 to 1-3 Shell to Shell CS	POC #3 JS BA AD	INSIDE JS I NS I	OUTSIDE FZ I GG I	POC #3 Lead SA QC AD	RT Spot JM AD		
Weld LS 33U Long Seam MK 1-3 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		
Weld GS 33U/38U Girth Seam MK 1-3 to 1-2 Shell to Shell	SLC #2 RS DG	INSIDE FZ III	OUTSIDE FZ III	POC #3 Lead SA QC AD	RT Spot JM AD		
Weld LS 38U Long Seam MK 1-2 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		
Weld GS 38U/36U Girth Seam MK 1-2 to 1-2 Shell to Shell	SLC #2 RS DG	INSIDE JF III FZ III	OUTSIDE JF III FZ III	POC #3 Lead SA QC AD	RT Spot JM AD		
Weld LS 36U Long Seam MK 1-2 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		
Weld GS 36U/34U Girth Seam MK 1-2 to 1-3 Shell to Shell	SLC #2 RS DG	INSIDE JF III	OUTSIDE JF III	POC #3 Lead SA QC AD	RT Spot JM AD		
Weld LS 34U Long Seam MK 1-3 Shell	SLC #2 BS DG	INSIDE RC II	OUTSIDE RC II	SLC #2 Lead RK QC DG	RT 100% SD		

EATON METAL PRODUCTS COMPANY LLC

IN-PROCESS INSPECTION RECORD AND WELD MAP DESCRIPTION

JOB NUMBER 5361-1

VESSEL SERIAL NUMBER _____

DESCRIPTION	FIT-UP	WELDER ID & PROCEDURE KEY		VISUAL ACCEPT	NDE ACCEPT/TYPE		
Weld GS 34U/HD Girth Seam MK 1-3 to 1-1 Shell to Head	SLC #2 CC DG	INSIDE FZ III	OUTSIDE JF III FZ III	POC #3 Lead SA QC AD	RT Spot JM AD		
Nozzle N1 RFLWN to Pipe 1D-9 to 1D-2	SLC #2 JW DG	INSIDE JW IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Nozzle N1 Pipe to Shell 1D-9 to 1-2	POC #3 JS AD	INSIDE NS I	OUTSIDE JS I	POC #3 Lead SA QC AD			
Nozzle N1 Pipe to Repad 1D-9 to 1D-14	POC #3 JS AD		OUTSIDE NF I	POC #3 Lead SA QC AD			
Nozzle N1 Repad to Shell 1D-14 to 1-2	POC #3 JS AD	INSIDE CD I NS I	OUTSIDE JS I	POC #3 Lead SA QC AD		POC #3 Air Test AD	
Nozzle N1 Pipe to Pipe 1G-4 to 1D-9	POC #3 CD BA AD	INSIDE CD IX	OUTSIDE CD IX	POC #3 Lead SA QC AD			
Nozzle N2 RFLWN to Pipe 1D-9 to 1D-2	SLC #2 JW DG	INSIDE JW IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Nozzle N2 Pipe to Shell 1D-9 to 1-3	SLC #2 RS RK DG	INSIDE SW I JE I	OUTSIDE SW I	SLC #2 Lead RK QC DG			
Nozzle N2 Pipe to Repad 1D-9 to 1D-14	SLC #2 RS RK DG		OUTSIDE SW I	SLC #2 Lead RK QC DG			
Nozzle N2 Repad to Shell 1D-14 to 1-3	SLC #2 RS DG		OUTSIDE JE I	SLC #2 Lead RK QC DG		SLC #2 Air Test DG	
Nozzle N3 RFLWN to Shell 1D-7 to 1-3	POC #3 JS AD	INSIDE CD I	OUTSIDE JS I	POC #3 Lead SA QC AD			
Nozzle N4 RFLWN to Shell 1D-7 to 1-3	POC #3 JS AD	INSIDE CD I	OUTSIDE JS I	POC #3 Lead SA QC AD			
Nozzle N6 RFLWN to Shell 1D-5 to 1-3	POC #3 BA AD	INSIDE JF I	OUTSIDE JS I NF I	POC #3 Lead SA QC AD			
Nozzle N7 RFLWN to Shell 1D-3 to 1-3	POC #3 BA AD	INSIDE JF I	OUTSIDE JS I NF I	POC #3 Lead SA QC AD			
Nozzle N8 RFLWN to Shell 1D-3 to 1-2	SLC #2 CC SW DG	INSIDE JE I	OUTSIDE RS I	SLC #2 Lead RK QC DG			
Nozzle N9A RFLWN to Shell 1D-5 to 1-3	SLC #2 CC SW DG	INSIDE SW I	OUTSIDE RS I	SLC #2 Lead RK QC DG			

EATON METAL PRODUCTS COMPANY LLC

IN-PROCESS INSPECTION RECORD AND WELD MAP DESCRIPTION

JOB NUMBER 5361-1

VESSEL SERIAL NUMBER _____

DESCRIPTION	FIT-UP	WELDER ID & PROCEDURE KEY		VISUAL ACCEPT	NDE ACCEPT/TYPE		
Nozzle N9B RFLWN to Shell 1D-5 to 1-3	SLC #2 CC SW DG	INSIDE JE I	OUTSIDE RS I	SLC #2 Lead RK QC DG			
Nozzle N9B Pipe to RFLWN 1D-11 to 1D-5	SLC #2 RK DG		OUTSIDE JW I	SLC #2 Lead RK QC DG			
Nozzle N10 RFLWN to Shell 1D-3 to 1-3	SLC #2 RK DG	INSIDE JE I	OUTSIDE SW I	SLC #2 Lead RK QC DG			
Nozzle N10 Plate to RFLWN 1D-16 to 1D-3	SLC #2 SW DG		OUTSIDE SW I	SLC #2 Lead RK QC DG			
Nozzle N10 Plate to RFLWN 1D-17 to 1D-3	SLC #2 SW DG		OUTSIDE SW I	SLC #2 Lead RK QC DG			
Nozzle N11 Coupling to Head 1D-8 to 1-1	SLC #2 RS DG	INSIDE RS I	OUTSIDE RS I	SLC #2 Lead RK QC DG			
Nozzle N12 RFLWN to Head 1D-4 to 1-1	SLC #2 RS DG	INSIDE RS I	OUTSIDE RS I	SLC #2 Lead RK QC DG			
Nozzle N13 RFLWN to Pipe 1D-1 to 1D-12	SLC #2 JW DG	INSIDE JW IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Nozzle N13 Pipe to Shell 1D-12 to 1-2	SLC #2 RS RK DG	INSIDE JE I SW I	OUTSIDE RS I CC I SW I	SLC #2 Lead RK QC DG			
Nozzle N13 Pipe to Repad 1D-12 to 1D-13	SLC #2 RS RK DG		OUTSIDE RS I CC I SW I	SLC #2 Lead RK QC DG			
Nozzle N13 Repad to Shell 1D-13 to 1-2	SLC #2 RS SW DG		OUTSIDE RS I CC I SW I	SLC #2 Lead RK QC DG		SLC #2 Air Test DG	
Boot Long Seam MK# 1H-2	SLC #2 BS DG	INSIDE JW IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Boot RFLWN to Plate 1H-1 to 1H-2	SLC #2 JW DG	INSIDE JW III	OUTSIDE JW III	SLC #2 Lead RK QC DG			
Boot Plate to Head 1H-2 to 1H-3	SLC #2 JW DG	INSIDE JW IV	OUTSIDE JW III	SLC #2 Lead RK QC DG			
Nozzle N14 RFLWN to Shell 1D-7 to 1-2	POC #3 JS AD	INSIDE CD I	OUTSIDE NS I	POC #3 Lead SA QC AD			
Nozzle N15A RFLWN to Pipe 1D-6 to 1D-10	SLC #2 RK DG	INSIDE JW VI	OUTSIDE JW VI	SLC #2 Lead RK QC DG			

EATON METAL PRODUCTS COMPANY LLC

IN-PROCESS INSPECTION RECORD AND WELD MAP DESCRIPTION

JOB NUMBER 5361-1
VESSEL SERIAL NUMBER _____

DESCRIPTION	FIT-UP	WELDER ID & PROCEDURE KEY		VISUAL ACCEPT	NDE ACCEPT/TYPE		
Nozzle N15A Pipe to Shell 1D-10 to 1-2	SLC #2 RS DG	INSIDE SW I	OUTSIDE JE I	SLC #2 Lead RK QC DG			
Nozzle N15B RFLWN to Boot 1H-5 to 1H-2	SLC #2 RK DG	INSIDE JW IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Nozzle N15C RFLWN to Boot 1H-5 to 1H-2	SLC #2 RK DG	INSIDE JW IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Nozzle N16 RFLWN to Pipe 1H-4 to 1H-6	SLC #2 JW DG	INSIDE JW III	OUTSIDE JW III	SLC #2 Lead RK QC DG			
Nozzle N16 Pipe to Pipe 1H-6 to 1H-7	SLC #2 JW DG	INSIDE JW III	OUTSIDE JW III	SLC #2 Lead RK QC DG			
Nozzle N16 Pipe to Boot 1H-6 to 1H-2	SLC #2 JW DG	INSIDE KE IV	OUTSIDE KE IV	SLC #2 Lead RK QC DG			
Nozzle N17A RFLWN to Boot 1H-5 to 1H-2	SLC #2 RK DG	INSIDE KE IV	OUTSIDE KE IV	SLC #2 Lead RK QC DG			
Nozzle N17B RFLWN to Boot 1H-5 to 1H-2	SLC #2 RK DG	INSIDE KE IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Nozzle N18 RFLWN to Head 1H-5 to 1H-3	SLC #2 RK KE DG	INSIDE JW IV	OUTSIDE JW IV	SLC #2 Lead RK QC DG			
Nozzle M1 RFLWN to Pipe 1C-1 to 1C-13	SLC #2 JW DG	INSIDE JW III	OUTSIDE JW III	SLC #2 Lead RK QC DG			
Nozzle M1 Pipe to Head 1C-13 to 1-1	SLC #2 JW JE DG	INSIDE JE I	OUTSIDE JE I	SLC #2 Lead RK QC DG			
Nozzle M1 Pipe to Repad 1C-13 to 1C-14	SLC #2 JE JE DG		OUTSIDE JE I	SLC #2 Lead RK QC DG			
Nozzle M1 Repad to Head 1C-14 to 1-1	SLC #2 JE JE DG		OUTSIDE JE I	SLC #2 Lead RK QC DG		SLC #2 Air Test DG	
Nozzle M1 Plate to RFLWN 1C-6 to 1C-1	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M1 Plate to RFLWN 1C-5 to 1C-1	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M1 Plate to Blind 1C-4 to 1C-2 x2	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			

EATON METAL PRODUCTS COMPANY LLC

IN-PROCESS INSPECTION RECORD AND WELD MAP DESCRIPTION

JOB NUMBER 5361-1

VESSEL SERIAL NUMBER _____

DESCRIPTION	FIT-UP	WELDER ID & PROCEDURE KEY		VISUAL ACCEPT	NDE ACCEPT/TYPE		
Nozzle M1 Rod to Blind 1C-8 to 1C-2	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M2 RFWN to Pipe 1J-1 to 1J-13	SLC #2 JW DG	INSIDE JW III	OUTSIDE JW III	SLC #2 Lead RK QC DG			
Nozzle M2 Pipe to Shell 1J-13 to 1-3	POC #3 JS AD	INSIDE CD I	OUTSIDE NS I	POC #3 Lead SA QC AD			
Nozzle M2 Pipe to Repad 1J-13 to 1J-14	POC #3 JS AD		OUTSIDE CD I	POC #3 Lead SA QC AD			
Nozzle M2 Repad to Shell 1J-14 to 1-3	POC #3 JS AD		OUTSIDE JS I	POC #3 Lead SA QC AD		POC #3 Air Test AD	
Nozzle M2 Plate to RFWN 1J-5 to 1J-1	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M2 Plate to RFWN 1J-6 to 1J-1	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M2 Plate to Blind 1J-4 to 1J-2	POC #3 JB AD		OUTSIDE JB	POC #3 Lead SA QC AD			
Nozzle M2 Rod to Blind 1J-8 to 1J-3	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M3 RFWN to Pipe 1J-1 to 1J-13	SLC #2 JW DG	INSIDE JW III	OUTSIDE JW III	SLC #2 Lead RK QC DG			
Nozzle M3 Pipe to Shell 1J-13 to 1-3	SLC #2 RS DG	INSIDE SW I	OUTSIDE RS I SW I	SLC #2 Lead RK QC DG			
Nozzle M3 Pipe to Repad 1J-13 to 1J-14	SLC #2 RS DG		OUTSIDE SW I	SLC #2 Lead RK QC DG			
Nozzle M3 Repad to Shell 1J-14 to 1-3	SLC #2 RS DG		OUTSIDE SW I RS I	SLC #2 Lead RK QC DG		SLC #2 Air Test DG	
Nozzle M3 Plate to RFWN 1J-5 to 1J-1	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M3 Plate to RFWN 1J-6 to 1J-1	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Nozzle M3 Plate to Blind 1J-4 to 1J-2	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			

EATON METAL PRODUCTS COMPANY LLC

IN-PROCESS INSPECTION RECORD AND WELD MAP DESCRIPTION

JOB NUMBER 5361-1

VESSEL SERIAL NUMBER _____

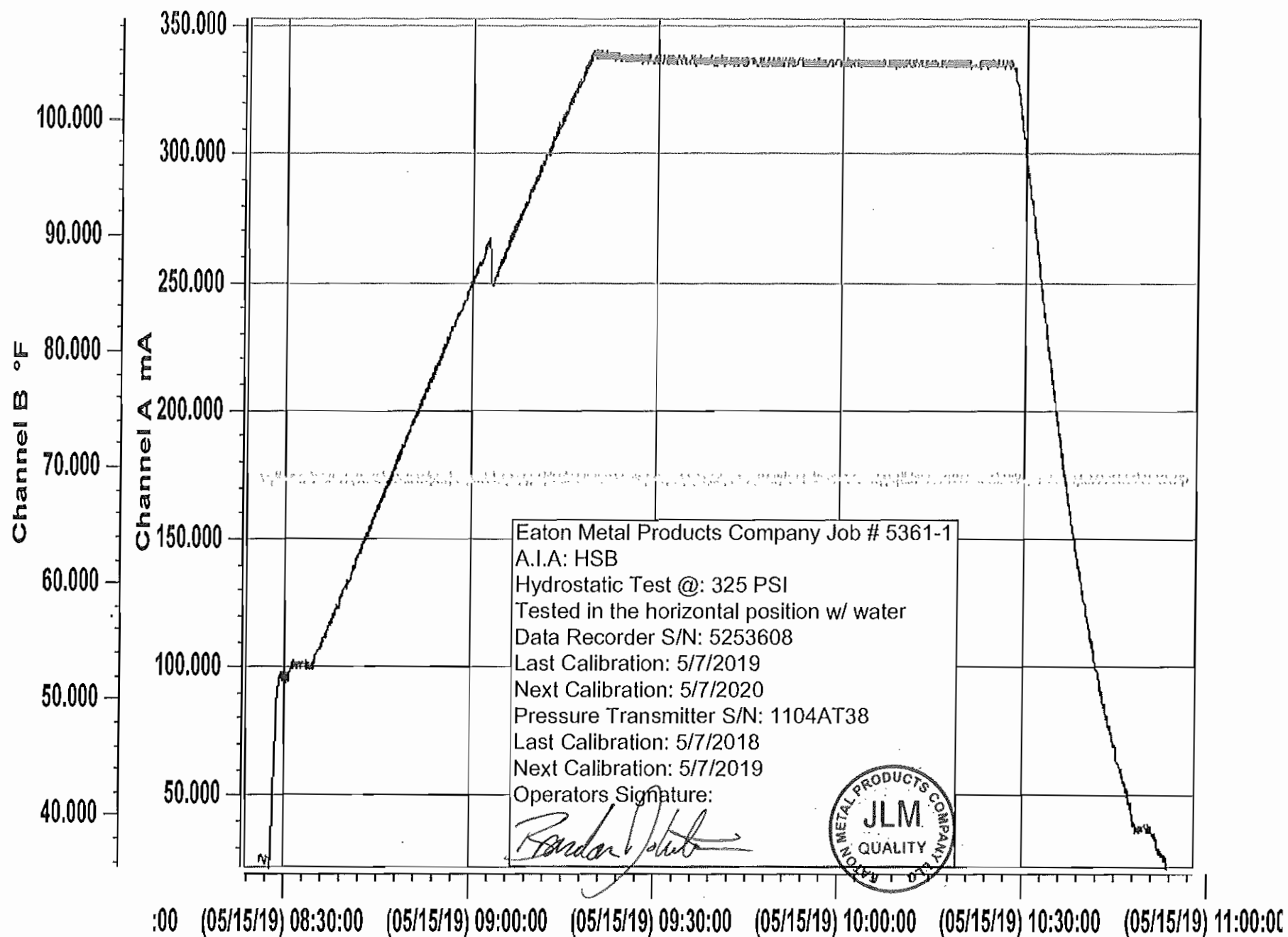
DESCRIPTION	FIT-UP	WELDER ID & PROCEDURE KEY		VISUAL ACCEPT	NDE ACCEPT/TYPE		
Nozzle M3 Rod to Blind 1J-8 to 1J-2	POC #3 JB AD		OUTSIDE JB I	POC #3 Lead SA QC AD			
Internals Weir Plate Plate to Shell 1E-3 to 1-2	SLC #2 JW DG		OUTSIDE CC I RS I	SLC #2 Lead RK QC DG			
Internals Vane Pack Plate to Shell 1E-1 to 1-2	SLC #2 JW DG		OUTSIDE CC I RP I	SLC #2 Lead RK QC DG			
Internals Plate Plate to Shell 1F-1 to 1-2	POC #3 BA AD		OUTSIDE CD IX NS IX	POC #3 Lead SA QC AD			
Internals Plate Plate to Shell 1F-3 to 1-2	POC #3 BA AD		OUTSIDE CD IX NS IX	POC #3 Lead SA QC AD			
Internals Plate Plate to Shell 1F-4 to 1-2	POC #3 BA AD		OUTSIDE CD IX NS IX	POC #3 Lead SA QC AD			
Internals Plate Plate to Shell 1G-7 to 1-2-3 x2	POC #3 BA AD		OUTSIDE CD IX NS IX	POC #3 Lead SA QC AD			
Internals Plate Plate to Shell 1G-8 to 1-3 x2	POC #3 BA AD		OUTSIDE CD IX NS IX	POC #3 Lead SA QC AD			
Internals Plate Plate to Shell 1G-9 to 1-3 x2	POC #3 BA AD		OUTSIDE CD IX NS IX	POC #3 Lead SA QC AD			
Internals Plate Plate to Shell 1G-10 to 1-3	POC #3 BA AD		OUTSIDE GG IX	POC #3 Lead SA QC AD			
Name Plate Plate to Head 1-4 to 1-1	POC #3 JS AD		OUTSIDE JS I	POC #3 Lead SA QC AD			
Saddle Pad Plate to Shell 1B-8 to 1-2 Left	POC #3 JS AD		OUTSIDE CD I	POC #3 Lead SA QC AD			
Saddle Pad Plate to Shell 1B-8 to 1-2 Right	POC #3 JS AD	INSIDE	OUTSIDE CD I	POC #3 Lead SA QC AD			

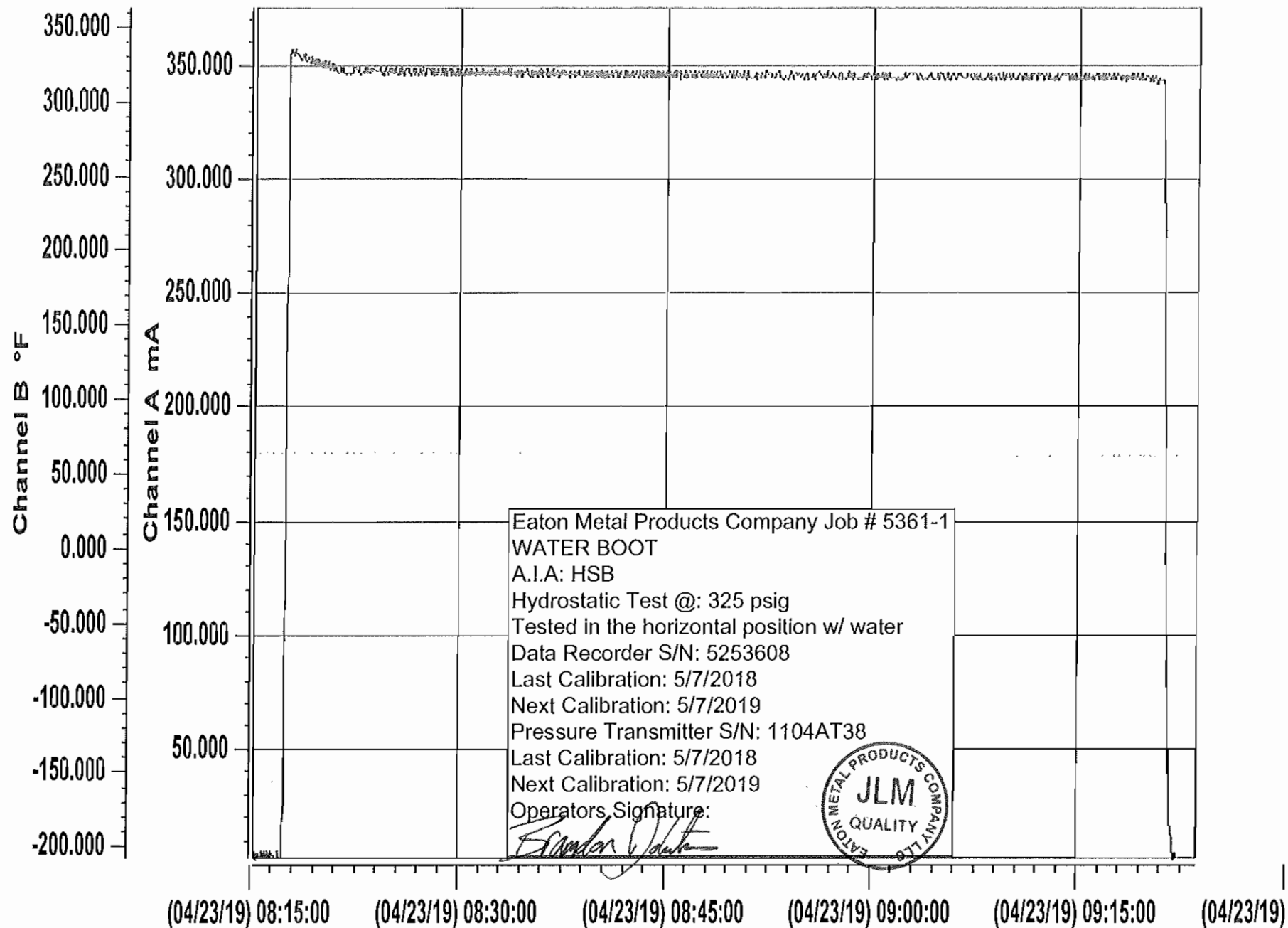
WELD PROCEDURE KEY:

I = P1-P1-GMAWP-AL
 II = P1-P1-EM14KT-A
 III = P1-P1-EM14K1-A
 IV = P1-P1-EM14K2-A
 V = P1-P1-FCAW-AL

VI = P1-P1-GTAW-AL
 VII = P1-P1-GMAWP-STT-A
 VIII = P1-P8-FCAW-AL
 IX = P1-P8-GMAWP-A
 X = P1-P8-GTAW-AL

XI = P8-P8-GMAWP-A
 XII = P8-P8-GTAW-AL
 XIII = P8-P8-SMAW-A
 XIV =
 XV =





Eaton Metal Products CO, LLC Daily Coating Inspection Report

Date:	5-13-19	M T W Th F S Su	Page 1 of 4
Job #:	5361-1	Attachments	
Inspector:	Jake Mowat	☒ DFT Sheet ☐ NCR ☐ _____ ☐ _____	
Customer:	ANADARKO		
Location:	Pocatello, ID		
Description:	132" ID Inlet Slug Ca.		
Requirements:	See paint sheet		
Contractor:	Airless	Spec. #	5361-PS1

Notes

SSPC-SP5 White Metal Blast (Green Diamond Media)

Finish Coat: 15.0-30.0 mils (INTERIOR COATING)

Sherwin-Williams Nova-Plate UHS Epoxy Novolac Tank Lining

Light Gray

40 mil MAX DFT in areas that have been stripe coated.

SSPC 6 Commercial Blast

primer 15-20 mils

Sherwin Williams Novolac UHS Epoxy

Ed's had canyon dust

Hold Point Inspections Performed

☐ 1. Pre Surface Prep/Condition & Cleanliness

☐ 2. Surface Preparation Monitoring

☒ 3. Post surface Preparation/Cleanliness & Profile

☐ 4. Pre Application Prep/Surface Cleanliness

☐ 5. Application Monitoring/Wet Film Thickness (WFT)

☒ 6. Post Application/Application Defects

☒ 7. Post Cure/Dry Film Thickness (DFT)

☐ 8. Nonconformance/corrective Actions Follow-up

☐ 9. Holiday Testing Per 1.5.5 of APC Spec

☐ 10. Final Inspection

Approved By: *J. Mowat*

Ambient Conditions

Time (am or pm)	5:30 AM			
Dry Bulb Temp° (C/F) or Ambient	69.8			
Wet Bulb Temp° (C/F)	53.2			
% Relative Humidity	21.9			
Surface Temp° (C/F) Min/Max				
Dew Point Temp° (C/F)	36.8			
Wind Direction / Speed (mph)	W-15 mph	mph	mph	mph
Weather Conditions	partly cloudy			

Testex Tape

Average Profile in mils: _____ mils

Surface Cleanliness & Profile Measurement

☒ SSPC/NACE-SP-6

☐ SSPC/NACE Spec/Ms Stds: _____

☐ Specified _____ mils avg./Achieved _____ mils

Customer's Inspector / Representative _____ Date _____

Start Time	Finish Time	Est. Sq/ft.
☐ Primer	☐ Intermediate	☐ Topcoat
☐ Touch-up		
Generic Type:	Qty Mixed:	30 gal
Manuf.: Sherwin Williams	Mix Ratio:	1 to 1
Prod. Name: Novolac UHS	Mix Method:	Drill
Prod. #: 358 0400	Strain/Screen:	60 mesh
Color: Carbonized Canyon Tan	Material Temp:	74.1 °F
Kit Sz/Cond.: 10 gal	Sweat-in Time	30 Min/Hrs
Shelf Life 24 mo.	Pot Life:	4 Min/Hrs
Batch #s	Reducer #:	N/A
(A) XM 072902	Qty Added:	N/A PVQ/Gal
(B) VM 8280 3478 26	% by Vol:	N/A %
(C)	Specific WFT Avg:	10.14 mils
Reducer:	Achieved WFT Avg:	10.14 mils
☒ Airless/Conv. Spray ☐ Brush ☐ Roller ☐ Other: _____		
☐ Air Cleanliness Check ☒ Oil Separator Check ☒ Filter Check / Replace ☐ Agitator Check		
PSI (A) 3500		
PSI (B) _____		
Painter's Signature <i>J. Mowat</i>		Date 5-13-19
Inspector's Signature <i>J. Mowat</i>		Date 5-13-19

Eaton Metal Products CO, LLC Daily Coating Inspection Report

Date:	5-6-19	M T W (Th) F S Su	Page 3 of 4
Job #:	5361-1	Attachments	
Inspector:	Jake Mowat	☒ DFT Sheet ☐ NCR ☐ ☐ 	
Customer:	ANADARKO		
Location:	Pocatello, ID		
Description:	132" ID Inlet Slug Ca.		
Requirements:	See paint sheet		
Contractor:	Airless	Spec. #	5361-PS1

Notes
SSPC-SP6 Commercial Blast Cleaning
Primer Coat: 5.0 - 10.0 mils
Sherwin-Williams Macropoxy 646 Fast Cure Epoxy
Carlsbad Canyon Tan
SSPC 5 white metal blast
Novu date with epoxy novu like
fining
light gray
40 mil MAX DFT in areas that have been strip coated

Hold Point Inspections Performed
☐ 1. Pre Surface Prep/Condition & Cleanliness
☐ 2. Surface Preparation Monitoring
☒ 3. Post surface Preparation/Cleanliness & Profile
☐ 4. Pre Application Prep/Surface Cleanliness
☐ 5. Application Monitoring/Wet Film Thickness (WFT)
☒ 6. Post Application/Application Defects
☐ 7. Post Cure/Dry Film Thickness (DFT)
☐ 8. Nonconformance/corrective Actions Follow-up
☒ 9. Holiday Testing Per 1.5.5 of APC Spec.
☒ 10. Final Inspection
Approved By: <i>J. Mowat</i>

Ambient Conditions			
Time (am or pm)	9:20		
Dry Bulb Temp° (C/F) or Ambient	75.3		
Wet Bulb Temp° (C/F)	55.2		
% Relative Humidity	26.5		
Surface Temp° (C/F) Min/Max			
Dew Point Temp° (C/F)	38.3		
Wind Direction / Speed (mph)	None mph	mph	mph
Weather Conditions	P. cloudy		

Testex Tape

Start Time	Finish Time	Est. Sq/ft.
☒ Primer	☐ Intermediate	☐ Topcoat
Generic Type:		☐ Touch-up
Manuf.: Sherwin Williams		Qty Mixed: 45 gal
Prod. Name: Novu date with epoxy novu like		Mix Ratio: 4:1
Prod. #: B6219220		Mix Method: Drill
Color: light gray		Strain/Screen: 60 mesh
Kit Sz/Cond.: 5 gal		Material Temp: 78.4 °F
Shelf Life 24 mo		Sweat-in Time 30 Min/Hrs
Batch #s		Pot Life: 7 Min/Hrs
(A) XM05871A		Reducer #: N/A
(B) XM07492A		Qty Added: ~ 100 P/Gal
(C)		% by Vol: ~ 10 %
Reducer:		Specific WFT Avg: ~ 100 Mils
		Achieved WFT Avg: ~ 100 Mils
☒ Airless/Conv. Spray ☐ Brush ☐ Roller ☐ Other:		

Surface Cleanliness & Profile Measurement	
☒ SSPONACE-SP- 5 white metal	
☐ SSPONACE Spec/Ms Stds:	
☐ Specified _____ mils avg./Achieved _____ mils	
Customer's Inspector / Representative _____ Date _____	

☒ Air Cleanliness Check	☒ Oil Separator Check
☒ Filter Check / Replace	☒ Agitator Check
PSI (A) 3500	
PSI (B)	
Painter's Signature <i>J. Mowat</i>	Date 5-6-19
Inspector's Signature <i>J. Mowat</i>	Date 5-6-19

